

# REGISTRATION FOR MODIFICATION OF AN EXISTING TRUE MINOR OIL AND NATURAL GAS SOURCE IN INDIAN COUNTRY PART 2 APPLICATION FOR PRIMUS FACILITY: PETROSHALE US 8H, US 12H, AND US 13H OIL AND GAS PRODUCTION FACILITY, MCKENZIE COUNTY, NORTH DAKOTA

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Registration for Modification of an Existing True Minor Oil and Natural Gas Source in Indian Country Part 2 Application for Primus Facility: PetroShale US 8H, US 12H, and US13H Oil and Gas Production Facility, McKenzie County, North Dakota
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i

#### **CONTENTS**

1	Introduct	ion	1
2	General F	Facility Information	2
3	Process D	escription	4
		•	
4		Calculation Methodology	
		ial to Emit	
		ated Actual Annual Emissions	
		ion Units	
	4.3.1	Crude Oil/Condensate Storage Tanks	
	4.3.2	Produced Water Tanks	
	4.3.3	Truck Loading.	
	4.3.4 4.3.5	SeparatorsFugitive Leaks	
	4.3.6	Flares	
	4.3.7	Engines	
		215.1145	
5	Emission	Summary	9
	5.1 Potent	ial to Emit	9
	5.2 Estima	ated Actual Annual Emissions	9
,	EID C O		
6 D		il and Natural Gas Well Production Facilities – Fort Berthold Indian	11
111	sci valion		**** 11
		Figures	
г:	1 C	and I are discover Color Provide	2
F18	gure 1. Gene	eral Location of the Facility	3
		Tables	
m-	1.1. 1 337.11	I. C	2
		Information	
		ion Information	
ı a		Production Data for Primus Facility: PetroShale US 8H, US 12H, and US 13H cility	5
Ta		tial to Emit in Tons per Year	
		nated Actual Annual Emissions in Tons per Year.	
		irements Referenced in the FIP for True Minor Sources in Indian Country in the Oil	
		d Natural Gas Industry Applicability Determination	11
Ta		ew of FIP for Oil & Gas Facilities in Fort Berthold Reservation	

#### **Appendices**

Appendix A. Registration for New True Minor Oil and Natural Gas Sources and Minor Modifications at Existing True Minor Oil and Natural Gas Sources Part 2 Form

Appendix B. Emission Calculations
Appendix C. Supporting Documentation

#### 1 INTRODUCTION

PetroShale (US), Inc. (PetroShale) is submitting the Registration for New True Minor Oil and Natural Gas Source form and application to the U.S. Environmental Protection Agency (EPA) Region 8 to modify the existing PetroShale US 8H facility by adding the PetroShale US 12H and 13H wells to the oil and gas production facility (Primus) (the facility). The required EPA registration form Part 2 is being submitted in accordance with the Federal Minor New Source Review (NSR) Rule codified at 40 CFR §49.151 and is included in Appendix A. The Registration for New True Minor Oil and Natural Gas Sources and Minor Modifications at Existing True Minor Oil and Natural Gas Sources Part 1 form was submitted to the EPA on December 21, 2018.

The existing PetroShale US 8H well was completed December 29, 2016 and was registered with the EPA by PetroShale on July 20, 2018. PetroShale is adding two new wells, PetroShale US 12H and US 13H, within 1/4 mile of the existing PetroShale US 8H facility. Due to the proximity of the PetroShale US 12H and US 13H wells to the existing PetroShale US 8H well, the 3 wells are considered one facility: the Primus facility. Construction commenced on the PetroShale US 12H and US 13H wells at the end of December 2018. The PetroShale US 13H well was completed May 7, 2019. The PetroShale US 12H well was completed in June 2019. Because the existing facility is located within the boundaries of the Fort Berthold Reservation and the modification commenced after October 3, 2016, the facility is registering a modification to an existing true minor oil and natural gas source per the Federal Indian Country Minor NSR Rule. All three wells are planned to operate at the facility.

Applicable attachments requested on the EPA registration form are included within this application. Section 2 of this application provides general facility information, a brief site description, and the site location. Section 3 provides a detailed process description of the operations and a discussion of the emission sources located at the newly modified existing facility. Section 4 provides a discussion of the methodology used for the emission calculations. Section 5 presents the potential to emit (PTE) and estimated actual annual emissions from the facility and compares the emissions to minor and major NSR thresholds. Section 6 reviews the requirements of the Federal Implementation Plan (FIP) for True Minor Oil and Natural Gas Sources in Indian Country and determines the applicability of each requirement to the facility. The Registration for New True Minor Oil and Natural Gas Sources and Minor Modifications at Existing True Minor Oil and Natural Gas Sources Part 2 form is included in Appendix A. Emission calculations are included in Appendix B. Supporting documentation, such as an oil and gas analyses, EPA Tanks 4.0.9d, and E&P TANK V2.0 modeling inputs and outputs, is included in Appendix C.

#### 2 GENERAL FACILITY INFORMATION

The Primus facility is an oil and gas well facility consisting of the PetroShale US 8H, US 12H, and US 13H wells. The facility operates year-round and includes equipment and related processes used in the extraction, production, separation, and storing the oil from the wells. This equipment has the potential to release regulated pollutants to the atmosphere. The facility is classified under Standard Industrial Classification (SIC) Code 1311 (crude petroleum and natural gas) and North American Industry Classification System (NAICS) Code 211111 (crude petroleum and natural gas extraction). Information concerning each well is presented in Table 1.

**Table 1. Well Information** 

Well Name	API Number	Completion Date	Status
PetroShale US 8H	33-053-07650	12/29/2016	Producing
PetroShale US 12H	33-053-07780	6/28/2019	Producing
PetroShale US 13H	33-053-07868	5/7/2019	Producing

Source: North Dakota Industrial Commission, Department of Mineral Resources, Oil and Gas Division

The Primus facility is located within the boundaries of the Fort Berthold Reservation, off Highway 23, approximately 12.5 miles west of New Town. Location information for the wells at the Primus facility is presented in Table 2. A site location map is included as Figure 1.

**Table 2. Location Information** 

Well Name	Well Name County S		Latitude, Longitude	Elevation
PetroShale US 8H	McKenzie	NENW, S17, T152N, 94W	47.991647, -102.740876	2,155 feet
PetroShale US 12H	McKenzie	NWNE, S17, T152N, 94W	47.991499, -102.736705	2,175 feet
PetroShale US 13H	McKenzie	NWNE, S17, T152N, 94W	47.991498, -102.7365	2,175 feet

Note: Primus Facility: PetroShale US 8H, US 12H, and US 13H are within the boundaries of the Fort Berthold Reservation in North Dakota.

McKenzie County is designated by the EPA as being in attainment or unclassified with respect to the National Ambient Air Quality Standards (NAAQS) for ozone  $(O_3)$ , carbon monoxide (CO), nitrogen dioxide  $(NO_2)$ , sulfur dioxide  $(SO_2)$ , particulate matter less than 10 microns in diameter  $(PM_{10})$ , particulate matter less than 2.5 microns in diameter  $(PM_{2.5})$ , and lead (Pb). Thus, the Primus Facility is not subject to nonattainment NSR.



Figure 1. General Location of the Facility

#### 3 PROCESS DESCRIPTION

This section provides a detailed description of the processes and equipment installed at the Primus facility. Emission sources located at the facility include both point and fugitive sources. The facility consists of the following primary production equipment and air pollutant emitting activities:

- One (1) separator with a 0.5 million British thermal units per hour (MMBtu/hr) heater treater fueled by produced gas;
- Two (2) separators with a 1.0 MMBtu/hr heater treater fueled by produced gas;
- One (1) 215-horsepower (hp) Caterpillar 3406NA engine fueled by natural gas;
- One (1) 400-hp Caterpillar 3408TA engine fueled by natural gas;
- Eight (8) 400-barrel crude oil/condensate storage tanks controlled by flares;
- Eight (8) 1,000-barrel crude oil/condensate storage tanks controlled by flares;
- Four (4) 400-barrel produced water storage tanks controlled by flares;
- Four (4) 1,000-barrel produced water storage tanks controlled by flares;
- Four (4) flares with 98% or greater control efficiency;
- Produced oil and gas sold via sales lines;
- Truck loading of produced water; and
- Flaring of the produced gas during upset conditions.

At the Primus facility, the produced fluids are flowing up the wellbores or are brought to the surface via the 400-hp Caterpillar 3408TA engine at PetroShale US 12H and US 13H wells and the 215-hp Caterpillar 3406NA engine at PetroShale US 8H. The produced fluids are routed via a closed system to a separator. A combination of higher temperatures and lower pressures allows for the separation of the components comprising the fluid stream. The separator reduces the pressure and heats the fluid stream to a desired temperature range to aid in the separation of oil, natural gas, and produced water. This treatment removes impurities and separates the phases to best meet sales delivery specifications for oil. The separation unit at PetroShale US 8H is heated by a 0.5 MMBtu/hr burner and fueled by produced gas. The separation units at PetroShale US 12H and 13H are each heated by 1.0 MMBtu/hr burners fueled by produced gas. The crude oil/condensate is temporarily stored in eight (8) 400-barrel storage tanks and eight (8) 1,000-barrel storage tanks before being sold via pipeline. The produced water is stored in four (4) 400-barrel storage tanks and four (4) 1,000-barrel storage tanks prior to being transported offsite by truck. The produced gas is sold via a sales gas line except during upset conditions. Four Steffesengineered flares control the emissions from the production tanks and the produced gas (with a control efficiency of 98% or greater).

#### 4 EMISSION CALCULATION METHODOLOGY

Emissions were estimated based on estimated annual production totals and the daily averages for monthly production data for the Primus Facility. The production data used in determining the facility emissions is presented in Table 3. Detailed production data is included in Appendix C.

Table 3. Well Production Data for Primus Facility: PetroShale US 8H, US 12H, and US 13H

Production Data fo Estimating Basis		Days of Production	Total Oil, BBLs	Daily Oil Production Average, BOPD <sup>1, 2</sup>	Total Gas, MCF	Daily Gas Production Average, MCFD <sup>1, 2</sup>	Total Water, BBLs	Daily Water Production Average, BWPD <sup>1, 2</sup>
100000000000000000000000000000000000000	US 8H	34	43,434	766.48	59,494	1,049.89	9,927	175.18
DTE	US 12H	30	35,421	708.42	43,525	870.50	3,235	242.63
PTE	US 13H	44	42,428	578.56	97,574	1,330.55	25,675	350.11
	Combined		121,283	2,053.47	200,593	3,250.95	38,837	767.92
	US 8H	365	144,873	396.91	212,509	582.22	45,937	125.85
Estimated Actual	US 12H	39	44,111	678.63	55,931	860.48	3,235 <sup>3</sup>	242.63 <sup>3</sup>
Annual Emissions	US 13H	117	49,008	251.32	97,574	500.38	27,965	143.41
	Combined		237,992	1,326.87	366,014	1,943.07	77,137	511.89

<sup>&</sup>lt;sup>1</sup> For PTE the daily production average assumes a 40% decline factor for the PetroShale US 8H, 12H, & 13H wells. Based on current operating conditions at the PetroShale US 8H well, it was conservatively assumed that 10% of the produced gas would be flared due to upset conditions and the rest sold via pipeline.

Emissions were estimated based on EPA AP-42 emission factors, E&P TANK V2.0 and EPA Tanks 4.0.9d tank emission models, manufacturer specifications, and site-specific facility data. Estimating the PTE used assumptions that differ from the assumptions used when estimating the actual facility emissions. The methodology for each is detailed below.

#### 4.1 Potential to Emit

In lieu of day-specific production data, the PTE was calculated based on the monthly production data for the PetroShale US 8H well for December 2016 and January 2017 (the first 34 days of production for the PetroShale US 8H well), the first 30 days of production data for the PetroShale US 12H well, and the monthly production data for May and June 2019 for the PetroShale US 13H well (the first 44 days of production for the PetroShale US 13H well) to estimate the potential average daily production of oil, water, and gas for each well. An individual oil well usually produces at its maximum rate immediately following the first date of production and subsequently declines. A 40% decline factor was applied to the daily production average for each well to account for this decline. The production rates for each well were combined to estimate the production emissions for the entire facility with all three wells operating.

The PetroShale US 8H well was connected to a gas sales pipeline on May 11, 2018 and in the most recent 12 months of production, approximately 8.4% of the produced gas was flared, the rest was sold via

<sup>&</sup>lt;sup>2</sup> The estimated actual annual emissions average daily production rate for the entire facility is based on the sum of the estimated actual daily production average was based on the most recent 12 months' of actual production for the PetroShale US 8H well. The estimated actual daily production average for the PetroShale US 12H well was based on the first 39 days of actual production. The estimated actual daily production average for the PetroShale US 13H well was based on the first 4 months of actual production.

<sup>&</sup>lt;sup>3</sup> The total water production and estimated actual annual emissions average daily water production rate for the PetroShale US 12H well is based on the first 8 days of production only.

pipeline. The US 12H and 13H wells are also connected to this gas sales pipeline. When estimating the potential to emit, it was conservatively assumed that 10% of the produced gas was flared. The flares have a 98% control efficiency. The use of the flares as air pollution control equipment is accounted for in the PTE because it is legally and practically enforceable. All produced gas from production and storage operations that is not sold must be sent to an emission control device with at least a 98% control efficiency for VOCs per the Federal Implementation Plan for Oil and Natural Gas Well Production Facilities Fort Berthold Indian Reservation (40 CFR §49.4164).

#### 4.2 Estimated Actual Annual Emissions

To estimate the actual annual emissions the actual daily production average for each well was multiplied by 365 days to get the total estimated annual production for the facility in a year. The actual daily production average was based on the production data for each well as follows:

- the most recent 12 months of operation (September 2018 through August 2019) of production for the PetroShale US 8H well;
- the first 39 days (end of August 2019 through the first of October 2019) of production for the PetroShale US 12H well; and
- the first 4 months (May 2019 through August 2019) of production for the PetroShale US 13H well.

The production rates for each well were combined to estimate the production emissions for the entire facility with all three wells operating. The PetroShale US 8H well was connected to a gas sales pipeline on May 11, 2018 and in the most recent 12 months of production, approximately 8.4% of the produced gas was flared, the rest was sold via pipeline. The US 12H and 13H wells are also connected to this gas sales pipeline. When estimating the actual annual emissions, it was assumed that the 12H and 13H wells would flare the same percentage of produced gas as the US 8H well flared for the past 12 months.

#### 4.3 Emission Units

The PTE and the estimated actual annual emissions for the Primus Facility are estimated according to the following methodology for each emission unit type.

#### 4.3.1 Crude Oil/Condensate Storage Tanks

To calculate the working, breathing, standing, and flashing losses from the eight (8) 400-barrel crude oil/condensate storage tanks and the eight (8) 1,000-barrel crude oil/condensate storage tanks, E&P TANK V2.0 was used. Inputs into the model include a representative oil and gas analysis and site-specific information. All tanks were modeled as one storage tank receiving all the produced oil from the wells. The crude oil/condensate storage tank emissions are controlled by four flares with a 98% destruction efficiency. Detailed inputs and outputs of the model are included in Appendix C.

#### 4.3.2 Produced Water Tanks

To calculate the working, breathing, standing, and flashing losses from the four (4) 400-barrel produced water storage tanks and the four (4) 1,000-barrel produced water storage tanks, EPA Tanks 4.0.9d was used. Site-specific information was input into the model. One 400-bbl tank was modeled receiving one-fourth of all the produced water from the PetroShale US 8H well. One 1,000-bbl tank was modeled

receiving one-fourth of all the produced water from the PetroShale US 12H and 13H wells. The emissions from these tank model runs were then each multiplied by four. The produced water storage tank emissions are controlled by four flares with a 98% destruction efficiency. Detailed inputs and outputs of the model are included in Appendix C.

#### 4.3.3 Truck Loading

Loading losses from produced water truck loading were calculated using AP-42 Section 5.2 – Transportation And Marketing Of Petroleum Liquids. Loading losses were calculated using the following equation:

$$L_L = 12.46 \frac{SPM}{(T + 460)}$$

Where  $L_L$  is the loading losses in pounds per 1,000 gallons of liquid loaded, S is the saturation factor for submerged loading (0.6), P is the true vapor pressure of the liquid loaded in psia (0.24 psia), M is the molecular weight of the vapors (20.7 lb/lb-mole), and T is the temperature of the bulk liquid loaded in degrees Fahrenheit (41.4 °F). All volatile organic compounds (VOCs) in the produced water are assumed to have been released to the atmosphere during truck loading.

#### 4.3.4 Separators

There are three separators used onsite for separating the produced fluid stream into oil, natural gas, and produced water. The maximum fire box heat input rating for two of the separator heaters is 1,000,000 Btu/hr, each. The maximum fire box heat input rating for the remaining separator heater is 500,000 Btu/hr. The separator heaters are fueled by produced gas which has a gross heating value of 1,535.4 Btu/scf. Any excess produced gas not sold via gas sales line is flared. There are no supplemental fuel sources. Due to design operational limits, the separator burners must be functioning while the facility is in operation. Combustion emissions from the burner used to heat the fluid stream are vented to the atmosphere.

Emissions are calculated based on the assumption that the separators will operate 8,760 hours per year. PTE and estimated actual annual emissions are based on the maximum fuel consumption of the separator heaters. Particulate matter, NO<sub>X</sub>, VOC, HAP, SO<sub>2</sub> and CO emissions have been calculated using emission factors obtained from *AP-42*, *Section 1.4 – Natural Gas Combustion, July 1998* for natural gas-fired external combustion sources. Appendix B includes detailed equations.

#### 4.3.5 Fugitive Leaks

Fugitive emissions are calculated based on the number of sources of fugitive leaks (valves, pump seals, connectors, flanges, open-ended lines, etc.) and the composition of the flashed gas from the crude oil/condensate storage tanks as calculated by E&P TANK V2.0. The number of components at the site that could be sources of fugitive leaks was estimated was based on actual counts from a similar facility. Emission factors for the fugitive leaks were based on the *US EPA Protocol for Equipment Leak Emission Estimates* (EPA-453/R-95-017) for light oil. The emission calculations for fugitive leaks are presented in Appendix B.

#### 4.3.6 Flares

Emissions from the storage tanks are vented to four Steffes-engineered flares with a 98% control efficiency. Any produced gas not used for fueling the separators or the flare pilot lights that wasn't able to

be sold via pipeline is also sent to the flare system. The pilot lights for the flares are fueled by produced gas which has a gross heating value of 1,535.4 Btu/scf. It is assumed that the pilot lights will burn continuously (8,760 hours per year) and that combustion emissions from each flare's pilot light are vented to the atmosphere.

Particulate matter,  $SO_2$ , and VOC emissions from the flare's pilot light have been calculated using emission factors obtained from AP-42,  $Section\ 1.4-Natural\ Gas\ Combustion$ , July 1998 for natural gas-fired external combustion sources.  $NO_X$  and CO emission factors are from AP-42  $Section\ 13.5-Industrial\ Flares$  to provide a more conservative estimate than the emission factors for  $NO_X$  and CO contained in AP-42  $Section\ 1.4$ . Appendix B includes detailed equations.

#### 4.3.7 Engines

The Primus Facility: PetroShale US 8H, US 12H, and US 13H facility uses an 215-hp Caterpillar 3406NA engine and a 400-hp Caterpillar 3408TA engine. The engines are fueled by natural gas and are certified to meet the emission standards of New Source Performance Standards Subpart JJJJ: Standards of Performance for Stationary Spark Ignition Internal Combustion Engines.

Emissions of CO, NO<sub>x</sub>, VOC, and CO<sub>2</sub> have been calculated based on the manufacturer's specifications. It was assumed that PM<sub>2.5</sub> was equivalent to PM<sub>10</sub> which was assumed to be equivalent to PM. For SO<sub>2</sub>, CO<sub>2</sub>, and HAPs, emission factors for a 4-stroke rich burn industrial engine from *AP-42*, *Section 3.2 – Natural Gas-Fired Reciprocating Engines* were used. A conservative estimate of the uncontrolled potential SO<sub>2</sub> emissions, using an emission factor based on the short-term (hourly) SO<sub>2</sub> emissions for natural gas (2,000 grains sulfur per million standard cubic feet of natural gas [gr S/10<sup>6</sup> scf NG]), is 0.00058 pound per million British thermal units (lb/MMBtu) (40 CFR 72.2). GHG emissions are calculated using emission factors provided from 40 CFR 98 Subpart C, Tables C-1 and C-2, for the combustion of natural gas.

Potential emissions are calculated based on the assumption that the engines will operate 8,760 hours per year. Maximum hourly emissions are calculated by multiplying the nominal bhp rating or the natural gas consumption rate of each engine and hours of operation per year by the appropriate emission factors. Appendix B provides the detailed emissions estimates with example calculations. The vendor-supplied engine certificates are included in Appendix C.

#### 5 EMISSION SUMMARY

The PTE and the estimated actual annual emissions for the facility are presented below. Detailed emission calculations are provided in Appendix B.

#### 5.1 Potential to Emit

The PTE calculated based is presented in Table 4.

Table 4. Potential to Emit in Tons per Year

Emission Source Category	voc	HAPs	NO <sub>x</sub>	СО	SO <sub>2</sub>	PM <sub>10</sub>	H <sub>2</sub> S
(3) 2-Phase Separators w/Heater Treaters	0.06	0.02	1.07	0.90	0.01	0.08	-
(16) Crude Oil/Condensate Storage Tanks	83.10	1.29	7.23	32.94	0.06	0.79	0.00
(8) Produced Water Storage Tanks	0.01	< 0.01	-	-	-	-	0.00
(4) Flare Pilots	< 0.01	< 0.01	0.02	0.09	< 0.01	< 0.01	-
Fugitive Leaks	6.61	0.34	_	-	_	_	0.00
Truck Loading	0.37	0.01	-	-	-	-	0.00
(2) Engines	4.16	0.70	5.94	11.88	0.01	0.21	-
Produced Gas	31.86	0.78	6.19	28.24	0.05	0.68	0.00
Total PTE	126.16	3.14	20.45	74.05	0.13	1.76	0.00
Minor NSR Threshold	5	-	10	10	10	5	2
Above Minor NSR Threshold?	Yes	N/A	Yes	Yes	No	No	No
Title V Major Source Threshold	100	25	100	100	100	100	-
Above Title V Major Source Threshold?	Yes	No	No	No	No	No	N/A
Major NSR Threshold	250	-	250	250	250	250	-
Above Major NSR Threshold?	No	N/A	No	No	No	No	N/A

Note:  $PM_{2.5}$  is assumed to be equal to  $PM_{10}$ .

The PTE for the entire is above the Title V major source threshold for VOC but below for the other pollutants. The PTE for the facility is above the minor NSR threshold for VOC, NO<sub>X</sub>, and CO. The Primus facility must register with the EPA per the Federal Indian Country Minor NSR Rule.

#### 5.2 Estimated Actual Annual Emissions

The estimated actual annual emissions for the Primus Facility are presented in Table 5.

Table 5. Estimated Actual Annual Emissions in Tons per Year

Emission Source Category	voc	HAPs	NO <sub>x</sub>	со	SO <sub>2</sub>	PM <sub>10</sub>	H₂S
(3) 2-Phase Separators w/Heater Treaters	0.06	0.02	1.07	0.90	0.01	0.08	~
(16) Crude Oil/Condensate Storage Tanks	53.70	0.84	4.67	21.29	0.04	0.51	0.00
(8) Produced Water Storage Tanks	0.01	< 0.01	-	-	-	-	0.00
(4) Flare Pilots	< 0.01	< 0.01	0.02	0.09	< 0.01	< 0.01	-
Fugitive Leaks	6.61	0.34	-	-	-	-	0.00

Emission Source Category	voc	HAPs	NO <sub>x</sub>	со	SO <sub>2</sub>	PM <sub>10</sub>	H₂S
Truck Loading	0.25	< 0.01	-	-	-	-	0.00
(2) Engines	4.16	0.70	5.94	11.88	0.01	0.21	_
Produced Gas	15.90	0.39	3.09	14.09	0.03	0.34	0.00
Total Actual Emissions	80.68	2.29	14.79	48.25	0.09	1.14	0.00
Minor NSR Threshold	5	-	10	10	10	5	2
Above Minor NSR Threshold?	Yes	N/A	Yes	Yes	No	No	No
Title V Major Source Threshold	100	25	100	100	100	100	-
Above Title V Major Source Threshold?	No	No	No	No	No	No	N/A
Major NSR Threshold	250	_	250	250	250	250	_
Above Major NSR Threshold?	No	N/A	No	No	No	No	N/A

Note:  $PM_{2.5}$  is assumed to be equal to  $PM_{10}$ .

The estimated actual annual emissions for the facility were greater than minor NSR thresholds (for VOC,  $NO_X$ , and CO) and, therefore, the facility must register with the EPA. The estimated actual annual emissions are less than major NSR thresholds and Title V major source thresholds.

### 6 FIP FOR OIL AND NATURAL GAS WELL PRODUCTION FACILITIES – FORT BERTHOLD INDIAN RESERVATION

The FIP is used instead of source-specific minor NSR preconstruction permits in Indian country. It incorporates emissions limits and other requirements from eight federal standards, applying limits for a range of equipment and processes used in oil and natural gas production and natural gas processing. Table 6 identifies those requirements and notes whether the requirement is applicable or not.

Table 6. Requirements Referenced in the FIP for True Minor Sources in Indian Country in the Oil and Natural Gas Industry Applicability Determination

Citation	Title	Potentially- Affected Facility Source(s)	Discussion	Applicability
40 CFR Part 60, Subpart OOOOa	The Facility: Primus Facility: PetroShale US 8H, US 12H, and US 13H, Storage Tanks, And US 13H, Storage Tanks, and Natural Gas Sector And Natural Gas Sector And And Natural Gas Sector And And Natural Gas Sector And And And Natural Gas Sector And And Is subject to the resulpart. The produced water exempt from the requirements. The well confacility are subject to the resulpart. The produced water exempt from the requirements. The well confacility are subject to the resulpart. The produced water exempt from the requirements. The well confacility are subject to the resulpart. The produced water exempt from the requirements. The well confacility are subject to the resulpart. The produced water exempt from the requirements. The well confacility are subject to the resulpart. The produced water exempt from the requirements. The well confacility are subject to the resulpart. The produced water exempt from the requirements. The well confacility are subject to the resulpart. The produced water exempt from the requirements. The well confacility are subject to the resulpart. The produced water exempt from the requirements. The well confacility are subject to the requirements. The well confacility are subject to the resulpart. The produced water exempt from the requirements. The well confacility are subject to the resulpart. The produced water exempt from the requirements and US 13H, Storage Tanks, and US 13H, Storage Tanks and US 1		The facility is a well-affected facility under this subpart and is subject to the subpart requirements. The well completions at the facility are subject to the requirements of this subpart. The produced water storage tanks are exempt from the requirements of this subpart because the PTE of the tanks is less than 1 tpy of VOC. The PTE of the crude oil/condensate storage tanks is 82.53 tpy (5.19 tpy per tank). Because the crude oil/condensate storage tanks have a PTE of less than 6 tpy per storage tank, they are exempt from the requirements of this subpart. Fugitive sources of emissions are subject to LDAR fugitive leak monitoring requirements amongst others.	Yes
40 CFR Part 60, Subpart Kb	Performance Standards for VOC Liquid Storage Tanks	Storage Tanks (≥ 75 m³)	The eight 1,000-bbl crude oil storage tanks at the facility are greater than 75 m³ (approx. 472 bbl). Therefore, these storage tanks are subject to the requirements of this subpart.	Yes
40 CFR Part 60, Subpart IIII	Performance Standards for Stationary Compression Ignition Internal Combustion Engines	None	There are no stationary compression ignition internal combustion engines at the facility.	No
40 CFR Part 60, Subpart JJJJ	Performance Standards for Stationary Spark Ignition Internal Combustion Engines	Engines	The engines at this facility are less than 500 hp and was manufactured after July 1, 2008 and is subject to the subpart requirements. The engines have been certified by the manufacturer to meet the emission standards of this subpart for non-emergency natural gas engines.	Yes
40 CFR Part 60, Subpart KKKK	Performance Standards for New Stationary Combustion Turbines	None	There are no stationary combustion turbines at the facility.	No
40 CFR Part 63, Subpart DDDDD	Air Toxics Standards for Industrial, Commercial, and Institutional Boilers and Process Heaters	Separator Heaters	The facility does not meet the subpart's definition of an affected source because it is not a major source of HAPs as defined in the subpart (the emissions from three wells at the facility are not to be combined when making the major source determination). Thus, the heaters are not subject to the requirements of this subpart.	No

Citation	Title	Potentially- Affected Facility Source(s)	Discussion	Applicability
40 CFR Part 63, Subpart HH	Air Toxics Standards for Oil and Natural Gas Production Facilities	The Facility: Primus Facility: PetroShale US 8H, US 12H, and US 13H	Primus Facility: PetroShale US 8H, US 12H, and US 13H well pad does not meet the definition of an affected facility under the referenced requirement because there are no tri-ethylene glycol dehydration units located at the facility. Therefore, the facility is not subject to the requirements of this subpart.	No
40 CFR Part 63, Subpart ZZZZ	Air Toxics Standards for Stationary Reciprocating Internal Combustion Engines	Engines	The stationary reciprocating internal combustion engine at the facility meets the requirements of subpart ZZZZ by meeting those of subpart JJJJ discussed above.	Yes

A summary of the requirements for the FIP for oil and gas well production facilities at Fort Berthold Indian Reservation is provided in Table 7.

Table 7. Review of FIP for Oil & Gas Facilities in Fort Berthold Reservation

Citation	Title	Applicability	Requirements	Compliance
			Gas produced during well (re)completion must be routed to a control device with a destruction efficiency (DRE) of at least 90%.	
40 CFR §49.4164	Construction and Operational Control Measures	Yes	Any gas emissions due to production or storage operations must be routed to a control device with a DRE of at least 90%.	PetroShale sends produced gas to a sales line except during upset conditions. The storage tank emissions are sent via a closed-vent system to the Steffes-
	Modelaree		Within 90 days from the first date of production, the facility must send the produced gas and any gas emissions from the storage tanks via a closed-vent system to either a gas sales line or to a control device with a DRE of at least 98%.	engineered flares with a DRE of 98%.
			Covers – every oil or water storage tank must have a cover that forms an impermeable barrier over the covered surface area. The cover should always be sealed shut except to add or remove material from the storage tank, inspect or sample the contained material, or for maintenance or inspections of equipment within the storage tank.	
			Closed Vent Systems – closed vent systems must always be operated properly and operate without detecting gas emissions. If the system has a bypass device, the bypass device must either have a continuously-reading natural gas flow indicator with an alarm, or else use a lock and key configuration to secure the bypass valve at the inlet to the bypass device.	
			Enclosed Combustors and Utility Flares – a flare must be operated per manufacturer specifications. The flare must be able to reduce gas VOC emissions by at least 98%. The flare must have a liquid knock-out system, a flash-back flame arrestor, either a continuously burning pilot flame with thermocouple or similar device, or an electronic automatic igniter, and a continuous monitoring system. The flare must be not be leaking or have any visible smoke emissions as determined by EPA Method 22. The flare must either:	The covers on the storage tanks at the Primus Facility: PetroShale US 8H, US
40 CFR §49.4165	Control Equipment	Yes	<ul> <li>a) have a diameter of 3" or greater, is non-assisted, has a hydrogen content of 8% by volume or more, and is designed and operated with an exit velocity less than 122 ft/s and less than V<sub>max</sub>.</li> </ul>	12H, and US 13H facility will be impermeable and used as required.  The closed vent system will be operated properly.
340.4100	Requirements		b) if the flare is unassisted, it must only be used with a net heating value for the combusted gas at 200 Btu/scf or greater; if the flare is steam- or air-assisted it must only be used when the net heating value of the combusted gas is 300 Btu/scf or greater and the maximum tip velocity (as determined in §60.18(c)(4)	The Steffes-engineered flares have all required features, will be operated per manufacturer specifications, and have a DRE of 98% as required.
			Pit Flares – pit flares that have no visible emissions and have an automatic igniter may be operated to reduce natural gas VOCs by at least 90%. An operating manual must be written specifically for the pit flare and facility. The pit flare may only be used to:	
			a) control gas emissions during well (re)completion operations, or	
			<ul> <li>to control oil or water storage tank emissions provided that the total VOC for all storage tanks at the facility is less than 20 tons per 12-month period, or</li> </ul>	
			<ul> <li>to control gas emissions that were diverted from pipeline injection to a backup control device temporarily (max. 500 hours).</li> </ul>	
			Other Control Devices – besides the control devices above, other control devices may be used with prior approval from the EPA as long as the device has a DRE of at least 98% for VOCs.	

Citation	Title	Applicability	Requirements	Compliance		
			Oil and gas production facilities at Fort Berthold Reservation will monitor the following, if applicable:			
				barrels of oil produced each time oil is unloaded from the storage tanks,		
			the volume of produced natural gas sent to the enclosed combustor, utility flare, and/or pit flare, and			
			<ul> <li>the volume of gas for all oil and produced water storage tanks that is sent to the enclosed combustor, utility flare, and/or pit flare.</li> </ul>			
40 CFR §49.4166	Monitoring Requirements	Yes	The following require quarterly visual inspections that must be done while the storage tanks are filling:  1) Tank hatches, covers, seals, pressure release valves, and closed vent systems.  2) Valves in the closed vent system and storage tank control system.	PetroShale will monitor produced oil and volume of gas sent to flares.  Quarterly visual inspections while the tanks are filling will be conducted as required.  PetroShale will inspect and monitor the flares as required.		
					Enclosed combustors, utility flares, and pit flares:	·
			Must be physically inspected each time an operator is on site (minimum quarterly).			
			<ul> <li>Must continuously monitor operational parameters that vary using malfunction alarms and remote notification systems where available.</li> </ul>			
			<ul> <li>Must monitor for visible smoke during operation each time an operator is on site (minimum quarterly).</li> </ul>			
			<ul> <li>Address any failures of the continuously burning pilot flame, automatic igniter, or improper operation of monitoring equipment.</li> </ul>			

Citation	Title	Applicability	Requirements	Compliance
200000000000000000000000000000000000000			Below is a list of records the facility is required to keep:	
			Oil production (barrels);	
			<ul> <li>Produced gas volume sent to combustor;</li> </ul>	
			<ul> <li>Volume of natural gas sent to the combustor from the storage tanks;</li> </ul>	
			<ul> <li>Well (re)completion data, including the lat/lon of the well, the date, time, &amp; duration (hours) of flowback from the well, the date, time, &amp; duration (hours) of casinghead gas venting, and reasons for venting the gas instead of capturing or combusting;</li> </ul>	
40 CFR §49.4167	Recordkeeping Requirements	Yes	<ul> <li>For each combustor/utility flare/pit flare record: operating manual, operation monitoring, deviation data (deviation operating time, date, time, length of time of deviation, corrective actions, preventative measures), records of missing pilot flame, malfunctioning automatic igniter, malfunctioning monitoring equipment, date &amp; time of occurrence, action taken, preventative measures adopted; recording data device failure, time periods that saw visible smoke emissions from the combustor/utility flare, or pit flare;</li> </ul>	PetroShale will keep the records required for each piece of applicable equipment.
			<ul> <li>For the pit flare: a log of times pit flare was operational because gas that was to be injected into pipeline was diverted. The log must note date &amp; time of flare start-up and shut-down, hours of operation due to infeasible pipeline injection from the previous 11 months thru now, and justification for each operation event;</li> </ul>	
			<ul> <li>Records of closed-vent system bypass or shutdown, reason, duration, volume of gas released, action taken, and preventative measures adopted; and</li> </ul>	
			<ul> <li>Produced water tanks and oil tanks inspection (as required by §49.4166) records, including date, findings, adjustments/repairs, name &amp; signature of inspector.</li> </ul>	
			The above records must be kept at the facility or at the location of that operates the facility on a daily basis. These records must be retained for 5 years from the date of record.	
			An annual report is due on 8/15 each year must cover all information for the previous year. The initial report must cover all information for that year.	
40 CFR §49.4168	Notification and Reporting Requirements	Yes	The annual report must contain: company name and address of oil and gas facility, identification of the production facility, reporting period beginning & ending dates, summary of all required records for each well (re)completion operation that occurred within the reporting period, first date of production for each well that began operating during the reporting period, summary of instances where well construction or operation was not in compliance with §49.4164, §49.4165, or §49.4166 for all wells at a facility, and certification of truth, accuracy, & completeness.	PetroShale will submit the required annual report with all required data by 8/15 each year.

#### **APPENDIX A**

Registration for New True Minor Oil and Natural Gas Sources and Minor Modifications at Existing True Minor Oil and Natural Gas Sources Part 2 Form



#### **United States Environmental Protection Agency**

https://www.epa.gov/tribal-air/tribal-minor-new-source-review January 4, 2017

### Part 2: Submit Within 60 Days After Startup of Production — Emission and Production Information

FEDERAL IMPLEMENTATION PLAN FOR TRUE MINOR SOURCES IN INDIAN COUNTRY IN THE OIL AND NATURAL GAS PRODUCTION AND NATURAL GAS PROCESSING SEGMENTS OF THE OIL AND NATURAL GAS SECTOR Registration for New True Minor Oil and Natural Gas Sources and Minor

Registration for New True Minor Oil and Natural Gas Sources and Minor Modifications at Existing True Minor Oil and Natural Gas Sources

#### Please submit information to:

[Reviewing Authority Address Phone] Air Program (Mail Code 8P-AR) US EPA Region 8 1595 Wynkoop St. Denver, CO 80202

#### A. GENERAL SOURCE INFORMATION (See Instructions Below)

1. Company Name		2. Source Name							
Petroshale (US), I	nc.	Primus Facility: PetroShale US 8H, US 12H, and US 13H Oil & Gas Production Facility							
3. Type of Oil and Natural Gas Crude petroleum and natura	*	4. New Minor Source? Yes No							
		5. True Source Modif	ication? Yes No						
6. NAICS Code		7. SIC Code							
211111		1311							
8. U.S. Well ID(s) or API Num	ber(s) [if applicable]								
33-053-07650, 33-0	)53-07780, 33	-053-07868							
9. Area of Indian Country	10. County	11a. Latitude	11b. Longitude						
Fort Berthold	McKenzie	47.991647	-102.740876						

#### **B. CONTACT INFORMATION (See Instructions Below)**

1. Owner Name	Title								
Petroshale (US), Inc Tony Izzo	Vice President - Engineering & Business Development								
Mailing Address									
303 East 17th Avenue, Suite 940 Denver, CO 80203									
Email Address									
izzo@petroshaleinc.com									
Telephone Number	Facsimile Number								
(403) 513-0107	(303) 484-3255								
2. Operator Name (if different from owner)	Title								
N/A	Same as Owner								
Mailing Address									
Email Address									
Telephone Number	Facsimile Number								
3. Source Contact	Title								
Lauren Morahan	Manager - Regulatory & Compliance								
Mailing Address									
303 East 17th Avenue, S	Suite 940 Denver, CO 80203								
Email Address									
morahan@petroshaleind	com								
Telephone Number	Facsimile Number								
(720) 343-8142	(303) 484-3255								

4. Compliance Contact	Title
Same as Source Contact	
Mailing Address	
Same as Source Contact	ct
Email Address	
Same as Source Contact	
Telephone Number	Facsimile Number
Same as Source Contact	

#### C. EMISSIONS AND OTHER SOURCE INFORMATION

Include all of the following information in the table below and as attachments to this form:

Note: The emission estimates can be based upon actual test data or, in the absence of such data, upon procedures acceptable to the Reviewing Authority. The following procedures are generally acceptable for estimating emissions from air pollution sources: (1) unit-specific emission tests; (2) mass balance calculations; (3) published, verifiable emission factors that are applicable to the unit (i.e., manufacturer specifications); (4) other engineering calculations; or (5) other procedures to estimate emissions specifically approved by the Reviewing Authority. Guidance for estimating emissions can be found at <a href="https://www.epa.gov/chief">https://www.epa.gov/chief</a>.

- Narrative description of the operations.
- Identification and description of any air pollution control equipment and compliance monitoring devices or activities.
- Type and actual amount (annually) of each fuel that will be used.
- Type of raw materials used (e.g., water for hydraulic fracturing).
- Actual, annual production rates.
- Actual operating schedules.
- Any existing limitations on source operations affecting emissions or any work practice standards, where applicable, for all regulated New Source Review (NSR) pollutants at your source. Indicate all requirements referenced in the Federal Implementation Plan (FIP) for True Minor Sources in Indian Country in the Oil and Natural Gas Production and Natural Gas Processing Segments of the Oil and Natural Gas Sector that apply to emissions units and air pollution generating activities at the source or proposed. Include statements indicating each emissions unit that is an emissions unit potentially subject to the requirements referenced in the FIP, but does not meet the definition of an affected facility under the referenced requirement, and therefore, is not subject to those requirements.
- For each emissions unit comprising the new source or modification, estimates of the total allowable (potential to emit) annual emissions at startup of production from the air pollution source for the following air pollutants: particulate matter, PM<sub>10</sub>, PM<sub>2.5</sub>, sulfur oxides (), nitrogen oxides (NO<sub>x</sub>), carbon monoxide (CO), volatile organic compound (VOC), lead (Pb) and lead compounds, fluorides (gaseous and particulate), sulfuric acid mist (H<sub>2</sub>SO<sub>4</sub>), hydrogen sulfide (H<sub>2</sub>S), total reduced sulfur (TRS) and reduced sulfur compounds, including all calculations for the estimates. Allowable annual emissions are defined as: emissions rate of an emissions unit calculated using the maximum capacity of a stationary source to emit a pollutant under its physical and operational design. Any physical

or operational limitation on the capacity of the source to emit a pollutant, including air pollution control equipment and restrictions on hours of operation or on the type or amount of material combusted, stored, or processed, shall be treated as part of its design if the limitation, or the effect it would have on emissions, is legally and practically enforceable. You must determine the potential for emissions within 30 days from the startup of production.

For each emissions unit comprising the new source or modification, estimates of the total actual annual emissions during the upcoming, consecutive 12 months from the air pollution source for the following air pollutants: particulate matter (PM, PM<sub>10</sub>, PM<sub>2.5</sub>), sulfur oxides (SO<sub>x</sub>), nitrogen oxides (NOx), carbon monoxide (CO), volatile organic compound (VOC), lead (Pb) and lead compounds, ammonia (NH<sub>3</sub>), fluorides (gaseous and particulate), sulfuric acid mist (H<sub>2</sub>SO<sub>4</sub>), hydrogen sulfide (H<sub>2</sub>S), total reduced sulfur (TRS) and reduced sulfur compounds, including all calculations for the estimates. Estimates of actual emissions must take into account equipment, operating conditions, and air pollution control measures. You should calculate an estimate of the actual annual emissions using estimated operating hours, production rates, in-place control equipment, and types of materials processed, stored, or combusted.

#### D. TABLE OF ESTIMATED EMISSIONS

Provide in the table below estimates of the total allowable annual emissions in tons per year (tpy) and total actual annual emissions (tpy) for the following pollutants for all emissions units comprising the new source or modification.

TOTAL ALLOWABLE ANNUAL EMISSIONS (TPY)	TOTAL ACTUAL ANNUAL EMISSIONS (TPY)
1.76	1.14
1.76	1.14
1.76	1.14
0.13	0.09
20.45	14.79
74.05	48.25
126.16	80.68
0.00	0.00
	1.76  1.76  1.76  20.45  74.05

POLLUTANT	TOTAL ALLOWABLE ANNUAL EMISSIONS (TPY)	TOTAL ACTUAL ANNUAL EMISSIONS (TPY)
NH3	0.00	0.00
Fluorides		
H <sub>2</sub> SO <sub>4</sub>	0.00	0.00
$H_2S$	0.00	0.00
TRS	0.00	0.00

#### **APPENDIX B**

**Emission Calculations** 

Table B.1. - Emission Sources

Emission Unit	Quantity	Rating/Capacity
2-Phase Separators w/Heater Treater	2	1.0 MMBtu/hr each
2-Phase Separators w/Heater Treater	1	0.5 MMBtu/hr
Crude Oil/Condensate Storage Tanks	8	400 BBL each
Crude Oil/Condensate Storage Tanks	8	1,000 BBL each
Produced Water Storage Tanks	4	400 BBL each
Produced Water Storage Tanks	4	1,000 BBL each
Flares	4	21.45 scf/hr pilot rating
Fugitive Leaks	-	-
Truck Loading	-	N/A
Compressor Engine	1	400 horsepower
Compressor Engine	1	215 horsepower
Produced Gas	-	-

Table B.2. - Summary of Uncontrolled Emissions in Pounds per Hour

Emission Source	voc	HAPs	NO <sub>x</sub>	со	SO <sub>2</sub>	H <sub>2</sub> S	PM <sub>10</sub>	PM <sub>2.5</sub>	CO₂e
2-Phase Separators w/Heater Treater	0.01	0.00	0.25	0.21	0.00	-	0.02	0.02	292.75
(16) Crude Oil/Condensate Storage Tanks	942.15	12.52	-	-	-	0.00	-	-	169.69
(8) Produced Water Storage Tanks	0.07	0.00	-	-	-	0.00	-	-	0.01
(4) Flares Pilots	-	-	-	-	-	-	-	-	-
Fugitive Leaks	1.51	0.08	-	-	-	0.00	-	-	0.19
Truck Loading	0.48	0.01	-	-	-	0.00	-	-	0.10
(2) Compressor Engines	0.23	0.16	36.41	2.07	0.00	-	0.05	0.05	576.06
Produced Gas	358.09	7.01	-	-	-	0.00	-	-	8,149.34
Total	1,302.53	19.77	36.65	2.28	0.00	0.00	0.07	0.07	9,188.15

Table B.3. - Summary of Uncontrolled Emissions in Tons Per Year

Emission Source	Voc	HAPs	NO <sub>x</sub>	co	SO <sub>2</sub>	H <sub>2</sub> S	PM <sub>10</sub>	PM <sub>2.5</sub>	CO <sub>2</sub> e
2-Phase Separators w/Heater Treater	0.06	0.02	0.25	0.21	0.00	-	0.08	0.08	1,282.22
(16) Crude Oil/Condensate Storage Tanks	4,126.64	54.82	-	-	-	0.00	-	-	743.26
(8) Produced Water Storage Tanks	0.29	0.00	-	-	-	0.00	-	_	0.06
(4) Flares Pilots	-	-	-	-	~	-	-	-	-
Fugitive Leaks	6.61	0.34	-	-	-	0.00	-	-	0.85
Truck Loading	0.37	0.01	-	-	~	0.00	-	-	0.08
(2) Compressor Engines	0.99	0.70	159.47	9.09	0.01	-	0.21	0.21	2,523.16
Produced Gas	1,568.43	30.69	-	-	-	0.00	-	-	35,694.09
Total	5,703.38	86.58	159.72	9.29	0.01	0.00	0.29	0.29	40,243.73

Table B.4. - Summary of Controlled Emissions in Pounds per Hour

Emission Source	voc	HAPs	NO <sub>X</sub>	со	SO <sub>2</sub>	H <sub>2</sub> S	PM <sub>10</sub>	PM <sub>2.5</sub>	CO <sub>2</sub> e
2-Phase Separators w/Heater Treater	0.01	0.00	0.25	0.21	0.00	-	0.02	0.02	292.75
(16) Crude Oil/Condensate Storage Tanks	18.97	0.30	1.65	7.52	0.01	0.00	0.18	0.18	2,845.84
(8) Produced Water Storage Tanks	0.00	0.00	-	-	-	0.00	-	-	0.00
(4) Flares Pilots	0.00	0.00	0.00	0.02	0.00	-	0.00	0.00	7.91
Fugitive Leaks	1.51	0.08	-	-	-	0.00	-	-	0.19
Truck Loading	0.48	0.01	-	-	-	0.00	-	-	0.10
(2) Compressor Engines	0.95	0.16	1.36	2.71	0.00	-	0.05	0.05	677.45
Produced Gas	7.27	0.18	1.41	6.45	0.01	0.00	0.16	0.16	2,608.15
Total	29.20	0.72	4.67	16.91	0.03	0.00	0.40	0.40	6,432.40

Table B.5. - Summary of Controlled Emissions in Tons Per Year

Emission Source	Voc	HAPs	NO <sub>x</sub>	со	SO <sub>2</sub>	H <sub>2</sub> S	PM <sub>10</sub>	PM <sub>2.5</sub>	CO₂e
2-Phase Separators w/Heater Treater	0.06	0.02	1.07	0.90	0.01	-	0.08	0.08	1,282.22
(16) Crude Oil/Condensate Storage Tanks	83.10	1.29	7.23	32.94	0.06	0.00	0.79	0.79	12,464.79
(8) Produced Water Storage Tanks	0.01	0.00	-	-	-	0.00	-	-	0.02
(4) Flares Pilots	0.00	0.00	0.02	0.09	0.00	-	0.00	0.00	34.65
Fugitive Leaks	6.61	0.34	-	-	_	0.00	-	-	0.85
Truck Loading	0.37	0.01	-	-	-	0.00	-	-	0.08
(2) Compressor Engines	4.16	0.70	5.94	11.88	0.01	-	0.21	0.21	2,967.25
Produced Gas	31.86	0.78	6.19	28.24	0.05	0.00	0.68	0.68	11,423.68
Total	126.16	3.14	20.45	74.05	0.13	0.00	1.76	1.76	28,173.54

Table B.6. - Summary of Uncontrolled HAP Emissions in Pounds per Hour

Hazardous Air Pollutant	Separators	Condensate Tanks	Produced Water Tanks	Flare Pilots	Fugitive Leaks	Truck Loading	Produced Gas	Compressor Engines	Total
1,1,2,2-Tetrachloroethane	-	-	-	-	-	-	-	8.3E-05	8.3E-05
1,1,2-Trichloroethane	-	-	-	-	-	-	-	5.0E-05	5.0E-05
1,3-Butadiene	-	-	-	-	-	-	-	2.2E-03	2.2E-03
1,3-Dichloropropene	-	_	-	-	-	-	-	4.2E-05	4.2E-05
2-Methylnaphthalene	5.9E-08	-	-	-	-	-	-	-	5.9E-08
2,2,4-Trimethylpentane	-	0.90	0.00	-	0.01	0.00	0.52	-	1.43
3-Methylchloranthrene	4.4E-09	-	-	-	-	-	-	-	4.4E-09
7,12-Dimethylbenz(a)anthracene	3.9E-08	-	-	-	-	-	-	-	3.9E-08
Acenaphthene	4.4E-09	-	-	-	-	-	-	-	4.4E-09
Acetaldehyde	-	-	-	-	-	-	-	9.2E-03	9.2E-03
Acrolein	-	-	-	-	-	-	-	8.7E-03	8.7E-03
Anthracene	5.9E-09	-	-	-	-	-	-	-	5.9E-09
Benzene	5.1E-06	1.10	6.6E-05	_	5.2E-03	6.0E-04	0.60	5.2E-03	1.71
Benzo(a)anthracene	4.4E-09	-	-	-	**	-	-	-	4.4E-09
Benzo(a)pyrene	2.9E-09	-	-	-	-	-	-	-	2.9E-09
Benzo(b)fluoranthene	4.4E-09	-	-	-	-	-	-	-	4.4E-09
Benzo(k)fluoranthene	4.4E-09	-	-	-	-	-	-	-	4.4E-09
Benzo(g,h,i)perylene	2.9E-09	-	-	-	-	-	-	-	2.9E-09
Carbon Tetrachloride	-	-	-	-	-	-	-	5.8E-05	5.8E-05
Chlorobenzene	-	-	-	-	-	-	-	4.2E-05	4.2E-05
Chloroform	-	-	-	-	-	-	-	4.5E-05	4.5E-05
Chrysene	4.4E-09	-	-	_	-	-	-	-	4.4E-09
Dibenz(a,h)anthracene	2.9E-09	-	-	-	-	-	-	-	2.9E-09
Dichlorobenzene	2.9E-06	-	-	-	-	-	-	-	2.9E-06
Ethylbenzene	-	7.3E-02	4.4E-06	-	3.1E-03	3.0E-04	0.04	8.2E-05	0.12
Ethylene Dibromide	-	-	-	-	-	-	-	7.0E-05	7.0E-05
Fluoranthene	7.4E-09	-	-	-	-	-	-	-	7.4E-09
Fluorene	6.9E-09	_	-	-	-	-	-	-	6.9E-09
Formaldehyde	1.8E-04	_	-	-	-	-	-	6.74E-02	6.76E-02
n-Hexane	4.4E-03	9.58	5.7E-04	-	0.03	0.00	7.01	-	16.62
Indeno(1,2,3-cd)pyrene	4.4E-09	-	-	-	~	-	-	-	4.4E-09
Methanol	-	-	-	-	-	-	-	1.0E-02	1.0E-02
Methylene Chloride	-	-	-	-	-	-	-	1.4E-04	1.4E-04
Naphthalene	1.5E-06	-	~	-	-	_	-	3.2E-04	3.2E-04
PAH	-	-	-	-	-	-	-	4.6E-04	4.6E-04
Phenanathrene	4.2E-08	-	-	-	-	-	-	-	4.2E-08
Pyrene	1.2E-08	-	-	-	-	-	-	-	1.2E-08
Styrene	-	-	-	-	-	-	-	3.9E-05	3.9E-05
Toluene	8.3E-06	0.56	3.4E-05	-	6.9E-03	4.0E-05	3.05	1.8E-03	3.62
Vinyl Chloride	-	-	-	-	-	-	-	2.4E-05	2.4E-05
Xylene		0.30	1.8E-05	-	2.2E-02	5.3E-03	0.16	6.4E-04	0.49
Total	4.61E-03	12.52	7.51E-04	0.00	0.08	0.01	11.38	0.11	24.09

Table B.7. - Summary of Controlled HAP Emissions in Pounds per Hour

Hazardous Air Pollutant	Separator	Condensate Tanks	Produced Water Tanks	Flare Pilot	Fugitive Leaks	Truck Loading	Produced Gas	Compressor Engines	Total
1,1,2,2-Tetrachloroethane	-	-	-	-	_	_	-	8.3E-05	8.3E-05
1,1,2-Trichloroethane	-	-	-	-	_	_	-	5.0E-05	5.0E-05
1,3-Butadiene	-	-	-	-	-	-	-	2.2E-03	2.2E-03
1,3-Dichloropropene	_	_	-	_	-	-	-	4.2E-05	4.2E-05
2-Methylnaphthalene	5.9E-08	-	-	1.6E-09	-	-	-	-	6.0E-08
2,2,4-Trimethylpentane	-	0.02	0.00	-	0.01	0.00	0.01	-	0.04
3-Methylchloranthrene	4.4E-09	-	-	1.2E-10	-	-	-	-	4.5E-09
7,12-Dimethylbenz(a)anthracene	3.9E-08	-	-	1.1E-09		-	-	-	4.0E-08
Acenaphthene	4.4E-09	-	-	1.2E-10	-	_	-	-	4.5E-09
Acetaldehyde	-	-	-	-	-	-	-	9.2E-03	9.2E-03
Acrolein		-	-	~	_	_	-	8.7E-03	8.7E-03
Anthracene	5.9E-09	-	-	1.6E-10	-	-	-	-	6.0E-09
Benzene	5.1E-06	2.2E-02	1.3E-06	1.4E-07	5.2E-03	6.0E-04	0.01	5.2E-03	0.05
Benzo(a)anthracene	4.4E-09	-	-	1.2E-10	-	-	-	-	4.5E-09
Benzo(b)fluoranthene	4.4E-09	-	-	1.2E-10	-	_	-	-	4.5E-09
Benzo(k)fluoranthene	4.4E-09	-	-	1.2E-10	-	-	-	-	4.5E-09
Benzo(a)pyrene	2.9E-09	-	-	7.9E-11	-	-	-	-	3.0E-09
Benzo(g,h,l)perylene	2.9E-09	-	-	7.9E-11	-	-	-	-	3.0E-09
Carbon Tetrachloride	-	-	-	-	-	-	-	5.8E-05	5.8E-05
Chlorobenzene	-	-	-	-	-	-	-	4.2E-05	4.2E-05
Chloroform	-	-	-	-	-	-	-	4.5E-05	4.5E-05
Chrysene	4.4E-09	-	-	1.2E-10	-	-	-	-	4.5E-09
Dibenz(a,h)anthracene	2.9E-09	-	-	7.9E-11	-	-	-	-	3.0E-09
Dichlorobenzene	2.9E-06	-	-	7.9E-08	-	-	-	-	3.0E-06
Ethylbenzene	-	1.5E-03	8.8E-08	-	3.1E-03	3.0E-04	8.1E-04	8.2E-05	5.8E-03
Ethylene Dibromide	-	-	-	-	-	-	-	7.0E-05	7.0E-05
Fluoranthene	7.4E-09	-	-	2.0E-10	-	-	-	-	7.6E-09
Fluorene	6.9E-09	-	-	1.9E-10	-	-	-	-	7.0E-09
Formaldehyde	1.8E-04	-	-	5.0E-06	-	-	-	6.74E-02	6.76E-02
n-Hexane	4.4E-03	0.23	1.1E-05	1.2E-04	0.03	0.00	0.18	-	0.45
Indeno(1,2,3-cd)pyrene	4.4E-09	-	-	1.2E-10	-	-	-	-	4.5E-09
Methanol	-	-	-	-	~	_	-	1.0E-02	1.0E-02
Methylene Chloride	-	-	-	-	-	-	-	1.4E-04	1.4E-04
Naphthalene	1.5E-06	-	-	4.0E-08	-	-	-	3.2E-04	3.2E-04
PAH	-	-	-	_	-	_	-	4.6E-04	4.6E-04
Phenanathrene	4.2E-08	-	-	1.1E-09	-	-	-	-	4.3E-08
Pyrene	1.2E-08	-	-	3.3E-10	-	-	-	-	1.3E-08
Styrene	-	-	-	-	-	-	-	3.9E-05	3.9E-05
Toluene	8.3E-06	1.1E-02	6.7E-07	2.3E-07	6.9E-03	4.0E-05	0.06	1.8E-03	0.08
Vinyl Chloride	-	-	-	-	-	-	-	2.4E-05	2.4E-05
Xylene	-	6.0E-03	3.6E-07	-	2.2E-02	5.3E-03	0.00	6.4E-04	0.04
Total	4.61E-03	0.29	1.50E-05	1.25E-04	0.08	0.01	0.26	0.11	0.75

Table B.8. - Summary of Uncontrolled HAP Emissions in Tons per Year

Hazardous Air Pollutant	Separator	Condensate Tanks	Produced Water Tanks	Flare Pilot	Fugitive Leaks	Truck Loading	Produced Gas	Compressor Engines	Total
1,1,2,2-Tetrachloroethane	-	-	-	-	-	-	-	3.6E-04	3.6E-04
1,1,2-Trichloroethane	-	-	-	_	-	-	_	2.2E-04	2.2E-04
1,3-Butadiene	-	-	-	-	-	-	-	9.6E-03	9.6E-03
1,3-Dichloropropene	-	-	-	-	-	-	-	1.8E-04	1.8E-04
2-Methylnaphthalene	2.6E-07	-	-	-	-	-	-	-	2.6E-07
2,2,4-Trimethylpentane	-	3.96	0.00	-	0.04	0.00	2.28	~	6.27
3-Methylchloranthrene	1.9E-08	-	-	-	-	-	-	-	1.9E-08
7,12-Dimethylbenz(a)anthracene	1.7E-07	-	-	-	-	-	-	-	1.7E-07
Acenaphthene	1.9E-08	-	-	-	-	-	-	-	1.9E-08
Acetaldehyde	-	-	-	-	-	-	-	0.04	0.04
Acrolein	-	-	-	-	-	-	-	3.8E-02	3.8E-02
Anthracene	2.6E-08	-	-	-	-	-	-	-	2.6E-08
Benzene	2.3E-05	4.83	2.9E-04	-	2.3E-02	4.6E-04	2.63	2.3E-02	7.50
Benzo(a)anthracene	1.9E-08	-	-	_	-	-	-	-	1.9E-08
Benzo(b)fluoranthene	1.9E-08	-	-	-	-	-	-	-	1.9E-08
Benzo(k)fluoranthene	1.9E-08	-	-	-	-	-	-	-	1.9E-08
Benzo(a)pyrene	1.3E-08	-	-	-	-	-	-	-	1.3E-08
Benzo(g,h,l)perylene	1.3E-08	-	-	-	-	-	_	-	1.3E-08
Carbon Tetrachloride	-	-	-		-	-	-	2.6E-04	2.6E-04
Chlorobenzene	-	-	-	-	-	-	-	1.9E-04	1.9E-04
Chloroform	-	-	-	-	-	-	-	2.0E-04	2.0E-04
Chrysene	1.9E-08	-	-	-	-	-	-	-	1.9E-08
Dibenz(a,h)anthracene	1.3E-08	-	-	-	-	-	-	-	1.3E-08
Dichlorobenzene	1.3E-05	-	-	-	-	-	-	-	1.3E-05
Ethylbenzene	-	3.2E-01	1.9E-05	-	1.4E-02	2.4E-04	0.18	3.6E-04	0.51
Ethylene Dibromide	-	-	-	-	-	-	-	3.1E-04	3.1E-04
Fluoranthene	3.2E-08	-	-	-	-	-	-	-	3.2E-08
Fluorene	3.0E-08	-	-	-	-	-	-	-	3.0E-08
Formaldehyde	8.1E-04	-	-	-	-	-	-	0.30	0.30
n-Hexane	0.02	41.94	2.5E-03	-	0.14	0.00	30.69	-	72.79
Indeno(1,2,3-cd)pyrene	1.9E-08	-	-	-	-	-	-	-	1.9E-08
Methanol	-	-	-	-	-	-	-	4.4E-02	4.4E-02
Methylene Chloride	-	-	-	-	-	-	-	5.9E-04	5.9E-04
Naphthalene	6.5E-06	-	-	-	-	-	-	1.4E-03	1.4E-03
PAH	-	-	-	_	-	-	-	2.0E-03	2.0E-03
Phenanathrene	1.8E-07	-	-		-	-	-	-	1.8E-07
Pyrene	5.4E-08	-	-	-	-	-	-	-	5.4E-08
Styrene	-	-	-	_	-	-	-	1.7E-04	1.7E-04
Toluene	3.7E-05	2.45	1.5E-04	-	3.0E-02	3.1E-05	13.37	8.0E-03	15.85
Vinyl Chloride	-	-	-	~	-	-	-	1.0E-04	1.0E-04
Xylene	-	1.32	7.9E-05	-	9.7E-02	4.2E-03	0.69	2.8E-03	2.12
Total	0.02	54.82	3.29E-03	0.00	0.34	0.01	49.83	0.47	105.48

Table B.9. - Summary of Controlled HAP Emissions in Tons per Year

Hazardous Air Pollutant	Separator	Condensate Tanks	Produced Water Tanks	Flare Pilot	Fugitive Leaks	Truck Loading	Produced Gas	Compressor Engines	Total
1,1,2,2-Tetrachloroethane		-	-		-	-		3.6E-04	3.6E-04
1,1,2-Trichloroethane	-	-	-	-	-	-	-	2.2E-04	2.2E-04
1,3-Butadiene	-	-	-	-	-	-	-	9.6E-03	9.6E-03
1,3-Dichloropropene	-	-	-	-	-	-	-	1.8E-04	1.8E-04
2-Methylnaphthalene	2.6E-07	-	-	7.0E-09	-	-	-	-	2.6E-07
2,2,4-Trimethylpentane	-	0.08	0.00	-	0.04	0.00	0.05	-	0.16
3-Methylchloranthrene	1.9E-08	-	-	5.2E-10	-	-	-	-	2.0E-08
7,12-Dimethylbenz(a)anthracene	1.7E-07	-	-	4.6E-09	-	-	-	-	1.8E-07
Acenaphthene	1.9E-08	-	-	5.2E-10	-	-	-	-	2.0E-08
Acetaldehyde	-	-	-	-	-	-	-	4.02E-02	4.02E-02
Acrolein	-	-	-	-	-	-	-	3.8E-02	3.8E-02
Anthracene	2.6E-08	-	-	7.0E-10	-	-	-	-	2.6E-08
Benzene	2.3E-05	9.7E-02	5.8E-06	6.1E-07	2.3E-02	4.6E-04	0.05	2.3E-02	0.20
Benzo(a)anthracene	1.9E-08	-	-	5.2E-10	-	-	-	-	2.0E-08
Benzo(b)fluoranthene	1.9E-08	-	-	5.2E-10	-	-	-	-	2.0E-08
Benzo(k)fluoranthene	1.9E-08	-	-	5.2E-10	-	_	-	-	2.0E-08
Benzo(a)pyrene	1.3E-08	-	-	3.5E-10	-	-	-	-	1.3E-08
Benzo(g,h,l)perylene	1.3E-08	-	-	3.5E-10	-	-	-	-	1.3E-08
Carbon Tetrachloride	-	-	-	-	-	-	-	2.6E-04	2.6E-04
Chlorobenzene	_	-	-		-	-	-	1.9E-04	1.9E-04
Chloroform	-	-	-	_	-	-	-	2.0E-04	2.0E-04
Chrysene	1.9E-08	-	-	5.2E-10	-	-	_	_	2.0E-08
Dibenz(a,h)anthracene	1.3E-08	-	_	3.5E-10	-	_	-	_	1.3E-08
Dichlorobenzene	1.3E-05	-	-	3.5E-07	-	_	-	-	1.3E-05
Ethylbenzene	-	6.4E-03	3.9E-07	-	1.4E-02	2.4E-04	3.5E-03	3.6E-04	2.4E-02
Ethylene Dibromide	-	-	-	_	-	_	_	3.1E-04	3.1E-04
Fluoranthene	3.2E-08	-	-	8.7E-10	-	-	-	-	3.3E-08
Fluorene	3.0E-08	-	-	8.1E-10	-	-	-	-	3.1E-08
Formaldehyde	8.1E-04	-	-	2.2E-05	-	_	-	0.30	0.30
n-Hexane	0.02	1.03	5.0E-05	5.2E-04	0.14	0.00	0.77	-	1.96
Indeno(1,2,3-cd)pyrene	1.9E-08	-	-	5.2E-10	-	-	-	-	2.0E-08
Methanol	-	-	-	-	-	_	-	4.4E-02	4.4E-02
Methylene Chloride	-	-	-	-	-	_	-	5.9E-04	5.9E-04
Naphthalene	6.5E-06	-	_	1.8E-07	-	_	_	1.4E-03	1.4E-03
PAH	-	-	-		-	-	-	2.0E-03	2.0E-03
Phenanathrene	1.8E-07	_	_	4.9E-09	_	_	-		1.9E-07
Pyrene	5.4E-08	-	_	1.5E-09	-	-	-	-	5.5E-08
Styrene	-	_	_	-	-	-	_	1.7E-04	1.7E-04
Toluene	3.7E-05	4.9E-02	2.9E-06	9.9E-07	3.0E-02	3.1E-05	0.27	8.0E-03	0.36
Vinyl Chloride		-	-	-	-		-	1.0E-04	1.0E-04
Xylene	-	2.6E-02	1.6E-06	-	9.7E-02	4.2E-03	0.01	2.8E-03	0.14
Total	0.02	1.28	6.58E-05	5.46E-04	0.34	0.01	1.16	0.47	3.27

#### Petroshale (US), Inc.

### Primus Facility: PetroShale US 8H, US12H, & US 13H Production Facility PTE Emission Calculations Most Recent Production Data

Table B.10.a - PetroShale US8H First 34 Days Production Data

Month	Days On	Oil Produced, BBLs	Water Produced, BBLs	Gas Produced, MSCF	Gas Flared, MCF
December 2016	3	3,421	2,926	4,373	4,373
January 2017	31	40,013	7,001	55,121	55,121
Daily Average		1,277.47	291.97	1,749.82	1,749.82
Adjusted Daily Average 1, 2		766.48	175.18	1,049.89	104.99

Note: Due to availability of monthly data in lieu of daily data the daily production average is based on the first 34 days of production.

Table B.10.b - PetroShale US12H First 30 Days of Operation Production Data

Month	Days On	Oil Produced, BBLs	Water Produced, BBLs	Gas Produced, MSCF	Gas Flared, MCF
August 2019	8	10,044	3,235	12,743	1,043
September 2019	22	25,377	N/A	30,782	N/A
Daily Average		1,180.70	404.38	1,450.83	130.38
Adjusted Daily Average 1, 2		708.42	242.63	870.50	87.05

<sup>&</sup>lt;sup>1</sup> Assuming a 40% decline in production for the first year of operation.

<sup>&</sup>lt;sup>1</sup> Assuming a 40% decline in production for the first year of operation.

<sup>&</sup>lt;sup>2</sup> As of May 11, 2018, the US8H well was connected to a gas sales pipeline. Per the most recent 12 months' production data, approximately 8.4% of the gas produced is flared due to upset conditions. The adjusted daily average estimates the PTE with the conservative assumption that 10% of the produced gas is flared.

<sup>&</sup>lt;sup>2</sup> The PetroShale US12H and US13H wells are connected to a gas sales pipeline. The adjusted daily average estimates the PTE with the conservative assumption that 10% of the produced gas is flared.

Table B.10.c - PetroShale US 13H First 44 Days Production Data

Date	Days On	Oil Produced, BBLs	Water Produced, BBLs	Gas Produced, MSCF	Gas Flared, MCF
June 2019	22	14,289	10,020	29,092	29,092
May 2019	22	28,139	15,655	68,482	64,284
Daily Average		964.27	583.52	2,217.59	2,122.18
Adjusted Daily Average 1, 2		578.56	350.11	1,330.55	133.06

Note: Due to availability of monthly data in lieu of daily data the daily production average is based on the first 44 days of production.

Table B.10.d - Daily Average Production of the Entire Primus Facility (all 3 wells)

Well	Oil Produced Per Day, BBLs	Water Produced Per Day, BBLs	Gas Produced Per Day, MSCF	Gas Flared Per Day, MCF
PetroShale US8H	766.48	175.18	1,049.89	104.99
PetroShale US12H	708.42	242.63	870.50	87.05
PetroShale US13H	578.56	350.11	1,330.55	133.06
Total Facility Daily Average <sup>1</sup>	2,053.47	767.92	3,250.95	325.09

<sup>&</sup>lt;sup>1</sup> Assuming a 40% decline in production for the first year of operation.

<sup>&</sup>lt;sup>1</sup> Assuming a 40% decline in production for the first year of operation.

 $<sup>^2</sup>$  The PetroShale US12H and US13H wells are connected to a gas sales pipeline. The adjusted daily average estimates the PTE with the conservative assumption that 10% of the produced gas is flared.

#### Petroshale (US), Inc.

### Primus Facility: PetroShale US 8H, US12H, & US 13H Production Facility PTE Emission Calculations Separator Burners

Table B.11. - Separator Burner Information

Parameter	Value
Burner Rating (each), MMBtu/hr	1.00
Number of Separator Burners	2
Burner Rating (each), MMBtu/hr	0.50
Number of Separator Burners	1
HHV, Btu/scf	1,535.40
Total Fuel Consumption, Mscf/day	39.08

Note: Fuel HHV from gas analysis dated March 6, 2017. Fuel consumption calculated using:

$$\frac{Mscf}{day} = \left[Burner\ rating, \frac{MMBtu}{hr}\right] \times \left[\frac{10^6Btu}{MMBtu}\right] \times \left[\frac{24hr}{day}\right] + \left[HHV, \frac{Btu}{scf}\right] + \left[\frac{1,000\ scf}{Mscf}\right]$$

Table B.12. - Separator Burner Criteria Pollutant Emissions

Pollutant	Emission Factor, lb/10 <sup>6</sup> scf	Emission Factor, lb/MMBtu	Emission Rate, lb/hr	Emission Rate, tpy
PM <sub>10</sub> 1	7.60	7.45E-03	0.02	0.08
PM <sub>2.5</sub> <sup>1</sup>	7.60	7.45E-03	0.02	0.08
SO₂	0.60	5.88E-04	1.47E-03	6.44E-03
NO <sub>X</sub>	100.00	0.10	0.25	1.07
со	84.00	0.08	0.21	0.90
voc	5.50	5.39E-03	0.01	0.06

Note: Based on EPA AP-42, Section 1.4, Natural Gas Combustion (Tables 1.4-1 and 1.4-2). Emission factors converted from lb/10<sup>6</sup> scf to lb/MMBtu by dividing by the average heat value of natural gas: 1,020 Btu/scf.

Table B.13. - Separator Burner Hazardous Air Pollutant Emissions

Pollutant	Emission Factor, lb/10 <sup>6</sup> scf	Emission Factor, lb/MMBtu	Emission Rate, lb/hr	Emission Rate, tpy
2-Methylnaphthalene	2.40E-05	2.35E-08	5.88E-08	2.58E-07
3-Methylchloranthrene	1.80E-06	1.76E-09	4.41E-09	1.93E-08
7,12-Dimethylbenz(a)anthracene	1.60E-05	1.57E-08	3.92E-08	1.72E-07
Acenaphthene	1.80E-06	1.76E-09	4.41E-09	1.93E-08
Anthracene	2.40E-06	2.35E-09	5.88E-09	2.58E-08
Benz(a)anthracene	1.80E-06	1.76E-09	4.41E-09	1.93E-08
Benzene	2.10E-03	2.06E-06	5.15E-06	2.25E-05
Benzo(a)pyrene	1.20E-06	1.18E-09	2.94E-09	1.29E-08
Benzo(b)fluoranthene	1.80E-06	1.76E-09	4.41E-09	1.93E-08
Benzo(g,h,i)perylene	1.20E-06	1.18E-09	2.94E-09	1.29E-08
Benzo(k)fluoranthene	1.80E-06	1.76E-09	4.41E-09	1.93E-08
Crysene	1.80E-06	1.76E-09	4.41E-09	1.93E-08
Dibenzo (a,h) anthracene	1.20E-06	1.18E-09	2.94E-09	1.29E-08
Dichlorobenzene	1.20E-03	1.18E-06	2.94E-06	1.29E-05
Fluoranthene	3.00E-06	2.94E-09	7.35E-09	3.22E-08
Fluorene	2.80E-06	2.75E-09	6.86E-09	3.01E-08
Formaldehyde	7.50E-02	7.35E-05	1.84E-04	8.05E-04
n-Hexane	1.80E+00	1.76E-03	4.41E-03	1.93E-02
Indeno(1,2,3-cd)pyrene	1.80E-06	1.76E-09	4.41E-09	1.93E-08
Naphthalene	6.10E-04	5.98E-07	1.50E-06	6.55E-06
Phenanathrene	1.70E-05	1.67E-08	4.17E-08	1.83E-07
Pyrene	5.00E-06	4.90E-09	1.23E-08	5.37E-08
Toluene	3.40E-03	3.33E-06	8.33E-06	3.65E-05
Total:			4.61E-03	0.02

Note: Based on EPA AP-42, Section 1.4, Natural Gas Combustion (Table 1.4-3). Emission factors converted from lb/10<sup>6</sup> scf to lb/MMBtu by dividing by the average heat value of natural gas: 1,020 Btu/scf.

Table B.14. - Separator Burner Greenhouse Gas Emissions

Pollutant	Emission Factor, kg/MMBtu	Emission Factor, lb/MMBtu	Emission Rate, lb/hr	Emission Rate, tpy
CO <sub>2</sub>	53.06	116.98	292.44	1,280.90
CH <sub>4</sub>	1.00E-03	2.20E-03	5.51E-03	0.02
N <sub>2</sub> O	1.00E-04	2.20E-04	5.51E-04	2.41E-03
	292.75	1,282.22		

Note: Emission factors from 40 CFR Part 98 Subpart C, Table C-1 and C-2. Converted from kilograms to pounds. Global warming potentials for CH<sub>4</sub> and N<sub>2</sub>O are 25 and 298, respectively.

 $<sup>^{1}\,\</sup>mathrm{PM}_{10}$  and  $\mathrm{PM}_{2.5}$  are assumed to equal total particulate matter.

### Primus Facility: PetroShale US 8H, US12H, & US 13H Production Facility **PTE Emission Calculations**

### **Crude Oil/Condensate Storage Tanks**

Table B.15. - Crude Oil/Condensate Storage Tank Vapor Sent to Flare Information

Parameter	Value
Tank Vapor Volume, scfm	148.92
Tank Vapor Heating Value, Btu/scf	2,715.46
Total Gas Volume per Hour, MMSCF/hr	0.00894

Note: Tank vapor volume and heating value from E&P Tanks modeling run.

Table B.16. - Crude Oil/Condensate Storage Tank Vapor Sent to Flare Criteria Pollutant Emissions

Pollutant	Emission Factor, lb/10 <sup>6</sup> scf	Emission Factor, lb/MMBtu	Emissions, lb/hr	Emissions, tpy
PM <sub>10</sub> 1	7.60	7.45E-03	0.18	0.79
PM <sub>2.5</sub> <sup>1</sup>	7.60	7.45E-03	0.18	0.79
SO <sub>2</sub>	0.60	5.88E-04	0.01	0.06
NO <sub>X</sub>	-	0.07	1.65	7.23
со	-	0.31	7.52	32.94
voc	5.50	5.39E-03	0.13	0.57

Note: Emission factors for NO<sub>x</sub> and CO from AP-42, Section 13.5, Industrial Flares, Table 13.5-1, and calculated using the equation below:

$$NO_{\chi} \ and \ CO, \frac{lb}{hr} = \left[HHV, \frac{\mathrm{Btu}}{\mathrm{scf}}\right] \times \left[\frac{\mathrm{scf}}{\mathrm{hr}}\right] \times \left[EF, \frac{\mathrm{lb}}{\mathrm{MMBtu}}\right] \times \left[\frac{\mathrm{MMBtu}}{10^{6}Btu}\right]$$
Emission factors for PM<sub>10</sub>, PM<sub>2.5</sub>, SO<sub>2</sub>, and VOC from AP-42, Section 1.4, Natural Gas Combustion, Table 1.4-2, calculated using the equation below:

$$PM_{10}, PM_{2.5}, SO_2, or\ VOC, \frac{lb}{hr} = \left[ Total\ gas\ volume, \frac{10^6\ scf}{hr} \right] \times \left[ EF, \frac{lb}{10^6\ scf} \right] \times \frac{Produced\ Gas\ heating\ value\ \left[ \frac{btu}{scf} \right]}{Average\ NG\ heating\ value\ (1,020)\ \left[ \frac{btu}{scf} \right]}$$

Table B.17. - Crude Oil/Condensate Storage Tank Vapor Sent to Flare Hazardous Air Pollutant Emissions

Pollutant	Emission Factor, lb/10 <sup>6</sup> scf	Emission Rate, lb/hr	Emission Rate, tpy
2-Methylnaphthalene	2.40E-05	5.71E-07	2.50E-06
3-Methylchloranthrene	1.80E-06	4.28E-08	1.88E-07
7,12-Dimethylbenz(a)anthracene	1.60E-05	3.81E-07	1.67E-06
Acenaphthene	1.80E-06	4.28E-08	1.88E-07
Anthracene	2.40E-06	5.71E-08	2.50E-07
Benz(a)anthracene	1.80E-06	4.28E-08	1.88E-07
Benzene	2.10E-03	5.00E-05	2.19E-04
Benzo(a)pyrene	1.20E-06	2.85E-08	1.25E-07
Benzo(b)fluoranthene	1.80E-06	4.28E-08	1.88E-07
Benzo(g,h,i)perylene	1.20E-06	2.85E-08	1.25E-07
Benzo(k)fluoranthene	1.80E-06	4.28E-08	1.88E-07
Crysene	1.80E-06	4.28E-08	1.88E-07
Dibenzo(a,h)anthracene	1.20E-06	2.85E-08	1.25E-07
Dichlorobenzene	1.20E-03	2.85E-05	1.25E-04
Fluoranthene	3.00E-06	7.14E-08	3.13E-07
Fluorene	2.80E-06	6.66E-08	2.92E-07
Formaldehyde	7.50E-02	1.78E-03	7.81E-03
n-Hexane	1.80E+00	4.28E-02	1.88E-01
Indeno(1,2,3-cd)pyrene	1.80E-06	4.28E-08	1.88E-07
Naphthalene	6.10E-04	1.45E-05	6.36E-05
Phenanathrene	1.70E-05	4.04E-07	1.77E-06
Pyrene	5.00E-06	1.19E-07	5.21E-07
Toluene	3.40E-03	8.09E-05	3.54E-04
Total:		0.04	0.20

Note: Based on EPA AP-42, Section 1.4, Natural Gas Combustion (Table 1.4-3).

Table B.18. - Crude Oil/Condensate Storage Tank Vapor Sent to Flare Greenhouse Gas Emissions

Pollutant	Emission Factor, kg/MMBtu	Emission Factor, lb/MMBtu	Emissions, lb/hr	Emissions, tpy
CO <sub>2</sub>	53.06	116.98	2,838.18	12,431.22
CH₄	1.00E-03	2.20E-03	5.35E-02	0.23
N <sub>2</sub> O	1.00E-04	2.20E-04	5.35E-03	2.34E-02
		Total CO₂e:	2,841.11	12,444.06

Note: Emission factors from 40 CFR Part 98 Subpart C, Table C-1 and C-2. Converted from kilograms to pounds. Global warming potentials for CH $_{\rm d}$  and N $_{\rm 2}$ O are 25 and 298, respectively.

## Petroshale (US), Inc. Primus Facility: PetroShale US 8H, US12H, & US 13H Production Facility PTE Emission Calculations Crude Oil/Condensate Storage Tanks

Table B.19. - E&P Tank Modeling Results and Percent Total

		Uncontrolled Emission	15	Controlled Emissions			
Parameter	E&P Tanks Model Results, tpy			E&P Tanks Model Results, tpy			
	Flashing	Working & Breathing	Total	Flashing	Working & Breathing	Total	
Total Emissions	974.62	3,813.39	4,788.01	19.49	76.27	95.76	
Emissions per Tank	60.91	238.34	299.25	1.22	4.77	5.99	
Percent of Total	20.4%	79.6%	100%	20.4%	79.6%	100%	

Note: Flashing and working & breathing losses are only provided for uncontrolled emissions in the E&P Tank model. These percentages of the total (20.4% for flashing emissions and 79.6% for working & breathing emissions) were used to estimate emissions for other pollutants (below, in Table B.20).

Table B.20. - Crude Oil/Condensate Storage Tank Emissions

		Uncontrolled Em	issions				Con	trolled Emissions				
Parameter	E&P Tanks Model Results			E&P Tan	E&P Tanks Model Results, tpy			Total Emissions		Emissions	per Tank	
	Flashing	Working & Breathing	Total, lb/hr	Total, tpy	Flashing	Working & Breathing	Total, tpy	Combustion Emissions, tpy	lb/hr	tpy	lb/hr	tpy
VOC	839.99	3,286.64	942.15	4,126.64	16.80	65.73	82.53	0.57	18.97	83.10	1.19	5.19
Total CO <sub>2</sub> e	151.29	591.96	169.69	743.26	4.22	16.51	20.73	12,444.06	2,845.84	12,464.79	177.87	779.05
CH <sub>4</sub>	6.00	23.49	6.73	29.49	0.12	0.47	0.59	0.23	0.19	0.82	0.01	0.05
CO <sub>2</sub>	1.22	4.77	1.37	5.98	1.22	4.77	5.98	12,431.22	2,839.54	12,437.20	177.47	777.33
N <sub>2</sub> O	-	-	-	-	-	-	-	0.02	5.35E-03	0.02	3.34E-04	1.46E-03
Total HAPs	11.16	43.66	12.52	54.82	0.22	0.87	1.10	0.20	0.30	1.29	0.02	0.08
Benzene	0.98	3.84	1.10	4.83	0.02	0.08	0.10	2.19E-04	0.02	0.10	1.38E-03	6.05E-03
Toluene	0.50	1.95	0.56	2.45	0.01	0.04	0.05	3.54E-04	0.01	0.05	7.05E-04	3.09E-03
Ethylbenzene	0.07	0.26	0.07	0.32	1.31E-03	5.11E-03	6.42E-03	-	1.47E-03	6.42E-03	9.16E-05	4.01E-04
Xylene	0.27	1.05	0.30	1.32	5.38E-03	0.02	0.03	-	6.03E-03	0.03	3.77E-04	1.65E-03
n-C6	8.54	33.40	9.58	41.94	0.17	0.67	0.84	0.19	0.23	1.03	0.01	0.06
2,2,4-Trimethylpentane	0.81	3.15	0.90	3.96	0.02	0.06	0.08	-	0.02	0.08	1.13E-03	4.95E-03
H <sub>2</sub> S	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-	0.00	0.00	0.00	0.00
PM <sub>10</sub>	-	-	-	-	_	-	-	0.79	0.18	0.79	0.01	0.05
PM <sub>2.5</sub>	-	-	-	-	-	-	-	0.79	0.18	0.79	0.01	0.05
SO <sub>2</sub>	-	-	-	- 1	-	-	-	0.06	0.01	0.06	8.92E-04	3.91E-03
NO <sub>X</sub>	-	-	-	-	-	-	-	7.23	1.65	7.23	0.10	0.45
со	-	-	-	-	-	-	-	32.94	7.52	32.94	0.47	2.06

Note: Uncontrolled and controlled emissions from E&P Tank model run using the oil analysis dated March 6, 2017, included in this appendix. Assumed 98% control efficiency for the flare. Flashing and working & breathing losses estimated for the pollutants above as a percentage of their total emissions (see Table B.19). For example, total uncontrolled flashing emissions was equal to 20.4% of total uncontrolled emissions. Therefore, for VOC, flashing emissions are 20.4% of total uncontrolled VOC emissions. Emissions in pounds per hour assumed to occur over 8,760 hours per year.

# Petroshale (US), Inc. Primus Facility: PetroShale US 8H, US12H, & US 13H Production Facility PTE Emission Calculations Produced Water Tanks

Table B.21. - Produced Water Tanks Emissions

Pollutant	Uncontroll	ed Emissions	Controlled Emissions		
Poliutant	lb/hr	tpy	lb/hr	tpy	
voc	0.07	0.29	1.31E-03	5.74E-03	
Total CO₂e	0.01	0.06	4.30E-03	0.02	
CH₄	4.04E-04	1.77E-03	8.08E-06	3.54E-05	
CO <sub>2</sub>	4.10E-03	0.02	4.10E-03	0.02	
Total HAPs	7.51E-04	3.29E-03	1.50E-05	6.58E-05	
Benzene	6.61E-05	2.89E-04	1.32E-06	5.79E-06	
Toluene	3.36E-05	1.47E-04	6.71E-07	2.94E-06	
Ethylbenzene	4.40E-06	1.93E-05	8.79E-08	3.85E-07	
Xylene	1.81E-05	7.92E-05	3.62E-07	1.58E-06	
n-C6	5.74E-04	2.52E-03	1.15E-05	5.03E-05	
2,2,4-Trimethylpentane	5.42E-05	2.37E-04	1.08E-06	4.75E-06	
H <sub>2</sub> S	0.00	0.00	0.00	0.00	

Note: Produced water tank emissions from EPA TANKS modeling run. Speciated HAPs are assumed to have the same proportion of emissions (HAP to VOC) as the crude oil/ condensate storage tanks. Assumed 98% control efficiency for the flare. Emissions in pounds per hour assumed to occur over 8,760 hours per year.

### Primus Facility: PetroShale US 8H, US12H, & US 13H Production Facility **PTE Emission Calculations Steffes Engineered Flare Pilot**

### Table B.22. - Steffes Engineered Flare Pilot Information

Parameter -	Value
Flare Pilot Usage, hours	8,760
Number of Flares	4
Flare Pilot Gas, scfm	0.2
Flare Pilot Gas Heating Value, Btu/scf	1,535.4
Total Gas Volume per Hour per Flare, MMSCF/hr	0.00001
Flare Control Efficiency	98%

Note: Flare pilot gas conservatively assumed and gas heating value is averaged from a produced gas analysis dated March 6, 2017.

Table B.23. - Steffes Engineered Flare Pilot Criteria Pollutant Emissions

Pollutant	Emission Factor, lb/10 <sup>6</sup> scf	Emission Factor, lb/MMBtu	Emissions, lb/hr	Emissions, tpy
PM <sub>10</sub> <sup>1</sup>	7.60	7.45E-03	5.03E-04	2.20E-03
PM <sub>2.5</sub> 1	7.60	7.45E-03	5.03E-04	2.20E-03
SO <sub>2</sub>	0.60	5.88E-04	3.97E-05	1.74E-04
$NO_{\chi}$	-	0.07	4.59E-03	2.01E-02
со	-	0.31	0.02	9.17E-02
voc	5.50	5.39E-03	3.64E-04	1.60E-03

Note: Emission factors for NO<sub>x</sub> and CO from AP-42, Section 13.5, Industrial Flares, Table 13.5-1, and calculated using the equation below:

$$NO_X \ and \ CO, \frac{lb}{hr} = \left[HHV, \frac{\text{Btu}}{\text{scf}}\right] \times \left[\frac{\text{scf}}{\text{hr}}\right] \times \left[EF, \frac{lb}{\text{MMBtu}}\right] \times \left[\frac{\text{MMBtu}}{10^6 Btu}\right]$$
 Emission factors for PM<sub>10</sub>, PM<sub>25</sub>, SO<sub>2</sub>, and VOC from AP-42, Section 1.4, Natural Gas Combustion, Table 1.4-2, calculated using the equation below:

$$PM_{10}, PM_{2.5}, SO_2, or\ VOC, \frac{lb}{hr} = \begin{bmatrix} Total\ gas\ volume, \frac{10^6\ scf}{hr} \\ \end{bmatrix} \times \begin{bmatrix} EF, \frac{lb}{10^6\ scf} \end{bmatrix} \times \frac{Produced\ Gas\ heating\ value\ \begin{bmatrix} btu\\ scf \end{bmatrix}}{Average\ NG\ heating\ value\ (1,020) \begin{bmatrix} btu\\ scf \end{bmatrix}}$$

$$^1 PM_{10} \ and\ PM_{2.5} \ are\ assumed\ to\ equal\ total\ particulate\ matter}.$$

Table B.24. - Steffes Engineered Flare Pilot Hazardous Air Pollutant Emissions

Pollutant	Emission Factor, lb/10 <sup>6</sup> scf	Emission Rate, lb/hr	Emission Rate, tpy
2-Methylnaphthalene	2.40E-05	1.59E-09	6.96E-09
3-Methylchloranthrene	1.80E-06	1.19E-10	5.22E-10
7,12-Dimethylbenz(a) anthracene	1.60E-05	1.06E-09	4.64E-09
Acenaphthene	1.80E-06	1.19E-10	5.22E-10
Anthracene	2.40E-06	1.59E-10	6.96E-10
Benz(a)anthracene	1.80E-06	1.19E-10	5.22E-10
Benzene	2.10E-03	1.39E-07	6.09E-07
Benzo(a)pyrene	1.20E-06	7.95E-11	3.48E-10
Benzo(b)fluoranthene	1.80E-06	1.19E-10	5.22E-10
Benzo(g,h,i)perylene	1.20E-06	7.95E-11	3.48E-10
Benzo(k)fluoranthene	1.80E-06	1.19E-10	5.22E-10
Crysene	1.80E-06	1.19E-10	5.22E-10
Dibenzo(a,h)anthracene	1.20E-06	7.95E-11	3.48E-10
Dichlorobenzene	1.20E-03	7.95E-08	3.48E-07
Fluoranthene	3.00E-06	1.99E-10	8.70E-10
Fluorene	2.80E-06	1.85E-10	8.12E-10
Formaldehyde	7.50E-02	4.97E-06	2.18E-05
n-Hexane	1.80E+00	1.19E-04	5.22E-04
Indeno(1,2,3-cd)pyrene	1.80E-06	1.19E-10	5.22E-10
Naphthalene	6.10E-04	4.04E-08	1.77E-07
Phenanathrene	1.70E-05	1.13E-09	4.93E-09
Pyrene	5.00E-06	3.31E-10	1.45E-09
Toluene	3.40E-03	2.25E-07	9.86E-07
Total:		1.25E-04	5.46E-04

Note: Based on EPA AP-42, Section 1.4, Natural Gas Combustion (Table 1.4-3).

Table B.25. - Steffes Engineered Flare Pilot Greenhouse Gas Emissions

Pollutant	Emission Factor, kg/MMBtu	Emission Factor, lb/MMBtu	Emissions, lb/hr	Emissions, tpy
CO <sub>2</sub>	53.06	116.98	7.90	34.61
CH₄	1.00E-03	2.20E-03	1.49E-04	6.52E-04
N₂O	1.00E-04	2.20E-04	1.49E-05	6.52E-05
		Total CO₂e:	7.91	34.65

Note: Emission factors from 40 CFR Part 98 Subpart C, Table C-1 and C-2. Converted from kilograms to pounds. Global warming potentials for CH<sub>4</sub> and N<sub>2</sub>O are 25 and 298,

## Petroshale (US), Inc. Primus Facility: PetroShale US 8H, US12H, & US 13H Production Facility PTE Emission Calculations Fugitive Leaks

Table B.26. - Fugitive Emissions: Emission Factors for Total Hydrocarbon (THC) Emissions

Equipment Type	Equipment Service Category, lb/hr/source					
	Gas	Heavy Oil (< 20° API)	Light Oil (>20° API)	Water/Light Oil		
Valves	9.92E-03	1.85E-05	5.51E-03	2.16E-04		
Pump Seals	5.29E-03	-	2.87E-02	5.29E-05		
Others	1.94E-02	7.05E-05	1.65E-02	3.09E-02		
Connectors	4.41E-04	1.65E-05	4.63E-04	2.43E-04		
Flanges	8.60E-04	8.60E-07	2.43E-04	6.39E-06		
Open-Ended Lines	4.41E-03	3.09E-04	3.09E-03	5.51E-04		

Note: From US EPA Protocol for Equipment Leak Emission Estimates (EPA-453/R-95-017). Emission factors converted from kg/source-hr to lb/source-hr The water/light oil emission factors apply to water streams in light oil service with water content between 50% and 99%. For streams with water content > 99%, the emission rate is considered negligible. The "other" equipment type includes compressor, pressure relief valves, diaphragms, drains, dump arms, hatches, instruments, meters, polished rods, and vents.

**Table B.27. - Fugitive THC Emissions** 

Equipment Type	Number of Components	Service	Emission Factor, lb/hr/source	THC Emissions, lb/hr	THC Emissions, tpy
Valves	78	Gas	9.92E-03	0.77	3.39
Valves	78	Light Oil	5.51E-03	0.43	1.88
Valves	8	Water/Light Oil	2.16E-04	1.73E-03	0.01
Pump Seals	0	Gas	5.29E-03	0.00	0.00
Pump Seals	0	Light Oil	2.87E-02	0.00	0.00
Pump Seals	0	Water/Light Oil	5.29E-05	0.00	0.00
Others	0	Gas	1.94E-02	0.00	0.00
Others	0	Light Oil	1.65E-02	0.00	0.00
Others	0	Water/Light Oil	3.09E-02	0.00	0.00
Connectors	672	Gas	4.41E-04	0.30	1.30
Connectors	354	Light Oil	4.63E-04	0.16	0.72
Connectors	52	Water/Light Oil	2.43E-04	0.01	0.06
Flanges	4	Gas	8.60E-04	3.44E-03	0.02
Flanges	0	Light Oil	2.43E-04	0.00	0.00
Flanges	0	Water/Light Oil	6.39E-06	0.00	0.00
Open-Ended Lines	0	Gas	4.41E-03	0.00	0.00
Open-Ended Lines	0	Light Oil	3.09E-03	0.00	0.00
Open-Ended Lines	0	Water/Light Oil	5.51E-04	0.00	0.00
***************************************	***************************************		Total THC Emissions:	1.68	7.38

Note: Number of components estimated from actual counts performed at similar facilities.

**Table B.28. - Speciated Fugitive Emission Factors** 

Pollutant -	Weight Fraction	Weight Fraction	Weight Fraction	Emissions, lb/hr	Facilities &
Poliutant	Gas	Light Oil	Water/Light Oil	EIMSSIONS, ID/IN	Emissions, tpy
THC	1.00	1.00	1.00	1.68	7.37
voc	0.84	1.00	1.00	1.51	6.61
Total CO₂e	-	-		0.19	0.85
CH <sub>4</sub>	7.20E-03	0.00	0.00	0.01	0.03
CO <sub>2</sub>	1.46E-03	0.00	0.00	1.57E-03	0.01
Total HAPs	1.23E-02	0.11	0.11	0.08	0.34
Benzene	1.05E-03	6.64E-03	6.64E-03	0.01	0.02
Toluene	7.08E-05	1.12E-02	1.12E-02	0.01	0.03
Ethylbenzene	5.35E-04	4.16E-03	4.16E-03	3.10E-03	0.01
Xylenes	9.43E-03	1.99E-02	1.99E-02	0.02	0.10
n-Hexane	2.76E-04	5.14E-02	5.14E-02	0.03	0.14
2,2,4-Trimethylpentane	9.12E-04	1.18E-02	1.18E-02	0.01	0.04
H <sub>2</sub> S	0.00	0.00	0.00	0.00	0.00

Note: Water/Light Oil and Light Oil Weight fractions based on E&P Tank modeling run flashed gas results for the oil storage tanks. All stream weight fractions for organic compounds used in calculations are normalized based on 100% THC since EPA emission factors are based on THC emission rate. Produced gas speciated HAPs are proportionally based on the speciated HAPs in the E&P TANK v2.0 flashed gas results, then normalized based on 100% THC.

# Petroshale (US), Inc. Primus Facility: PetroShale US 8H, US12H, & US 13H Production Facility PTE Emission Calculations Truck Loading

Table B.29. - Truck Loading Emissions Calculation Inputs - Produced Water Only

Parameter	Value
Saturation Factor (S)	0.6
True Vapor Pressure of Liquid Loaded (P), psia	0.24
Molecular Weight of Vapors (M), lb/lb-mole	20.68
Temperature of Bulk Liquid Loaded (T), °F	41.45
Loading Losses, lb/1,000 gallons	0.08
Water Production, BPD	767.9
Average Water Loadout Rate, gallons/hr	1,343.9
Maximum Water Loadout Rate, gallons/hr	7,560.0
Maximum Yearly Throughput, gallons/yr	11,772,229

Note: Loading losses based on EPA AP-42 Section 5.2-4:

$$L_L = 12.46 \frac{SPM}{(T + 460)}$$

Saturation factor based on submerged loading: dedicated normal service. Molecular weight of vapors and liquid bulk temperature from EPA Tank run. TVP of liquid loaded is assumed to be the maximum vapor pressure from hottest month (July) to be conservative.

Table B.30. - Truck Loading Emissions in Tons Per Year

Dallistant	Mariaha Farasian	Produced V	Vater Loading
Pollutant	Weight Fraction	lb/hr	tpy
THC	1.00	0.57	0.44
voc	0.84	0.48	0.37
Total CO₂e	-	0.10	0.08
CH <sub>4</sub>	7.20E-03	4.08E-03	3.18E-03
CO <sub>2</sub>	1.46E-03	8.28E-04	6.44E-04
Total HAPs	1.23E-02	0.01	5.42E-03
Benzene	1.05E-03	5.97E-04	4.65E-04
Toluene	7.08E-05	4.02E-05	3.13E-05
Ethylbenzene	5.35E-04	3.03E-04	2.36E-04
Xylenes	9.43E-03	0.01	4.16E-03
n-Hexane	2.76E-04	1.57E-04	1.22E-04
2,2,4-Trimethylpentane	9.12E-04	5.17E-04	4.03E-04
H <sub>2</sub> S	0.00	0.00	0.00

Note: Weight fractions based on E&P Tank modeling run working and breathing gas composition for the crude oil/condensate storage tanks, which is included in this appendix. Truck loading emissions in lb/hr use maximum loadout rate. Note that crude oil/condensate is removed from site via pipeline so no loading emissions for crude oil/condensate are calculated.

## Petroshale (US), Inc. Primus Facility: PetroShale US 8H, US12H, & US 13H Production Facility PTE Emission Calculations Compressor Engine 1

Table B.31. - Engine Information

Parameter	Value
Engine #1 Horsepower (hp)	400
Number of Units	1
Fuel	Natural Gas
Annual Hours of Operation per Unit (hr)	8,760
Fuel Heat Rating (Btu/hr) <sup>1</sup>	3,290,000
Maximum Heat Input (MMBtu/hr)	3.29
Fuel Specific HHV (Btu/scf)	1,020
Fuel Use Rate (scf/hr)	3,225.49
Annual Fuel Consumption (MMBtu/year)	28,820.40
Annual Fuel Consumption (MMSCF/year)	28.26

<sup>&</sup>lt;sup>1</sup> Values from engine manufacturer's specifications.

Table B.32. - Uncontrolled Compressor Engine Emissions

A	Uncontrolled Emi	ssion Factor 1	Uncontrolled E	Uncontrolled Emission Rate	
Component	lb/MMBtu	g/bhp-hr	lb/hr	tons/year	
NO <sub>X</sub>	-	26.27	23.17	101.47	
со	-	1.60	1.41	6.18	
VOCs	-	0.16	0.14	0.62	
Formaldehyde	2.05E-02	-	6.74E-02	0.30	
PM <sub>2.5</sub>	9.50E-03	-	3.13E-02	0.14	
PM <sub>10</sub>	9.50E-03	-	3.13E-02	0.14	
PM	9.10E-03	-	2.99E-02	0.13	
SO <sub>2</sub>	5.88E-04	-	1.93E-03	0.01	
CH <sub>4</sub>	0.23	-	0.76	3.31	
N <sub>2</sub> O	1.32E-03	-	4.35E-03	0.02	
CO <sub>2</sub>	110.00	-	361.90	1,585.12	
CO₂e ²	110.00	-	382.11	1,673.66	

<sup>&</sup>lt;sup>1</sup> The emission factors for CO, NOx, and VOC are based on the manufacturer's specifications. All other emission factors from AP-42 Chapter 3 Section 2, Table 3.2-3.

Table B.33. - Controlled Compressor Engine Emissions

	Controlled En	nission Factor <sup>1</sup>	Controlled E	mission Rate
Component	lb/MMBtu	g/bhp-hr	lb/hr	tons/year
NO <sub>X</sub>	-	1.00	0.88	3.86
со	-	2.00	1.76	7.72
VOCs	-	0.70	0.62	2.70
Formaldehyde	2.05E-02	-	6.74E-02	0.30
PM <sub>2.5</sub>	9.50E-03	-	3.13E-02	0.14
PM <sub>10</sub>	9.50E-03	-	3.13E-02	0.14
PM	9.10E-03	-	2.99E-02	0.13
SO <sub>2</sub>	5.88E-04	-	1.93E-03	0.01
CH <sub>4</sub>	0.23	-	0.76	3.31
N <sub>2</sub> O	1.32E-03	-	4.35E-03	0.02
CO <sub>2</sub>	-	459.00	404.77	1,772.89
CO₂e ²	-	-	424.98	1,861.43

 $<sup>^{1}</sup>$  The emission factors for CO, NOx, and VOC are based on the gram per brake-horsepower-hour (g/bhp-hr) uncontrolled rates. Engines would meet the emission standards of NSPS JJJJ for Non-Emergency Natural Gas Engines. The emission factor  $CO_2$  is based on the manufacturer's specifications. All other emission factors from AP-42 Chapter 3 Section 2, Table 3.2-3.

### Primus Facility: PetroShale US 8H, US12H, & US 13H Production Facility

### **PTE Emission Calculations**

### **Compressor Engine 1**

 $^2$  Global warming potentials obtained from Table A-1 to Subpart 98 - Global Warming Potentials Equation

A-1: CO₂e = ∑GHGi x GWPi

Where:

CO<sub>2</sub>e = Carbon dioxide equivalent (tons/year) GHGi = Mass emissions of each GHG (tons/year)

GWPi = Global warming potential for each GHG (1 for CO<sub>2</sub>; 25 for CH<sub>4</sub>; 298 for N<sub>2</sub>O)

 $^2$  Global warming potentials obtained from Table A-1 to Subpart 98 - Global Warming Potentials

Equation A-1:  $CO_2e = \sum GHGi \times GWPi$ 

Where:

CO<sub>2</sub>e = Carbon dioxide equivalent (tons/year) GHGi = Mass emissions of each GHG (tons/year)

GWPi = Global warming potential for each GHG (1 for CO<sub>2</sub>; 25 for CH<sub>4</sub>; 298 for N<sub>2</sub>O)

Table B.34. - Compressor Engine HAP Emissions

~	AP-42 Emission Factor 1	Uncontrolled	f Emission Rate	Controlled E	mission Rate
Component	lb/MMBtu	lb/hr	tons/year	lb/hr	tons/year
1,1,2,2-Tetrachloroethane	2.53E-05	8.32E-05	3.65E-04	8.32E-05	3.65E-04
1,1,2-Trichloroethane	1.53E-05	5.03E-05	2.20E-04	5.03E-05	2.20E-04
1,3-Butadiene	6.63E-04	2.18E-03	9.55E-03	2.18E-03	9.55E-03
1,3-Dichloropropene	1.27E-05	4.18E-05	1.83E-04	4.18E-05	1.83E-04
Acetaldehyde	2.79E-03	9.18E-03	4.02E-02	9.18E-03	4.02E-02
Acrolein	2.63E-03	8.65E-03	3.79E-02	8.65E-03	3.79E-02
Benzene	1.58E-03	5.20E-03	2.28E-02	5.20E-03	2.28E-02
Carbon Tetrachloride	1.77E-05	5.82E-05	2.55E-04	5.82E-05	2.55E-04
Chlorobenzene	1.29E-05	4.24E-05	1.86E-04	4.24E-05	1.86E-04
Chloroform	1.37E-05	4.51E-05	1.97E-04	4.51E-05	1.97E-04
Ethylbenzene	2.48E-05	8.16E-05	3.57E-04	8.16E-05	3.57E-04
Ethylene Dibromide	2.13E-05	7.01E-05	3.07E-04	7.01E-05	3.07E-04
Methanol	3.06E-03	1.01E-02	4.41E-02	1.01E-02	4.41E-02
Methylene Chloride	4.12E-05	1.36E-04	5.94E-04	1.36E-04	5.94E-04
Naphthalene	9.71E-05	3.19E-04	1.40E-03	3.19E-04	1.40E-03
PAH	1.41E-04	4.64E-04	2.03E-03	4.64E-04	2.03E-03
Styrene	1.19E-05	3.92E-05	1.71E-04	3.92E-05	1.71E-04
Toluene	5.58E-04	1.84E-03	8.04E-03	1.84E-03	8.04E-03
Vinyl Chloride	7.18E-06	2.36E-05	1.03E-04	2.36E-05	1.03E-04
Xylene	1.95E-04	6.42E-04	2.81E-03	6.42E-04	2.81E-03
Total HAPs <sup>2</sup>	3.24E-02	0.11	0.47	0.11	0.47

<sup>&</sup>lt;sup>1</sup> Emission factors from AP-42 Chapter 3 Section 2, Table 3.2-3.

<sup>&</sup>lt;sup>2</sup> Total HAPs emissions include formaldehyde emissions from Tables B.32 and B.33.

## Petroshale (US), Inc. Primus Facility: PetroShale US 8H, US12H, & US 13H Production Facility PTE Emission Calculations Compressor Engine 2

**Table B.35. - Engine Information** 

Parameter	Value
Engine #2 Horsepower (hp)	215
Number of Units	1
Fuel	Natural Gas
Annual Hours of Operation per Unit (hr)	8,760
Fuel Heat Rating (Btu/hr) <sup>1</sup>	1,669,905
Maximum Heat Input (MMBtu/hr)	1.67
Fuel Specific HHV (Btu/scf)	1,020
Fuel Use Rate (scf/hr)	1,637.16
Annual Fuel Consumption (MMBtu/year)	14,628.37
Annual Fuel Consumption (MMSCF/year)	14.34

<sup>&</sup>lt;sup>1</sup> Values from engine manufacturer's specifications.

**Table B.36. - Uncontrolled Compressor Engine Emissions** 

Component	AP-42 Emissio	on Factor <sup>1</sup> g/bhp-hr	Uncontrolled Er	mission Rate tons/year
NO <sub>X</sub>	-	27.94	13.24	58.01
со	-	1.40	0.66	2.91
VOCs	-	0.18	0.09	0.37
Formaldehyde	2.05E-02	-	3.42E-02	0.15
PM <sub>2.5</sub>	0.0095	-	1.59E-02	0.07
PM <sub>10</sub>	0.0095	-	1.59E-02	0.07
PM	0.0091	-	1.52E-02	0.07
SO <sub>2</sub>	0.000588	-	9.82E-04	4.30E-03
CH <sub>4</sub>	0.23	-	0.38	1.68
N <sub>2</sub> O	1.32E-03	-	2.21E-03	0.01
CO <sub>2</sub>	110.00	-	183.69	804.56
CO₂e <sup>2</sup>	110.00		193.95	849.50

<sup>&</sup>lt;sup>1</sup> The emission factors for CO, NOx, and VOC are based on the manufacturer's specifications. All other emission factors from AP-42 Chapter 3 Section 2, Table 3.2-3.

Table B.37. - Controlled Compressor Engine Emissions

	Controlled En	nission Factor <sup>1</sup>	Controlled E	Emission Rate
Component	lb/MMBtu	g/bhp-hr	lb/hr	tons/year
NO <sub>x</sub>	-	1.00	0.47	2.08
со	-	2.00	0.95	4.15
VOCs	-	0.70	0.33	1.45
Formaldehyde	2.05E-02	-	3.42E-02	0.15
PM <sub>2.5</sub>	9.50E-03	-	1.59E-02	0.07
PM <sub>10</sub>	9.50E-03	-	1.59E-02	0.07
PM	9.10E-03	-	1.52E-02	0.07
SO <sub>2</sub>	5.88E-04	-	9.82E-04	4.30E-03
CH <sub>4</sub>	0.23	-	0.38	1.68
N <sub>2</sub> O	1.32E-03	-	2.21E-03	0.01
CO <sub>2</sub>	-	511.00	242.21	1,060.88
CO₂e ²	-	511.00	252.47	1,105.82

 $<sup>^{1}</sup>$  The emission factors for CO, NOx, and VOC are based on the gram per brake-horsepower-hour (g/bhp-hr) uncontrolled rates. Engines would meet the emission standards of NSPS JJJJ for Non-Emergency Natural Gas Engines. The emission factor CO<sub>2</sub> is based on the manufacturer's specifications. All other emission factors from AP-42 Chapter 3 Section 2, Table 3.2-3.

### Primus Facility: PetroShale US 8H, US12H, & US 13H Production Facility

### **PTE Emission Calculations**

### **Compressor Engine 2**

 $^2$  Global warming potentials obtained from Table A-1 to Subpart 98 - Global Warming Potentials Equation

A-1: CO₂e = ∑GHGi x GWPi

Where:

CO<sub>2</sub>e = Carbon dioxide equivalent (tons/year) GHGi = Mass emissions of each GHG (tons/year)

GWPi = Global warming potential for each GHG (1 for CO<sub>2</sub>; 25 for CH<sub>4</sub>; 298 for N<sub>2</sub>O)

 $^{2}$  Global warming potentials obtained from Table A-1 to Subpart 98 - Global Warming Potentials

Equation A-1: CO<sub>2</sub>e = ∑GHGi x GWPi

Where:

CO<sub>2</sub>e = Carbon dioxide equivalent (tons/year) GHGi = Mass emissions of each GHG (tons/year)

GWPi = Global warming potential for each GHG (1 for CO<sub>2</sub>; 25 for CH<sub>4</sub>; 298 for N<sub>2</sub>O)

Table B.38. - Compressor Engine HAP Emissions

C	AP-42 Emission Factor 1	Uncontrolled	l Emission Rate	Controlled E	mission Rate
Component	lb/MMBtu	lb/hr	tons/year	lb/hr	tons/year
1,1,2,2-Tetrachloroethane	2.53E-05	4.22E-05	1.85E-04	4.22E-05	1.85E-04
1,1,2-Trichloroethane	1.53E-05	2.55E-05	1.12E-04	2.55E-05	1.12E-04
1,3-Butadiene	6.63E-04	1.11E-03	4.85E-03	1.11E-03	4.85E-03
1,3-Dichloropropene	1.27E-05	2.12E-05	9.29E-05	2.12E-05	9.29E-05
Acetaldehyde	2.79E-03	4.66E-03	2.04E-02	4.66E-03	2.04E-02
Acrolein	2.63E-03	4.39E-03	1.92E-02	4.39E-03	1.92E-02
Benzene	1.58E-03	2.64E-03	1.16E-02	2.64E-03	1.16E-02
Carbon Tetrachloride	1.77E-05	2.96E-05	1.29E-04	2.96E-05	1.29E-04
Chlorobenzene	1.29E-05	2.15E-05	9.44E-05	2.15E-05	9.44E-05
Chloroform	1.37E-05	2.29E-05	1.00E-04	2.29E-05	1.00E-04
Ethylbenzene	2.48E-05	4.14E-05	1.81E-04	4.14E-05	1.81E-04
Ethylene Dibromide	2.13E-05	3.56E-05	1.56E-04	3.56E-05	1.56E-04
Methanol	3.06E-03	5.11E-03	2.24E-02	5.11E-03	2.24E-02
Methylene Chloride	4.12E-05	6.88E-05	3.01E-04	6.88E-05	3.01E-04
Naphthalene	9.71E-05	1.62E-04	7.10E-04	1.62E-04	7.10E-04
PAH	1.41E-04	2.35E-04	1.03E-03	2.35E-04	1.03E-03
Styrene	1.19E-05	1.99E-05	8.70E-05	1.99E-05	8.70E-05
Toluene	5.58E-04	9.32E-04	4.08E-03	9.32E-04	4.08E-03
Vinyl Chloride	7.18E-06	1.20E-05	5.25E-05	1.20E-05	5.25E-05
Xylene	1.95E-04	3.26E-04	1.43E-03	3.26E-04	1.43E-03
Total HAPs <sup>2</sup>	3.24E-02	5.41E-02	0.24	5.41E-02	0.24

<sup>&</sup>lt;sup>1</sup> Emission factors from AP-42 Chapter 3 Section 2, Table 3.2-3.

<sup>&</sup>lt;sup>2</sup> Total HAPs emissions include formaldehyde emissions from Tables B.36 and B.37.

### Primus Facility: PetroShale US 8H, US12H, & US 13H Production Facility **PTE Emission Calculations Produced Gas**

Table B.39. - Produced Gas Sent to Flare Information

Parameter	Value
Produced Gas Volume, MCFD	325.09
Produced Gas Volume, scf/hr	13,545.62
Produced Gas Heating Value, Btu/scf	1,535.40
Total Gas Volume per Hour, 10 <sup>6</sup> scf/hr	0.01

Note: The wells are connected to a gas sales pipeline. The flared gas volumes for the US12H and US13H wells are based on the percentage of gas flared for the US8H well. Heating value based on gas analysis dated March 6, 2017 (included in this appendix).

Table B.40. - Produced Gas Sent to Flare Criteria Pollutant Emissions

Pollutant	Emission Factor, lb/10 <sup>6</sup> scf	Emission Factor, Ib/MMBtu	Emissions, lb/hr	Emissions, tpy
PM <sub>10</sub> 1	7.60	7.451E-03	0.15	0.68
PM <sub>2.5</sub> 1	7.60	7.451E-03	0.15	0.68
SO <sub>2</sub>	0.60	5.882E-04	0.01	0.05
NOχ	-	0.07	1.41	6.19
со	-	0.31	6.45	28.24
voc	5.50	5.392E-03	0.11	0.49

Note: SO, and VOC emissions are calculated using fuel in Table B.36. Emission factors for NOX and CO from AP-42, Section 13.5, Industrial Flares, Table 13.5-1, and calculated using the equation below:

$$NO_{x} \ and \ CO, \\ \frac{lb}{hr} = \left[HHV, \\ \frac{\text{Btu}}{\text{scf}}\right] \times \left[\frac{\text{scf}}{\text{hr}}\right] \times \left[EF, \\ \frac{lb}{\text{MMBtu}}\right] \times \left[\frac{\text{MMBtu}}{10^{6}Btu}\right]$$
 Emission factors for PM<sub>10</sub>, PM<sub>2.5</sub>, VOC, and SO<sub>2</sub> from AP-42, Section 1.4, Natural Gas Combustion, Table 1.4-2, calculated using the equation below:

$$PM_{10}, PM_{2.5}, \frac{lb}{hr} = \begin{bmatrix} Total\ gas\ volume, \frac{10^6\ scf}{hr} \end{bmatrix} \times \begin{bmatrix} EF, \frac{lb}{10^6\ scf} \end{bmatrix} \times \frac{Produced\ Gas\ heating\ value\ \left[\frac{btu}{scf}\right]}{Average\ NG\ heating\ value\ (1,020)} \begin{bmatrix} \frac{btu}{scf} \end{bmatrix}$$

$$^{1}\text{PM}_{10} \text{ and PM}_{25} \text{ are assumed to equal\ total\ particulate\ matter.}$$

Table B.41. - Produced Gas Sent to Flare Hazardous Air Pollutant Emissions

Pollutant	Emission Factor, lb/10 <sup>6</sup> scf	Emission Rate, lb/hr	Emission Rate, tpy
2-Methylnaphthalene	2.40E-05	4.89E-07	2.14E-06
3-Methylchloranthrene	1.80E-06	3.67E-08	1.61E-07
7,12-Dimethylbenz(a)anthracene	1.60E-05	3.26E-07	1.43E-06
Acenaphthene	1.80E-06	3.67E-08	1.61E-07
Anthracene	2.40E-06	4.89E-08	2.14E-07
Benz(a)anthracene	1.80E-06	3.67E-08	1.61E-07
Benzene	2.10E-03	4.28E-05	1.88E-04
Benzo(a)pyrene	1.20E-06	2.45E-08	1.07E-07
Benzo(b)fluoranthene	1.80E-06	3.67E-08	1.61E-07
Benzo(g,h,i)perylene	1.20E-06	2.45E-08	1.07E-07
Benzo(k)fluoranthene	1.80E-06	3.67E-08	1.61E-07
Crysene	1.80E-06	3.67E-08	1.61E-07
Dibenzo(a,h)anthracene	1.20E-06	2.45E-08	1.07E-07
Dichlorobenzene	1.20E-03	2.45E-05	1.07E-04
Fluoranthene	3.00E-06	6.12E-08	2.68E-07
Fluorene	2.80E-06	5.71E-08	2.50E-07
Formaldehyde	7.50E-02	1.53E-03	6.70E-03
n-Hexane	1.80E+00	3.67E-02	1.61E-01
indeno(1,2,3-cd)pyrene	1.80E-06	3.67E-08	1.61E-07
Naphthalene	6.10E-04	1.24E-05	5.45E-05
Phenanathrene	1.70E-05	3.47E-07	1.52E-06
Pyrene	5.00E-06	1.02E-07	4.47E-07
Toluene	3.40E-03	6.93E-05	3.04E-04
Total:		0.04	0.17

Note: Based on EPA AP-42, Section 1.4, Natural Gas Combustion (Table 1.4-3).

Table B.42. - Produced Gas Sent to Flare Greenhouse Gas Emissions

Pollutant	Emission Factor, kg/MMBtu	Emission Factor, lb/MMBtu	Emissions, lb/hr	Emissions, tpy
CO₂	53.06	116.98	2,432.89	10,656.04
CH₄	1.00E-03	2.20E-03	0.05	0.20
N <sub>2</sub> O	1.00E-04	2.20E-04	0.00	0.02
		Total CO₂e:	2,435.40	10,667.05

Note: Emission factors from 40 CFR Part 98 Subpart C, Table C-1 and C-2. Converted from kilograms to pounds. Global warming potentials for CH<sub>4</sub> and N<sub>2</sub>O are 25 and 298, respectively.

## Petroshale (US), Inc. Primus Facility: PetroShale US 8H, US12H, & US 13H Production Facility PTE Emission Calculations Produced Gas

Table B.43. - Flare and Produced Gas Information

Parameter	Value
Flare Destruction Efficiency, %	98
Specific Gravity of Produced Gas	0.92
Molecular Weight of Produced Gas, lb/lb-mole	26.53
HHV of Produced Gas, Btu/scf	1,535.40
Volume of Produced Gas to Flare, MCFD	325.09
Volume of Produced Gas to Flare, scf/hr	13,545.62

Note: Heating value based on gas analysis dated March 6, 2017 (included in this appendix). Molecular weight of gas calculated by multiplying the specific gravity by the molecular weight of air (28.96443 lb/lb-mole).

Table B.44. - Uncontrolled and Controlled Produced Gas Emissions

	Gas Ana	lysis Data	Uncor	itrolled	Cont	rolled	Calculated	Total Contro	led Emissions
Pollutant	Weight Percent	Mole Percent	lb/hr	tpy	lb/hr	tpy	Combustion Emissions, tpy	lb/hr	tpy
voc	37.76	-	358.09	1,568.43	7.16	31.37	0.49	7.27	31.86
Total CO₂e	-	-	8,149.34	35,694.09	172.75	756.64	10,667.05	2,608.15	11,423.68
CH <sub>4</sub>	34.33	-	325.57	1,426.02	6.51	28.52	0.20	6.56	28.72
CO <sub>2</sub>	1.05	-	9.96	43.63	9.96	43.63	10,656.04	2,442.85	10,699.67
N <sub>2</sub> O	-	-	-	-	-	-	0.02	4.59E-03	0.02
Total HAPs	0.74	-	7.01	30.69	0.14	0.61	0.17	0.18	0.78
Benzene	0.06	-	0.60	2.63	0.01	0.05	1.88E-04	0.01	0.05
Toluene	0.32	-	3.05	13.37	0.06	0.27	3.04E-04	0.06	0.27
Ethylbenzene	4.26E-03	-	0.04	0.18	8.08E-04	3.54E-03	-	8.08E-04	3.54E-03
Xylene	0.02	-	0.16	0.69	3.15E-03	0.01	-	3.15E-03	0.01
n-C6	0.74	-	7.01	30.69	0.14	0.61	0.16	0.18	0.77
2,2,4-Trimethylpentane	0.05	-	0.52	2.28	0.01	0.05	-	0.01	0.05
H <sub>2</sub> S	0.00	_	0.00	0.00	0.00	0.00	0.00	0.00	0.00
PM <sub>10</sub>	-	-	-	-			0.68	0.16	0.68
PM <sub>2.5</sub>	-	-	-	-			0.68	0.16	0.68
SO₂	-	_	-	_			0.05	0.01	0.05
NO <sub>X</sub>	-	-	-	-			6.19	1.41	6.19
Note: Speciated HADs are present in pully because	-	-	-	-			28.24	6.45	28.24

Note: Speciated HAPs are proportionally based on the speciated HAPs in the E&P TANK v2.0 flashed gas results. Emission factors for NO<sub>x</sub> and CO from AP-42, Chapter 13.5, Industrial Flares, Table 13.5-1. Emissions in tons per year assume flaring 8,760 hours per year. Uncontrolled emissions for VOC, HAPs, and H<sub>2</sub>S were calculated using the following equation:

$$VOC, HAPs, and \ H_2S \ uncontrolled \ emission \ rate, \\ \frac{lb}{hr} = Molecular \ weight, \\ \frac{lb}{lb-mole} \times \\ \frac{1 \ lb-mole}{379 \ scf} \times Volume \ of \ gas, \\ \frac{scf}{hr} \times Weight \ Percent \ School \ School$$

Table B.1. - Emission Sources

Emission Unit	Quantity	Rating/Capacity
2-Phase Separators w/Heater Treater	2	1.0 MMBtu/hr each
2-Phase Separators w/Heater Treater	1	0.5 MMBtu/hr
Crude Oil/Condensate Storage Tanks	8	400 BBL each
Crude Oil/Condensate Storage Tanks	8	1,000 BBL each
Produced Water Storage Tanks	4	400 BBL each
Produced Water Storage Tanks	4	1,000 BBL each
Flares	4	21.45 scf/hr pilot rating
Fugitive Leaks	-	-
Truck Loading	-	N/A
Compressor Engine	1	400 horsepower
Compressor Engine	1	215 horsepower
Produced Gas	-	-

Table B.2. - Summary of Uncontrolled Emissions in Pounds per Hour

Emission Source	voc	HAPs	NO <sub>x</sub>	co	SO <sub>2</sub>	H₂S	PM <sub>10</sub>	PM <sub>2.5</sub>	CO₂e
2-Phase Separators w/Heater Treater	0.01	0.00	0.25	0.21	0.00	-	0.02	0.02	292.75
(16) Crude Oil/Condensate Storage Tanks	608.79	8.09	-	-	-	0.00	-	-	109.65
(8) Produced Water Storage Tanks	0.06	0.00	-	-	-	0.00	-	_	0.01
(4) Flares Pilots	-		-	-	-	-	-	-	-
Fugitive Leaks	1.51	0.08	-	-	-	0.00	-	-	0.19
Truck Loading	0.48	0.01	-	-	-	0.00	-	-	0.10
(2) Compressor Engines	0.23	0.16	36.41	2.07	0.00	-	0.05	0.05	576.06
Produced Gas	178.69	3.50	-	-	-	0.00	-	-	4,066.53
Total	789.76	11.83	36.65	2.28	0.00	0.00	0.07	0.07	5,045.30

Table B.3. - Summary of Uncontrolled Emissions in Tons Per Year

Emission Source	voc	HAPs	NO <sub>x</sub>	co	SO <sub>2</sub>	H <sub>2</sub> S	PM <sub>10</sub>	PM <sub>2.5</sub>	CO <sub>2</sub> e
2-Phase Separators w/Heater Treater	0.06	0.02	0.25	0.21	0.00	-	0.08	0.08	1,282.22
(16) Crude Oil/Condensate Storage Tanks	2,666.49	35.42	-	-	-	0.00	-	-	480.27
(8) Produced Water Storage Tanks	0.26	0.00	-	-	-	0.00	-	_	0.06
(4) Flares Pilots	~	-	-	-	-	-	-	-	-
Fugitive Leaks	6.61	0.34	-	-	-	0.00	-	-	0.85
Truck Loading	0.25	0.00	-	-	~	0.00	-	-	0.05
(2) Compressor Engines	0.99	0.70	159.47	9.09	0.01	-	0.21	0.21	2,523.16
Produced Gas	782.65	15.31	-	-	-	0.00	-	-	17,811.42
Total	3,457.30	51.80	159.72	9.29	0.01	0.00	0.29	0.29	22,098.03

Table B.4. - Summary of Controlled Emissions in Pounds per Hour

Emission Source	voc	HAPs	NO <sub>X</sub>	со	SO <sub>2</sub>	H <sub>2</sub> S	PM <sub>10</sub>	PM <sub>2.5</sub>	CO <sub>2</sub> e
2-Phase Separators w/Heater Treater	0.01	0.00	0.25	0.21	0.00	-	0.02	0.02	292.75
(16) Crude Oil/Condensate Storage Tanks	12.26	0.19	1.07	4.86	0.01	0.00	0.12	0.12	1,838.84
(8) Produced Water Storage Tanks	0.00	0.00	-	-	-	0.00	-	-	0.00
(4) Flares Pilots	0.00	0.00	0.00	0.02	0.00	-	0.00	0.00	7.91
Fugitive Leaks	1.51	0.08	_	-	-	0.00	-	-	0.19
Truck Loading	0.48	0.01	-	-	-	0.00	-	-	0.10
(2) Compressor Engines	0.95	0.16	1.36	2.71	0.00	-	0.05	0.05	677.45
Produced Gas	3.63	0.09	0.71	3.22	0.01	0.00	0.08	0.08	1,301.47
Total	18.84	0.53	3.38	11.02	0.02	0.00	0.26	0.26	4,118.72

Table B.5. - Summary of Controlled Emissions in Tons Per Year

Emission Source	voc	HAPs	NO <sub>X</sub>	со	SO <sub>2</sub>	H <sub>2</sub> S	PM <sub>10</sub>	PM <sub>2.5</sub>	CO₂e
2-Phase Separators w/Heater Treater	0.06	0.02	1.07	0.90	0.01	-	0.08	0.08	1,282.22
(16) Crude Oil/Condensate Storage Tanks	53.70	0.84	4.67	21.29	0.04	0.00	0.51	0.51	8,054.10
(8) Produced Water Storage Tanks	0.01	0.00	-	-		0.00	-	-	0.02
(4) Flares Pilots	0.00	0.00	0.02	0.09	0.00	-	0.00	0.00	34.65
Fugitive Leaks	6.61	0.34	-	-	-	0.00	-	-	0.85
Truck Loading	0.25	0.00	-	-	-	0.00	-	-	0.05
(2) Compressor Engines	4.16	0.70	5.94	11.88	0.01	-	0.21	0.21	2,967.25
Produced Gas	15.90	0.39	3.09	14.09	0.03	0.00	0.34	0.34	5,700.44
Total	80.68	2.29	14.79	48.25	0.09	0.00	1.14	1.14	18,039.59

Table B.6. - Summary of Uncontrolled HAP Emissions in Pounds per Hour

Hazardous Air Pollutant	Separators	Condensate Tanks	Produced Water Tanks	Flare Pilots	Fugitive Leaks	Truck Loading	Produced Gas	Compressor Engines	Total
1,1,2,2-Tetrachloroethane	-	-	-	-	-	-	-	8.3E-05	8.3E-05
1,1,2-Trichloroethane	-	-	-	-	-	-	-	5.0E-05	5.0E-05
1,3-Butadiene	-	-	-	-	-	-	-	2.2E-03	2.2E-03
1,3-Dichloropropene	-	_	-	-	-	-	-	4.2E-05	4.2E-05
2-Methylnaphthalene	5.9E-08	_	-	-	-	-	-	-	5.9E-08
2,2,4-Trimethylpentane	-	0.58	0.00		0.01	0.00	0.26	-	0.85
3-Methylchloranthrene	4.4E-09	-	-	-	-	-	-	-	4.4E-09
7,12-Dimethylbenz(a)anthracene	3.9E-08	-	-	-	-	-	-	-	3.9E-08
Acenaphthene	4.4E-09	-	-	-	-	-	-	-	4.4E-09
Acetaldehyde	-	-	-	-	-	-	-	9.2E-03	9.2E-03
Acrolein	-	-	-	-	-	-	-	8.7E-03	8.7E-03
Anthracene	5.9E-09	-	-	-	-	-	-	-	5.9E-09
Benzene	5.1E-06	0.71	5.9E-05	-	5.2E-03	6.0E-04	0.30	5.2E-03	1.02
Benzo(a)anthracene	4.4E-09	-	-	-	-	-	-	-	4.4E-09
Benzo(a)pyrene	2.9E-09	-	-	-	-	-	-	-	2.9E-09
Benzo(b)fluoranthene	4.4E-09	-	-	-	-	-	-	-	4.4E-09
Benzo(k)fluoranthene	4.4E-09	-	-	-	-	-	-	-	4.4E-09
Benzo(g,h,i)perylene	2.9E-09	-	-	-	-	_	-	-	2.9E-09
Carbon Tetrachloride	-	-	-	-	-	-	-	5.8E-05	5.8E-05
Chlorobenzene	-	-	-	-	-	-	-	4.2E-05	4.2E-05
Chloroform	-	-	-	-	-	-	-	4.5E-05	4.5E-05
Chrysene	4.4E-09	-	-	-	-	-	-	-	4.4E-09
Dibenz(a,h)anthracene	2.9E-09	-	-	-	-	-	-	-	2.9E-09
Dichlorobenzene	2.9E-06	-	-	-	-	-	-	-	2.9E-06
Ethylbenzene	-	4.7E-02	3.9E-06	-	3.1E-03	3.0E-04	0.02	8.2E-05	0.07
Ethylene Dibromide	-	-	-	-	-	-	-	7.0E-05	7.0E-05
Fluoranthene	7.4E-09	-	-	-	-	-	-	-	7.4E-09
Fluorene	6.9E-09	-	-	-	-	_	-	-	6.9E-09
Formaldehyde	1.8E-04	-	-	-	-	-	-	6.74E-02	6.76E-02
n-Hexane	4.4E-03	6.19	5.1E-04	-	0.03	0.00	3.50	-	9.72
Indeno(1,2,3-cd)pyrene	4.4E-09	-	-	-	-	-	-	-	4.4E-09
Methanol	-	-	-	-	-	-	-	1.0E-02	1.0E-02
Methylene Chloride	-	-	-	-	-	-	-	1.4E-04	1.4E-04
Naphthalene	1.5E-06	-	-	-	-		-	3.2E-04	3.2E-04
PAH	-	-	-	-		-	-	4.6E-04	4.6E-04
Phenanathrene	4.2E-08	-	-	-	-	-	-	-	4.2E-08
Pyrene	1.2E-08	-	-	-	-	-	-	-	1.2E-08
Styrene	-	-	-	-	-	-	-	3.9E-05	3.9E-05
Toluene	8.3E-06	0.36	3.0E-05	-	6.9E-03	4.0E-05	1.52	1.8E-03	1.89
Vinyl Chloride	-	-	-	-	-	-	-	2.4E-05	2.4E-05
Xylene	-	0.19	1.6E-05	-	2.2E-02	5.3E-03	0.08	6.4E-04	0.30
Total	4.61E-03	8.09	6.71E-04	0.00	0.08	0.01	5.68	0.11	13.96

Table B.7. - Summary of Controlled HAP Emissions in Pounds per Hour

Hazardous Air Pollutant	Separator	Condensate Tanks	Produced Water Tanks	Flare Pilot	Fugitive Leaks	Truck Loading	Produced Gas	Compressor Engines	Total
1,1,2,2-Tetrachloroethane	_	-	-	-	_	_	-	8.3E-05	8.3E-05
1,1,2-Trichloroethane	-	-	-	-	_	_	-	5.0E-05	5.0E-05
1,3-Butadiene	-	-	-	-	-	-	-	2.2E-03	2.2E-03
1,3-Dichloropropene	-	_	-	_	-	-	-	4.2E-05	4.2E-05
2-Methylnaphthalene	5.9E-08	-	-	1.6E-09	-	-	-	-	6.0E-08
2,2,4-Trimethylpentane		0.01	0.00	-	0.01	0.00	0.01	-	0.03
3-Methylchloranthrene	4.4E-09	-	-	1.2E-10	-	-	-	-	4.5E-09
7,12-Dimethylbenz(a)anthracene	3.9E-08	-	-	1.1E-09		-	-	-	4.0E-08
Acenaphthene	4.4E-09	-	-	1.2E-10	-	_	-	-	4.5E-09
Acetaldehyde	-	-	-	-	-	-	-	9.2E-03	9.2E-03
Acrolein	_	-	-	-	-	-	-	8.7E-03	8.7E-03
Anthracene	5.9E-09	-	-	1.6E-10	-	-	-	-	6.0E-09
Benzene	5.1E-06	1.4E-02	1.2E-06	1.4E-07	5.2E-03	6.0E-04	0.01	5.2E-03	0.03
Benzo(a)anthracene	4.4E-09	-	-	1.2E-10	-	-	-	-	4.5E-09
Benzo(b)fluoranthene	4.4E-09	-	-	1.2E-10	-	-	-	-	4.5E-09
Benzo(k)fluoranthene	4.4E-09	-	-	1.2E-10	-	-	-	-	4.5E-09
Benzo(a)pyrene	2.9E-09	-	-	7.9E-11	-	-	-	-	3.0E-09
Benzo(g,h,l)perylene	2.9E-09	-	-	7.9E-11	-	-	-	-	3.0E-09
Carbon Tetrachloride	-	-	-	-	-	-	-	5.8E-05	5.8E-05
Chlorobenzene		-	-	-	-	-	-	4.2E-05	4.2E-05
Chloroform	-	-	-	-	-	-	-	4.5E-05	4.5E-05
Chrysene	4.4E-09	-	-	1.2E-10	-	-	-	-	4.5E-09
Dibenz(a,h)anthracene	2.9E-09	-	-	7.9E-11	-	-	-	-	3.0E-09
Dichlorobenzene	2.9E-06	-	-	7.9E-08	-	-	-	-	3.0E-06
Ethylbenzene	-	9.5E-04	7.9E-08	-	3.1E-03	3.0E-04	4.0E-04	8.2E-05	4.8E-03
Ethylene Dibromide	-	-	-	-	-	-	-	7.0E-05	7.0E-05
Fluoranthene	7.4E-09	-	-	2.0E-10	-	-	-	-	7.6E-09
Fluorene	6.9E-09	-	-	1.9E-10	-	-	-	-	7.0E-09
Formaldehyde	1.8E-04	-	-	5.0E-06	-	-	-	6.74E-02	6.76E-02
n-Hexane	4.4E-03	0.15	1.0E-05	1.2E-04	0.03	0.00	0.09	-	0.28
Indeno(1,2,3-cd)pyrene	4.4E-09	-	-	1.2E-10	-	-	-	-	4.5E-09
Methanol		-	-	-	~	-	-	1.0E-02	1.0E-02
Methylene Chloride	~	-	-	-	~	-	-	1.4E-04	1.4E-04
Naphthalene	1.5E-06	-	-	4.0E-08	-	-	-	3.2E-04	3.2E-04
PAH	-	-	-	-	-	-	-	4.6E-04	4.6E-04
Phenanathrene	4.2E-08	-	-	1.1E-09	-	-	-	-	4.3E-08
Pyrene	1.2E-08	-	-	3.3E-10	-	-	-	-	1.3E-08
Styrene	-	-	-	-	-	-	-	3.9E-05	3.9E-05
Toluene	8.3E-06	7.3E-03	6.0E-07	2.3E-07	6.9E-03	4.0E-05	0.03	1.8E-03	0.05
Vinyl Chloride	-	-	-	-	-	-	-	2.4E-05	2.4E-05
Xylene	-	3.9E-03	3.2E-07	-	2.2E-02	5.3E-03	0.00	6.4E-04	0.03
Total	4.61E-03	0.19	1.34E-05	1.25E-04	0.08	0.01	0.13	0.11	0.52

Table B.8. - Summary of Uncontrolled HAP Emissions in Tons per Year

Hazardous Air Pollutant	Separator	Condensate Tanks	Produced Water Tanks	Flare Pilot	Fugitive Leaks	Truck Loading	Produced Gas	Compressor Engines	Total
1,1,2,2-Tetrachloroethane	-	-	-		-	-	-	3.6E-04	3.6E-04
1,1,2-Trichloroethane	-	-	-	-	-	-	-	2.2E-04	2.2E-04
1,3-Butadiene	-	-	-	-	-	-	-	9.6E-03	9.6E-03
1,3-Dichloropropene	-	-	-	-	-	-	-	1.8E-04	1.8E-04
2-Methylnaphthalene	2.6E-07	-	-	-	-	_	-	-	2.6E-07
2,2,4-Trimethylpentane	-	2.56	0.00	-	0.04	0.00	1.14	-	3.73
3-Methylchloranthrene	1.9E-08	-	-	-	-	-	-	-	1.9E-08
7,12-Dimethylbenz(a)anthracene	1.7E-07	-	-	-	-	-	-	-	1.7E-07
Acenaphthene	1.9E-08	-	-	-	-	-	-	-	1.9E-08
Acetaldehyde	-	-	-	-	-	-	-	0.04	0.04
Acrolein	-	-	-	_	-	-	-	3.8E-02	3.8E-02
Anthracene	2.6E-08	-	-	-	-	_	-	-	2.6E-08
Benzene	2.3E-05	3.12	2.6E-04	_	2.3E-02	3.1E-04	1.31	2.3E-02	4.48
Benzo(a)anthracene	1.9E-08	-	-	-	-	-	-	-	1.9E-08
Benzo(b)fluoranthene	1.9E-08	-	-	-	-	_	-	-	1.9E-08
Benzo(k)fluoranthene	1.9E-08	-	-	-	-	-	-	-	1.9E-08
Benzo(a)pyrene	1.3E-08	-	-	-	-	-	-	-	1.3E-08
Benzo(g,h,l)perylene	1.3E-08	-	-	_	-	_	-	-	1.3E-08
Carbon Tetrachloride	-	-	-	_	-	-	-	2.6E-04	2.6E-04
Chlorobenzene	-	-	_	_	-	-	_	1.9E-04	1.9E-04
Chloroform	_	_	_	-	-	_	_	2.0E-04	2.0E-04
Chrysene	1.9E-08	_	_	_	-	-	_	_	1.9E-08
Dibenz(a,h)anthracene	1.3E-08	-	-	-	-	-	-	-	1.3E-08
Dichlorobenzene	1.3E-05	-	-	-	-	-	-	-	1.3E-05
Ethylbenzene	-	2.1E-01	1.7E-05	-	1.4E-02	1.6E-04	0.09	3.6E-04	0.31
Ethylene Dibromide	-	-	-	-	-	-	_	3.1E-04	3.1E-04
Fluoranthene	3.2E-08	-	_	_	-	-	_	_	3.2E-08
Fluorene	3.0E-08	_	-	-	-	-	-	_	3.0E-08
Formaldehyde	8.1E-04	_	_	-	-	-	_	0.30	0.30
n-Hexane	0.02	27.10	2.2E-03	_	0.14	0.00	15.31	_	42.57
Indeno(1,2,3-cd)pyrene	1.9E-08	-	-	_	-	-	-	-	1.9E-08
Methanol	-	-	_	-	-	-	_	4.4E-02	4.4E-02
Methylene Chloride	-	-	_	-	-	-	-	5.9E-04	5.9E-04
Naphthalene	6.5E-06	-	_	-	-	_	_	1.4E-03	1.4E-03
PAH	-	-	_	_	_	_	_	2.0E-03	2.0E-03
Phenanathrene	1.8E-07	-	-		-	-	-	-	1.8E-07
Pyrene	5.4E-08	-	-	-	-	-	-	-	5.4E-08
Styrene	-	-	-	_	-	-	-	1.7E-04	1.7E-04
Toluene	3.7E-05	1.58	1.3E-04	_	3.0E-02	2.1E-05	6.67	8.0E-03	8.29
Vinyl Chloride		-		-	-		-	1.0E-04	1.0E-04
Xylene	-	0.85	7.1E-05	-	9.7E-02	2.8E-03	0.34	2.8E-03	1.30
Total	0.02	35.42	2.94E-03	0.00	0.34	0.00	24.86	0.47	61.12

Table B.9. - Summary of Controlled HAP Emissions in Tons per Year

Hazardous Air Pollutant	Separator	Condensate Tanks	Produced Water Tanks	Flare Pilot	Fugitive Leaks	Truck Loading	Produced Gas	Compressor Engines	Total
1,1,2,2-Tetrachloroethane		-	-	**		-		3.6E-04	3.6E-04
1,1,2-Trichloroethane	-	-	-	-	-	-	-	2.2E-04	2.2E-04
1,3-Butadiene	_	-	-	-	-	-	-	9.6E-03	9.6E-03
1,3-Dichloropropene	•	-	-	-	-	-	-	1.8E-04	1.8E-04
2-Methylnaphthalene	2.6E-07	-	-	7.0E-09	-	-	-	-	2.6E-07
2,2,4-Trimethylpentane	-	0.05	0.00	-	0.04	0.00	0.02	-	0.11
3-Methylchloranthrene	1.9E-08	-	-	5.2E-10	-	-	-	-	2.0E-08
7,12-Dimethylbenz(a)anthracene	1.7E-07	-	-	4.6E-09	-	-	-	-	1.8E-07
Acenaphthene	1.9E-08	-	-	5.2E-10	-	-	-	-	2.0E-08
Acetaldehyde	-	-	-	-	-	-	-	4.02E-02	4.02E-02
Acrolein	_	-	-	-	-	-	-	3.8E-02	3.8E-02
Anthracene	2.6E-08	-	-	7.0E-10	-	-	-	-	2.6E-08
Benzene	2.3E-05	6.3E-02	5.2E-06	6.1E-07	2.3E-02	3.1E-04	0.03	2.3E-02	0.13
Benzo(a)anthracene	1.9E-08	-	-	5.2E-10	-	-	-	-	2.0E-08
Benzo(b)fluoranthene	1.9E-08	-	-	5.2E-10	-	-	-	-	2.0E-08
Benzo(k)fluoranthene	1.9E-08	-	-	5.2E-10	-	-	-	-	2.0E-08
Benzo(a)pyrene	1.3E-08	-	-	3.5E-10	-	-	-	-	1.3E-08
Benzo(g,h,l)perylene	1.3E-08	-	-	3.5E-10	-	-	-	-	1.3E-08
Carbon Tetrachloride	-	-	-	-	-	-	-	2.6E-04	2.6E-04
Chlorobenzene	-	-	-	-	-	-	-	1.9E-04	1.9E-04
Chloroform	-	-	-	-	-	-	-	2.0E-04	2.0E-04
Chrysene	1.9E-08	-	-	5.2E-10	-	-	_	_	2.0E-08
Dibenz(a,h)anthracene	1.3E-08	-	-	3.5E-10	_	-	-	-	1.3E-08
Dichlorobenzene	1.3E-05	-	-	3.5E-07	-	-	-	-	1.3E-05
Ethylbenzene	_	4.2E-03	3.5E-07	_	1.4E-02	1.6E-04	1.8E-03	3.6E-04	2.0E-02
Ethylene Dibromide	_	-	-	_	_	-	-	3.1E-04	3.1E-04
Fluoranthene	3.2E-08	-	-	8.7E-10	-	-	-	-	3.3E-08
Fluorene	3.0E-08	-	-	8.1E-10	_	-	-	-	3.1E-08
Formaldehyde	8.1E-04	-	-	2.2E-05	-	-	-	0.30	0.30
n-Hexane	0.02	0.66	4.5E-05	5.2E-04	0.14	0.00	0.39	-	1.21
Indeno(1,2,3-cd)pyrene	1.9E-08	-	-	5.2E-10	-	-	-	-	2.0E-08
Methanol	-	-	-	-	-	-	-	4.4E-02	4.4E-02
Methylene Chloride	-	-	-	-	-	-	-	5.9E-04	5.9E-04
Naphthalene	6.5E-06	-	-	1.8E-07	-	-	-	1.4E-03	1.4E-03
PAH	-	-	-	~	_	-	-	2.0E-03	2.0E-03
Phenanathrene	1.8E-07	-	-	4.9E-09	**	-	-	-	1.9E-07
Pyrene	5.4E-08	-	-	1.5E-09	_	-	-	-	5.5E-08
Styrene	-	-	-	_	-	-	-	1.7E-04	1.7E-04
Toluene	3.7E-05	3.2E-02	2.6E-06	9.9E-07	3.0E-02	2.1E-05	0.13	8.0E-03	0.20
Vinyl Chloride	-	-	-	-	-	-	-	1.0E-04	1.0E-04
Xylene	-	1.7E-02	1.4E-06	-	9.7E-02	2.8E-03	0.01	2.8E-03	0.13
Total	0.02	0.83	5.88E-05	5.46E-04	0.34	0.00	0.58	0.47	2.24

## Primus Facility: PetroShale US 8H, US12H, & US 13H Production Facility Actual Emission Calculations Most Recent Production Data

Table B.10.a - PetroShale US8H Most Recent Year of Production Data

Month	Oil Produced, BBLs	Water Produced, BBLs	Gas Produced, MSCF	Gas Flared, MCF
August 2019	5,377	1,798	0	0
July 2019	10,479	4,143	18,547	8,468
June 2019	14,908	5,446	26,100	10
May 2019	15,957	6,775	25,826	789
April 2019	16,997	10,371	24,445	2,967
March 2019	2,381	1,737	148	35
February 2019	9,346	1,586	13,089	408
January 2019	11,406	1,985	14,935	46
December 2019	11,919	2,191	16,915	155
November 2018	13,540	2,786	20,861	4,240
October 2018	16,223	3,615	25,952	198
September 2018	16,340	3,504	25,691	465
Daily Average	396.91	125.85	582.22	48.72

Table B.10.b - PetroShale US12H Production Data Since Well Completion

Month	Days On	Oil Produced, BBLs	Water Produced, BBLs	Gas Produced, MSCF	Gas Flared <sup>1</sup> , MCF
August 2019	8	10,044	3,235	12,743	1,043
September 2019	30	33,122	N/A	41,778	3,496
October 2019	1	945	N/A	1,410	118
Daily Average		1,131.05	404.38	1,434.13	119.40
Adjusted Daily Average <sup>2</sup>		678.63	242.63	860.48	71.64

 $<sup>^{\</sup>mathrm{1}}$  Assumed the gas flared would be at the same rate as the US8H well.

<sup>&</sup>lt;sup>2</sup> Assuming a 40% decline in production for the first year of operation.

Table B.10.c - PetroShale US 13H Production Data Since Well Completion

Date	Oil Produced, BBLs	Water Produced, BBLs	Gas Produced, MSCF	Gas Flared <sup>1</sup> , MCF
August 2019	6,580	2,290	0	0
July 2019	0	0	0	0
June 2019	14,289	10,020	29,092	2,434
May 2019	28,139	15,655	68,482	5,730
Daily Average	418.87	239.02	833.97	69.78
Adjusted Daily Average <sup>2</sup>	251.32	143.41	500.38	41.87

<sup>&</sup>lt;sup>1</sup> Assumed the gas flared would be at the same rate as the US8H well.

Table B.10.d - Daily Average Production of the Entire Primus Facility (all 3 wells)

Well	Oil Produced Per Day, BBLs		Gas Produced Per Day, MSCF	Gas Flared Per Day, MCF
PetroShale US8H	396.91	125.85	582.22	48.72
PetroShale US12H	678.63	242.63	860.48	71.64
PetroShale US13H	251.32	143.41	500.38	41.87
Total Facility Daily Average	1,326.87	511.89	1,943.07	162.22

<sup>&</sup>lt;sup>1</sup> Assuming a 40% decline in production for the first year of operation.

<sup>&</sup>lt;sup>2</sup> Assuming a 40% decline in production for the first year of operation.

### Primus Facility: PetroShale US 8H, US12H, & US 13H Production Facility Actual Emission Calculations Separator Burners

Table B.11. - Separator Burner Information

Parameter	Value
Burner Rating (each), MMBtu/hr	1.00
Number of Separator Burners	2
Burner Rating (each), MMBtu/hr	0.50
Number of Separator Burners	1
HHV, Btu/scf	1,535.40
Total Fuel Consumption, Mscf/day	39.08

Note: Fuel HHV from gas analysis dated March 6, 2017. Fuel consumption calculated using:

$$\frac{Mscf}{day} = \left[Burner\ rating, \frac{MMBtu}{hr}\right] \times \left[\frac{10^6Btu}{MMBtu}\right] \times \left[\frac{24hr}{day}\right] + \left[HHV, \frac{Btu}{scf}\right] + \left[\frac{1,000\ scf}{Mscf}\right]$$

Table B.12. - Separator Burner Criteria Pollutant Emissions

Pollutant	Emission Factor, lb/10 <sup>6</sup> scf	Emission Factor, lb/MMBtu	Emission Rate, lb/hr	Emission Rate, tpy
PM <sub>10</sub> 1	7.60	7.45E-03	0.02	0.08
PM <sub>2.5</sub> 1	7.60	7.45E-03	0.02	0.08
SO <sub>2</sub>	0.60	5.88E-04	1.47E-03	6.44E-03
NO <sub>X</sub>	100.00	0.10	0.25	1.07
со	84.00	0.08	0.21	0.90
voc	5.50	5.39E-03	0.01	0.06

Note: Based on EPA AP-42, Section 1.4, Natural Gas Combustion (Tables 1.4-1 and 1.4-2). Emission factors converted from lb/10<sup>6</sup> scf to lb/MMBtu by dividing by the average heat value of natural gas: 1,020 Btu/scf.

Table B.13. - Separator Burner Hazardous Air Pollutant Emissions

Pollutant	Emission Factor, lb/10 <sup>6</sup> scf	Emission Factor, lb/MMBtu	Emission Rate, lb/hr	Emission Rate, tpy
2-Methylnaphthalene	2.40E-05	2.35E-08	5.88E-08	2.58E-07
3-Methylchloranthrene	1.80E-06	1.76E-09	4.41E-09	1.93E-08
7,12-Dimethylbenz(a)anthracene	1.60E-05	1.57E-08	3.92E-08	1.72E-07
Acenaphthene	1.80E-06	1.76E-09	4.41E-09	1.93E-08
Anthracene	2.40E-06	2.35E-09	5.88E-09	2.58E-08
Benz(a)anthracene	1.80E-06	1.76E-09	4.41E-09	1.93E-08
Benzene	2.10E-03	2.06E-06	5.15E-06	2.25E-05
Benzo(a)pyrene	1.20E-06	1.18E-09	2.94E-09	1.29E-08
Benzo(b) fluoranthene	1.80E-06	1.76E-09	4.41E-09	1.93E-08
Benzo(g,h,i)perylene	1.20E-06	1.18E-09	2.94E-09	1.29E-08
Benzo(k)fluoranthene	1.80E-06	1.76E-09	4.41E-09	1.93E-08
Crysene	1.80E-06	1.76E-09	4.41E-09	1.93E-08
Dibenzo (a, h) anthracene	1.20E-06	1.18E-09	2.94E-09	1.29E-08
Dichlorobenzene	1.20E-03	1.18E-06	2.94E-06	1.29E-05
Fluoranthene	3.00E-06	2.94E-09	7.35E-09	3.22E-08
Fluorene	2.80E-06	2.75E-09	6.86E-09	3.01E-08
Formaldehyde	7.50E-02	7.35E-05	1.84E-04	8.05E-04
n-Hexane	1.80E+00	1.76E-03	4.41E-03	1.93E-02
Indeno(1,2,3-cd)pyrene	1.80E-06	1.76E-09	4.41E-09	1.93E-08
Naphthalene	6.10E-04	5.98E-07	1.50E-06	6.55E-06
Phenanathrene	1.70E-05	1.67E-08	4.17E-08	1.83E-07
Pyrene	5.00E-06	4.90E-09	1.23E-08	5.37E-08
Toluene	3.40E-03	3.33E-06	8.33E-06	3.65E-05
Total:			4.61E-03	0.02

Note: Based on EPA AP-42, Section 1.4, Natural Gas Combustion (Table 1.4-3). Emission factors converted from lb/10<sup>6</sup> scf to lb/MMBtu by dividing by the average heat value of natural gas: 1,020 Btu/scf.

Table B.14. - Separator Burner Greenhouse Gas Emissions

Pollutant	Emission Factor, kg/MMBtu	Emission Factor, lb/MMBtu	Emission Rate, lb/hr	Emission Rate, tpy		
CO <sub>2</sub>	53.06	116.98	292.44	1,280.90		
CH <sub>4</sub>	1.00E-03	2.20E-03	5.51E-03	0.02		
N <sub>2</sub> O	1.00E-04	2.20E-04	5.51E-04	2.41E-03		
	Total CO <sub>2</sub> e:					

Note: Emission factors from 40 CFR Part 98 Subpart C, Table C-1 and C-2. Converted from kilograms to pounds. Global warming potentials for CH<sub>4</sub> and N<sub>2</sub>O are 25 and 298, respectively.

 $<sup>^{1}\,\</sup>mathrm{PM}_{10}$  and  $\mathrm{PM}_{2.5}$  are assumed to equal total particulate matter.

### Primus Facility: PetroShale US 8H, US12H, & US 13H Production Facility **Actual Emission Calculations**

### **Crude Oil/Condensate Storage Tanks**

Table B.15. - Crude Oil/Condensate Storage Tank Vapor Sent to Flare Information

Parameter	Value
Tank Vapor Volume, scfm	96.22
Tank Vapor Heating Value, Btu/scf	2,715.46
Total Gas Volume per Hour, MMSCF/hr	0.00577

Note: Tank vapor volume and heating value from E&P Tanks modeling run.

Table B.16. - Crude Oil/Condensate Storage Tank Vapor Sent to Flare Criteria Pollutant Emissions

Pollutant	Emission Factor, lb/10 <sup>6</sup> scf	Emission Factor, lb/MMBtu	Emissions, lb/hr	Emissions, tpy
PM <sub>10</sub> 1	7.60	7.45E-03	0.12	0.51
PM <sub>2.5</sub> 1	7.60	7.45E-03	0.12	0.51
SO₂	0.60	5.88E-04	0.01	0.04
NO <sub>X</sub>	-	0.07	1.07	4.67
со	-	0.31	4.86	21.29
voc	5.50	5.39E-03	0.08	0.37

Note: Emission factors for NO<sub>x</sub> and CO from AP-42, Section 13.5, Industrial Flares, Table 13.5-1, and calculated using the equation below:

$$NO_{\chi} \ and \ CO, \frac{lb}{hr} = \left[HHV, \frac{\mathrm{Btu}}{\mathrm{scf}}\right] \times \left[\frac{\mathrm{scf}}{\mathrm{hr}}\right] \times \left[EF, \frac{\mathrm{lb}}{\mathrm{MMBtu}}\right] \times \left[\frac{\mathrm{MMBtu}}{10^{6}Btu}\right]$$
Emission factors for PM<sub>10</sub>, PM<sub>2.5</sub>, SO<sub>2</sub>, and VOC from AP-42, Section 1.4, Natural Gas Combustion, Table 1.4-2, calculated using the equation below:

$$PM_{10}, PM_{2.5}, SO_2, or\ VOC, \frac{lb}{hr} = \left[ Total\ gas\ volume, \frac{10^6\ scf}{hr} \right] \times \left[ EF, \frac{lb}{10^6\ scf} \right] \times \frac{Produced\ Gas\ heating\ value\ \left[ \frac{btu}{scf} \right]}{Average\ NG\ heating\ value\ (1,020)\ \left[ \frac{btu}{scf} \right]}$$

Table B.17. - Crude Oil/Condensate Storage Tank Vapor Sent to Flare Hazardous Air Pollutant Emissions

Pollutant	Emission Factor, lb/10 <sup>6</sup> scf	Emission Rate, lb/hr	Emission Rate, tpy
2-Methylnaphthalene	2.40E-05	3.69E-07	1.62E-06
3-Methylchloranthrene	1.80E-06	2.77E-08	1.21E-07
7,12-Dimethylbenz(a)anthracene	1.60E-05	2.46E-07	1.08E-06
Acenaphthene	1.80E-06	2.77E-08	1.21E-07
Anthracene	2.40E-06	3.69E-08	1.62E-07
Benz(a)anthracene	1.80E-06	2.77E-08	1.21E-07
Benzene	2.10E-03	3.23E-05	1.41E-04
Benzo(a)pyrene	1.20E-06	1.84E-08	8.08E-08
Benzo(b)fluoranthene	1.80E-06	2.77E-08	1.21E-07
Benzo(g,h,i)perylene	1.20E-06	1.84E-08	8.08E-08
Benzo(k)fluoranthene	1.80E-06	2.77E-08	1.21E-07
Crysene	1.80E-06	2.77E-08	1.21E-07
Dibenzo(a,h)anthracene	1.20E-06	1.84E-08	8.08E-08
Dichlorobenzene	1.20E-03	1.84E-05	8.08E-05
Fluoranthene	3.00E-06	4.61E-08	2.02E-07
Fluorene	2.80E-06	4.30E-08	1.88E-07
Formaldehyde	7.50E-02	1.15E-03	5.05E-03
n-Hexane	1.80E+00	2.77E-02	1.21E-01
Indeno(1,2,3-cd)pyrene	1.80E-06	2.77E-08	1.21E-07
Naphthalene	6.10E-04	9.38E-06	4.11E-05
Phenanathrene	1.70E-05	2.61E-07	1.14E-06
Pyrene	5.00E-06	7.68E-08	3.37E-07
Toluene	3.40E-03	5.23E-05	2.29E-04
Total:		0.03	0.13

Note: Based on EPA AP-42, Section 1.4, Natural Gas Combustion (Table 1.4-3).

Table B.18. - Crude Oil/Condensate Storage Tank Vapor Sent to Flare Greenhouse Gas Emissions

Pollutant	Emission Factor, kg/MMBtu	Emission Factor, lb/MMBtu	Emissions, lb/hr	Emissions, tpy
CO <sub>2</sub>	53.06	116.98	1,833.88	8,032.41
CH <sub>4</sub>	1.00E-03	2.20E-03	3.46E-02	0.15
N <sub>2</sub> O	1.00E-04	2.20E-04	3.46E-03	1.51E-02
		Total CO₂e:	1,835.78	8,040.71

Note: Emission factors from 40 CFR Part 98 Subpart C, Table C-1 and C-2. Converted from kilograms to pounds. Global warming potentials for CH $_{\rm d}$  and N $_{\rm 2}$ O are 25 and 298, respectively.

## Petroshale (US), Inc. Primus Facility: PetroShale US 8H, US12H, & US 13H Production Facility Actual Emission Calculations Crude Oil/Condensate Storage Tanks

Table B.19. - E&P Tank Modeling Results and Percent Total

		Uncontrolled Emission	15	Controlled Emissions				
Parameter	E	E&P Tanks Model Results, tpy			E&P Tanks Model Results, tpy			
	Flashing	Working & Breathing	Total	Flashing	Working & Breathing	Total		
Total Emissions	629.76	2,464.08	3,093.84	12.60	49.28	61.88		
Emissions per Tank	39.36	154.00	193.37	0.79	3.08	3.87		
Percent of Total	20.4%	79.6%	100%	20.4%	79.6%	100%		

Note: Flashing and working & breathing losses are only provided for uncontrolled emissions in the E&P Tank model. These percentages of the total (20.4% for flashing emissions and 79.6% for working & breathing emissions) were used to estimate emissions for other pollutants (below, in Table B.20).

Table B.20. - Crude Oil/Condensate Storage Tank Emissions

		Uncontrolled Em	ilssions				Con	trolled Emissions				
Parameter		E&P Tanks Model Results		E&P Tan	E&P Tanks Model Results, tpy		Calculated Tank Vapor	Total Emissions		Emissions per Tank		
	Flashing	Working & Breathing	Total, lb/hr	Total, tpy	Flashing	Working & Breathing	Total, tpy	Combustion Emissions, tpy	lb/hr	tpy	lb/hr	tpy
VOC	542.77	2,123.71	608.79	2,666.49	10.86	42.47	53.33	0.37	12.26	53.70	0.77	3.36
Total CO <sub>2</sub> e	97.76	382.51	109.65	480.27	2.73	10.67	13.39	8,040.71	1,838.84	8,054.10	114.93	503.38
CH₄	3.88	15.18	4.35	19.06	0.08	0.30	0.38	0.15	0.12	0.53	0.01	0.03
CO <sub>2</sub>	0.79	3.08	0.88	3.87	0.79	3.08	3.87	8,032.41	1,834.77	8,036.28	114.67	502.27
N <sub>2</sub> O	-	-	-	-	<del>-</del>	-	-	0.02	3.46E-03	0.02	2.16E-04	9.46E-04
Total HAPs	7.21	28.21	8.09	35.42	0.14	0.56	0.71	0.13	0.19	0.84	0.01	0.05
Benzene	0.63	2.48	0.71	3.12	0.01	0.05	0.06	1.41E-04	0.01	0.06	8.92E-04	3.91E-03
Toluene	0.32	1.26	0.36	1.58	0.01	0.03	0.03	2.29E-04	0.01	0.03	4.55E-04	1.99E-03
Ethylbenzene	0.04	0.17	0.05	0.21	8.47E-04	3.31E-03	4.16E-03	~	9.50E-04	4.16E-03	5.94E-05	2.60E-04
Xylene	0.17	0.68	0.19	0.85	3.47E-03	0.01	0.02	-	3.89E-03	0.02	2.43E-04	1.07E-03
n-C6	5.52	21.58	6.19	27.10	0.11	0.43	0.54	0.12	0.15	0.66	0.01	0.04
2,2,4-Trimethylpentane	0.52	2.04	0.58	2.56	0.01	0.04	0.05	-	0.01	0.05	7.30E-04	3.20E-03
H <sub>2</sub> S	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-	0.00	0.00	0.00	0.00
PM <sub>10</sub>	-	-	-	-	-	-	-	0.51	0.12	0.51	0.01	0.03
PM <sub>2.5</sub>	-	-	-	-	-	~	-	0.51	0.12	0.51	0.01	0.03
SO <sub>2</sub>	-	-	-	-	-	-	-	0.04	0.01	0.04	5.76E-04	2.52E-03
NO <sub>X</sub>	-	-	-	-	-	-	-	4.67	1.07	4.67	0.07	0.29
со	-	-	-	-	_	-	-	21.29	4.86	21.29	0.30	1.33

Note: Uncontrolled and controlled emissions from E&P Tank model run using the oil analysis dated March 6, 2017, included in this appendix. Assumed 98% control efficiency for the flare. Flashing and working & breathing losses estimated for the pollutants above as a percentage of their total emissions (see Table B.19). For example, total uncontrolled flashing emissions was equal to 20.4% of total uncontrolled emissions. Therefore, for VOC, flashing emissions are 20.4% of total uncontrolled VOC emissions. Emissions in pounds per hour assumed to occur over 8,760 hours per year.

# Petroshale (US), Inc. Primus Facility: PetroShale US 8H, US12H, & US 13H Production Facility Actual Emission Calculations Produced Water Tanks

Table B.21. - Produced Water Tanks Emissions

Pollutant	Uncontroll	ed Emissions	Controlled Emissions		
Poliutant	lb/hr	tpy	lb/hr	tpy	
voc	0.06	0.26	1.17E-03	5.14E-03	
Total CO₂e	0.01	0.06	3.84E-03	0.02	
CH <sub>4</sub>	3.61E-04	1.58E-03	7.22E-06	3.16E-05	
CO <sub>2</sub>	3.66E-03	0.02	3.66E-03	0.02	
Total HAPs	6.71E-04	2.94E-03	1.34E-05	5.88E-05	
Benzene	5.91E-05	2.59E-04	1.18E-06	5.18E-06	
Toluene	3.00E-05	1.31E-04	6.00E-07	2.63E-06	
Ethylbenzene	3.94E-06	1.73E-05	7.88E-08	3.45E-07	
Xylene	1.62E-05	7.08E-05	3.23E-07	1.42E-06	
n-C6	5.14E-04	2.25E-03	1.03E-05	4.50E-05	
2,2,4-Trimethylpentane	4.85E-05	2.12E-04	9.69E-07	4.25E-06	
H <sub>2</sub> S	0.00	0.00	0.00	0.00	

Note: Produced water tank emissions from EPA TANKS modeling run. Speciated HAPs are assumed to have the same proportion of emissions (HAP to VOC) as the crude oil/ condensate storage tanks. Assumed 98% control efficiency for the flare. Emissions in pounds per hour assumed to occur over 8,760 hours per year.

### Primus Facility: PetroShale US 8H, US12H, & US 13H Production Facility **Actual Emission Calculations Steffes Engineered Flare Pilot**

Table B.22. - Steffes Engineered Flare Pilot Information

Parameter	Value
Flare Pilot Usage, hours	8,760
Number of Flares	4
Flare Pilot Gas, scfm	0.2
Flare Pilot Gas Heating Value, Btu/scf	1,535.4
Total Gas Volume per Hour per Flare, MMSCF/hr	0.00001
Flare Control Efficiency	98%

Note: Flare pilot gas conservatively assumed and gas heating value is averaged from a produced gas analysis dated March 6, 2017.

Table B.23. - Steffes Engineered Flare Pilot Criteria Pollutant Emissions

Pollutant	Emission Factor, lb/10 <sup>6</sup> scf	Emission Factor, lb/MMBtu	Emissions, lb/hr	Emissions, tpy
PM <sub>10</sub> <sup>1</sup>	7.60	7.45E-03	5.03E-04	2.20E-03
PM <sub>2.5</sub> <sup>1</sup>	7.60	7.45E-03	5.03E-04	2.20E-03
SO₂	0.60	5.88E-04	3.97E-05	1.74E-04
NO <sub>X</sub>	~	0.07	4.59E-03	2.01E-02
со	-	0.31	0.02	9.17E-02
voc	5.50	5.39E-03	3.64E-04	1.60E-03

Note: Emission factors for NO<sub>x</sub> and CO from AP-42, Section 13.5, Industrial Flares, Table 13.5-1, and calculated using the equation below:

$$NO_X \ and \ CO, \frac{lb}{hr} = \left[HHV, \frac{\text{Btu}}{\text{scf}}\right] \times \left[\frac{\text{scf}}{\text{hr}}\right] \times \left[EF, \frac{lb}{\text{MMBtu}}\right] \times \left[\frac{\text{MMBtu}}{10^6 Btu}\right]$$
 Emission factors for PM<sub>10</sub>, PM<sub>25</sub>, SO<sub>2</sub>, and VOC from AP-42, Section 1.4, Natural Gas Combustion, Table 1.4-2, calculated using the equation below:

$$PM_{10}, PM_{2.5}, SO_2, or\ VOC, \frac{lb}{hr} = \begin{bmatrix} Total\ gas\ volume, \frac{10^6\ scf}{hr} \\ \end{bmatrix} \times \begin{bmatrix} EF, \frac{lb}{10^6\ scf} \end{bmatrix} \times \frac{Produced\ Gas\ heating\ value\ \begin{bmatrix} btu\\ scf \end{bmatrix}}{Average\ NG\ heating\ value\ (1,020) \begin{bmatrix} btu\\ scf \end{bmatrix}}$$

$$^1 PM_{10} \ and\ PM_{2.5} \ are\ assumed\ to\ equal\ total\ particulate\ matter}.$$

Table B.24. - Steffes Engineered Flare Pilot Hazardous Air Pollutant Emissions

Pollutant	Emission Factor, lb/10 <sup>6</sup> scf	Emission Rate, lb/hr	Emission Rate, tpy
2-Methylnaphthalene	2.40E-05	1.59E-09	6.96E-09
3-Methylchloranthrene	1.80E-06	1.19E-10	5.22E-10
7,12-Dimethylbenz(a) anthracene	1.60E-05	1.06E-09	4.64E-09
Acenaphthene	1.80E-06	1.19E-10	5.22E-10
Anthracene	2.40E-06	1.59E-10	6.96E-10
Benz(a)anthracene	1.80E-06	1.19E-10	5.22E-10
Benzene	2.10E-03	1.39E-07	6.09E-07
Benzo(a)pyrene	1.20E-06	7.95E-11	3.48E-10
Benzo(b)fluoranthene	1.80E-06	1.19E-10	5.22E-10
Benzo(g,h,i)perylene	1.20E-06	7.95E-11	3.48E-10
Benzo(k)fluoranthene	1.80E-06	1.19E-10	5.22E-10
Crysene	1.80E-06	1.19E-10	5.22E-10
Dibenzo(a,h)anthracene	1.20E-06	7.95E-11	3.48E-10
Dichlorobenzene	1.20E-03	7.95E-08	3.48E-07
Fluoranthene	3.00E-06	1.99E-10	8.70E-10
Fluorene	2.80E-06	1.85E-10	8.12E-10
Formaldehyde	7.50E-02	4.97E-06	2.18E-05
n-Hexane	1.80E+00	1.19E-04	5.22E-04
Indeno(1,2,3-cd)pyrene	1.80E-06	1.19E-10	5.22E-10
Naphthalene	6.10E-04	4.04E-08	1.77E-07
Phenanathrene	1.70E-05	1.13E-09	4.93E-09
Pyrene	5.00E-06	3.31E-10	1.45E-09
Toluene	3.40E-03	2.25E-07	9.86E-07
Total:		1.25E-04	5.46E-04

Note: Based on EPA AP-42, Section 1.4, Natural Gas Combustion (Table 1.4-3).

Table B.25. - Steffes Engineered Flare Pilot Greenhouse Gas Emissions

Pollutant	Emission Factor, kg/MMBtu	Emission Factor, lb/MMBtu	Emissions, lb/hr	Emissions, tpy
CO <sub>2</sub>	53.06	116.98	7.90	34.61
CH₄	1.00E-03	2.20E-03	1.49E-04	6.52E-04
N <sub>2</sub> O	1.00E-04	2.20E-04	1.49E-05	6.52E-05
		Total CO₂e:	7.91	34.65

Note: Emission factors from 40 CFR Part 98 Subpart C, Table C-1 and C-2. Converted from kilograms to pounds. Global warming potentials for CH<sub>4</sub> and N<sub>2</sub>O are 25 and 298,

## Petroshale (US), Inc. Primus Facility: PetroShale US 8H, US12H, & US 13H Production Facility Actual Emission Calculations Fugitive Leaks

Table B.26. - Fugitive Emissions: Emission Factors for Total Hydrocarbon (THC) Emissions

Equipment Type	Equipment Service Category, lb/hr/source						
	Gas	Heavy Oil (< 20° API)	Light Oil (>20° API)	Water/Light Oil			
Valves	9.92E-03	1.85E-05	5.51E-03	2.16E-04			
Pump Seals	5.29E-03	-	2.87E-02	5.29E-05			
Others	1.94E-02	7.05E-05	1.65E-02	3.09E-02			
Connectors	4.41E-04	1.65E-05	4.63E-04	2.43E-04			
Flanges	8.60E-04	8.60E-07	2.43E-04	6.39E-06			
Open-Ended Lines	4.41E-03	3.09E-04	3.09E-03	5.51E-04			

Note: From US EPA Protocol for Equipment Leak Emission Estimates (EPA-453/R-95-017). Emission factors converted from kg/source-hr to lb/source-hr The water/light oil emission factors apply to water streams in light oil service with water content between 50% and 99%. For streams with water content > 99%, the emission rate is considered negligible. The "other" equipment type includes compressor, pressure relief valves, diaphragms, drains, dump arms, hatches, instruments, meters, polished rods, and vents.

**Table B.27. - Fugitive THC Emissions** 

Equipment Type	Number of Components	Service	Emission Factor, lb/hr/source	THC Emissions, lb/hr	THC Emissions, tpy
Valves	78	Gas	9.92E-03	0.77	3.39
Valves	78	Light Oil	5.51E-03	0.43	1.88
Valves	8	Water/Light Oil	2.16E-04	1.73E-03	0.01
Pump Seals	0	Gas	5.29E-03	0.00	0.00
Pump Seals	0	Light Oil	2.87E-02	0.00	0.00
Pump Seals	0	Water/Light Oil	5.29E-05	0.00	0.00
Others	0	Gas	1.94E-02	0.00	0.00
Others	0	Light Oil	1.65E-02	0.00	0.00
Others	0	Water/Light Oil	3.09E-02	0.00	0.00
Connectors	672	Gas	4.41E-04	0.30	1.30
Connectors	354	Light Oil	4.63E-04	0.16	0.72
Connectors	52	Water/Light Oil	2.43E-04	0.01	0.06
Flanges	4	Gas	8.60E-04	3.44E-03	0.02
Flanges	0	Light Oil	2.43E-04	0.00	0.00
Flanges	0	Water/Light Oil	6.39E-06	0.00	0.00
Open-Ended Lines	0	Gas	4.41E-03	0.00	0.00
Open-Ended Lines	0	Light Oil	it Oil 3.09E-03 0.00		0.00
Open-Ended Lines	0	Water/Light Oil	5.51E-04	0.00	0.00
			Total THC Emissions:	1.68	7.38

Note: Number of components estimated from actual counts performed at similar facilities.

**Table B.28. - Speciated Fugitive Emission Factors** 

Pollutant	Weight Fraction Gas	Weight Fraction Light Oil	Weight Fraction Water/Light Oil	Emissions, lb/hr	Emissions, tpy
THC	1.00	1.00	1.00	1.68	7.37
voc	0.84	1.00	1.00	1.51	6.61
Total CO₂e		-	_	0.19	0.85
CH <sub>4</sub>	7.20E-03	0.00	0.00	0.01	0.03
CO <sub>2</sub>	1.46E-03	0.00	0.00	1.57E-03	0.01
Total HAPs	1.23E-02	0.11	0.11	0.08	0.34
Benzene	1.05E-03	6.64E-03	6.64E-03	0.01	0.02
Toluene	7.08E-05	1.12E-02	1.12E-02	0.01	0.03
Ethylbenzene	5.35E-04	4.16E-03	4.16E-03	3.10E-03	0.01
Xylenes	9.43E-03	1.99E-02	1.99E-02	0.02	0.10
n-Hexane	2.76E-04	5.14E-02	5.14E-02	0.03	0.14
2,2,4-Trimethylpentane	9.12E-04	1.18E-02	1.18E-02	0.01	0.04
H <sub>2</sub> S	0.00	0.00	0.00	0.00	0.00

Note: Water/Light Oil and Light Oil Weight fractions based on E&P Tank modeling run flashed gas results for the oil storage tanks. All stream weight fractions for organic compounds used in calculations are normalized based on 100% THC since EPA emission factors are based on THC emission rate. Produced gas speciated HAPs are proportionally based on the speciated HAPs in the E&P TANK v2.0 flashed gas results, then normalized based on 100% THC.

# Petroshale (US), Inc. Primus Facility: PetroShale US 8H, US12H, & US 13H Production Facility Actual Emission Calculations Truck Loading

Table B.29. - Truck Loading Emissions Calculation Inputs - Produced Water Only

Parameter	Value
Saturation Factor (S)	0.6
True Vapor Pressure of Liquid Loaded (P), psia	0.24
Molecular Weight of Vapors (M), lb/lb-mole	20.68
Temperature of Bulk Liquid Loaded (T), °F	41.45
Loading Losses, lb/1,000 gallons	80.0
Water Production, BPD	511.9
Average Water Loadout Rate, gallons/hr	895.8
Maximum Water Loadout Rate, gallons/hr	7,560.0
Maximum Yearly Throughput, gallons/yr	7,847,274

Note: Loading losses based on EPA AP-42 Section 5.2-4:

$$L_L = 12.46 \frac{SPM}{(T + 460)}$$

Saturation factor based on submerged loading: dedicated normal service. Molecular weight of vapors and liquid bulk temperature from EPA Tank run. TVP of liquid loaded is assumed to be the maximum vapor pressure from hottest month (July) to be conservative.

Table B.30. - Truck Loading Emissions in Tons Per Year

Dalliaa	384-1-4-6 F	Produced Water Loading		
Pollutant	Weight Fraction	lb/hr	tpy	
тнс	1.00	0.57	0.29	
voc	0.84	0.48	0.25	
Total CO₂e	-	0.10	0.05	
CH <sub>4</sub>	7.20E-03	4.08E-03	2.12E-03	
CO <sub>2</sub>	1.46E-03	8.28E-04	4.29E-04	
Total HAPs	1.23E-02	0.01	3.61E-03	
Benzene	1.05E-03	5.97E-04	3.10E-04	
Toluene	7.08E-05	4.02E-05	2.08E-05	
Ethylbenzene	5.35E-04	3.03E-04	1.57E-04	
Xylenes	9.43E-03	0.01	2.78E-03	
n-Hexane	2.76E-04	1.57E-04	8.13E-05	
2,2,4-Trimethylpentane	9.12E-04	5.17E-04	2.68E-04	
H <sub>2</sub> S	0.00	0.00	0.00	

Note: Weight fractions based on E&P Tank modeling run working and breathing gas composition for the crude oil/condensate storage tanks, which is included in this appendix. Truck loading emissions in lb/hr use maximum loadout rate. Note that crude oil/condensate is removed from site via pipeline so no loading emissions for crude oil/condensate are calculated.

Table B.31. - Engine Information

Parameter	Value
Engine #1 Horsepower (hp)	400
Number of Units	1
Fuel	Natural Gas
Annual Hours of Operation per Unit (hr)	8,760
Fuel Heat Rating (Btu/hr) <sup>1</sup>	3,290,000
Maximum Heat Input (MMBtu/hr)	3.29
Fuel Specific HHV (Btu/scf)	1,020
Fuel Use Rate (scf/hr)	3,225.49
Annual Fuel Consumption (MMBtu/year)	28,820.40
Annual Fuel Consumption (MMSCF/year)	28.26

<sup>&</sup>lt;sup>1</sup> Values from engine manufacturer's specifications.

Table B.32. - Uncontrolled Compressor Engine Emissions

Component	Uncontrolled Emi	ssion Factor 1	Uncontrolled E	Uncontrolled Emission Rate	
Component	lb/MMBtu	g/bhp-hr	lb/hr	tons/year	
NO <sub>X</sub>	~	26.27	23.17	101.47	
со	-	1.60	1.41	6.18	
VOCs		0.16	0.14	0.62	
Formaldehyde	2.05E-02	-	6.74E-02	0.30	
PM <sub>2.5</sub>	9.50E-03	-	3.13E-02	0.14	
PM <sub>10</sub>	9.50E-03	-	3.13E-02	0.14	
PM	9.10E-03	-	2.99E-02	0.13	
SO <sub>2</sub>	5.88E-04	-	1.93E-03	0.01	
CH₄	0.23	-	0.76	3.31	
N <sub>2</sub> O	1.32E-03	-	4.35E-03	0.02	
CO <sub>2</sub>	110.00	-	361.90	1,585.12	
CO₂e <sup>2</sup>	110.00	-	382.11	1,673.66	

<sup>&</sup>lt;sup>1</sup> The emission factors for CO, NOx, and VOC are based on the manufacturer's specifications. All other emission factors from AP-42 Chapter 3 Section 2, Table 3.2-3.

**Table B.33. - Controlled Compressor Engine Emissions** 

£	Controlled Em	nission Factor <sup>1</sup>	Controlled Emission Rate		
Component	lb/MMBtu	g/bhp-hr	lb/hr	tons/year	
NO <sub>X</sub>	-	1.00	0.88	3.86	
со	-	2.00	1.76	7.72	
VOCs	-	0.70	0.62	2.70	
Formaldehyde	2.05E-02	•	6.74E-02	0.30	
PM <sub>2.5</sub>	9.50E-03	-	3.13E-02	0.14	
PM <sub>10</sub>	9.50E-03	-	3.13E-02	0.14	
PM	9.10E-03	-	2.99E-02	0.13	
SO <sub>2</sub>	5.88E-04	-	1.93E-03	0.01	
CH <sub>4</sub>	0.23	-	0.76	3.31	
N <sub>2</sub> O	1.32E-03	-	4.35E-03	0.02	
CO <sub>2</sub>	-	459.00	404.77	1,772.89	
CO₂e ²	-	-	424.98	1,861.43	

 $<sup>^{1}</sup>$  The emission factors for CO, NOx, and VOC are based on the gram per brake-horsepower-hour (g/bhp-hr) uncontrolled rates. Engines would meet the emission standards of NSPS JJJJ for Non-Emergency Natural Gas Engines. The emission factor CO<sub>2</sub> is based on the manufacturer's specifications. All other emission factors from AP-42 Chapter 3 Section 2, Table 3.2-3.

### Primus Facility: PetroShale US 8H, US12H, & US 13H Production Facility

### **Actual Emission Calculations**

### **Compressor Engine 1**

 $^2$  Global warming potentials obtained from Table A-1 to Subpart 98 - Global Warming Potentials Equation

A-1: CO₂e = ∑GHGi x GWPi

Where:

CO<sub>2</sub>e = Carbon dioxide equivalent (tons/year) GHGi = Mass emissions of each GHG (tons/year)

GWPi = Global warming potential for each GHG (1 for CO<sub>2</sub>; 25 for CH<sub>4</sub>; 298 for N<sub>2</sub>O)

 $^{2}$  Global warming potentials obtained from Table A-1 to Subpart 98 - Global Warming Potentials

Equation A-1: CO<sub>2</sub>e = ∑GHGi x GWPi

Where:

CO<sub>2</sub>e = Carbon dioxide equivalent (tons/year) GHGi = Mass emissions of each GHG (tons/year)

GWPi = Global warming potential for each GHG (1 for CO<sub>2</sub>; 25 for CH<sub>4</sub>; 298 for N<sub>2</sub>O)

Table B.34. - Compressor Engine HAP Emissions

<u></u>	AP-42 Emission Factor 1	Uncontrolled	Emission Rate	Controlled E	Controlled Emission Rate	
Component	lb/MMBtu	lb/hr	tons/year	lb/hr	tons/year	
1,1,2,2-Tetrachloroethane	2.53E-05	8.32E-05	3.65E-04	8.32E-05	3.65E-04	
1,1,2-Trichloroethane	1.53E-05	5.03E-05	2.20E-04	5.03E-05	2.20E-04	
1,3-Butadiene	6.63E-04	2.18E-03	9.55E-03	2.18E-03	9.55E-03	
1,3-Dichloropropene	1.27E-05	4.18E-05	1.83E-04	4.18E-05	1.83E-04	
Acetaldehyde	2.79E-03	9.18E-03	4.02E-02	9.18E-03	4.02E-02	
Acrolein	2.63E-03	8.65E-03	3.79E-02	8.65E-03	3.79E-02	
Benzene	1.58E-03	5.20E-03	2.28E-02	5.20E-03	2.28E-02	
Carbon Tetrachloride	1.77E-05	5.82E-05	2.55E-04	5.82E-05	2.55E-04	
Chlorobenzene	1.29E-05	4.24E-05	1.86E-04	4.24E-05	1.86E-04	
Chloroform	1.37E-05	4.51E-05	1.97E-04	4.51E-05	1.97E-04	
Ethylbenzene	2.48E-05	8.16E-05	3.57E-04	8.16E-05	3.57E-04	
Ethylene Dibromide	2.13E-05	7.01E-05	3.07E-04	7.01E-05	3.07E-04	
Methanol	3.06E-03	1.01E-02	4.41E-02	1.01E-02	4.41E-02	
Methylene Chloride	4.12E-05	1.36E-04	5.94E-04	1.36E-04	5.94E-04	
Naphthalene	9.71E-05	3.19E-04	1.40E-03	3.19E-04	1.40E-03	
PAH	1.41E-04	4.64E-04	2.03E-03	4.64E-04	2.03E-03	
Styrene	1.19E-05	3.92E-05	1.71E-04	3.92E-05	1.71E-04	
Toluene	5.58E-04	1.84E-03	8.04E-03	1.84E-03	8.04E-03	
Vinyl Chloride	7.18E-06	2.36E-05	1.03E-04	2.36E-05	1.03E-04	
Xylene	1.95E-04	6.42E-04	2.81E-03	6.42E-04	2.81E-03	
Total HAPs <sup>2</sup>	3.24E-02	0.11	0.47	0.11	0.47	

<sup>&</sup>lt;sup>1</sup> Emission factors from AP-42 Chapter 3 Section 2, Table 3.2-3.

<sup>&</sup>lt;sup>2</sup> Total HAPs emissions include formaldehyde emissions from Tables B.32 and B.33.

**Table B.35. - Engine Information** 

Parameter	Value
Engine #2 Horsepower (hp)	215
Number of Units	1
Fuel	Natural Gas
Annual Hours of Operation per Unit (hr)	8,760
Fuel Heat Rating (Btu/hr) <sup>1</sup>	1,669,905
Maximum Heat Input (MMBtu/hr)	1.67
Fuel Specific HHV (Btu/scf)	1,020
Fuel Use Rate (scf/hr)	1,637.16
Annual Fuel Consumption (MMBtu/year)	14,628.37
Annual Fuel Consumption (MMSCF/year)	14.34

<sup>&</sup>lt;sup>1</sup> Values from engine manufacturer's specifications.

**Table B.36. - Uncontrolled Compressor Engine Emissions** 

Component	AP-42 Emissio Ib/MMBtu	on Factor <sup>1</sup> g/bhp-hr	Uncontrolled Er lb/hr	nission Rate tons/year
NO <sub>X</sub>	-	27.94	13.24	58.01
со	-	1.40	0.66	2.91
VOCs	-	0.18	0.09	0.37
Formaldehyde	2.05E-02	-	3.42E-02	0.15
PM <sub>2.5</sub>	0.0095	-	1.59E-02	0.07
PM <sub>10</sub>	0.0095	-	1.59E-02	0.07
PM	0.0091	-	1.52E-02	0.07
SO <sub>2</sub>	0.000588	-	9.82E-04	4.30E-03
CH <sub>4</sub>	0.23	_	0.38	1.68
N <sub>2</sub> O	1.32E-03	-	2.21E-03	0.01
CO <sub>2</sub>	110.00	-	183.69	804.56
CO₂e ²	110.00	<i>,,</i> ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	193.95	849.50

<sup>&</sup>lt;sup>1</sup> The emission factors for CO, NOx, and VOC are based on the manufacturer's specifications. All other emission factors from AP-42 Chapter 3 Section 2, Table 3.2-3.

**Table B.37. - Controlled Compressor Engine Emissions** 

6	Controlled En	Controlled Emission Factor 1		mission Rate
Component	lb/MMBtu	g/bhp-hr	lb/hr	tons/year
$NO_X$	-	1.00	0.47	2.08
со	-	2.00	0.95	4.15
VOCs	-	0.70	0.33	1.45
Formaldehyde	2.05E-02	-	3.42E-02	0.15
PM <sub>2.5</sub>	9.50E-03	-	1.59E-02	0.07
PM <sub>10</sub>	9.50E-03	-	1.59E-02	0.07
PM	9.10E-03	-	1.52E-02	0.07
SO <sub>2</sub>	5.88E-04	-	9.82E-04	4.30E-03
CH₄	0.23	-	0.38	1.68
N₂O	1.32E-03	-	2.21E-03	0.01
CO <sub>2</sub>	-	511.00	242.21	1,060.88
CO₂e ²	-	511.00	252.47	1,105.82

 $<sup>^{1}</sup>$  The emission factors for CO, NOx, and VOC are based on the gram per brake-horsepower-hour (g/bhp-hr) uncontrolled rates. Engines would meet the emission standards of NSPS JJJJ for Non-Emergency Natural Gas Engines. The emission factor  $\mathrm{CO}_2$  is based on the manufacturer's specifications. All other emission factors from AP-42 Chapter 3 Section 2, Table 3.2-3.

### Primus Facility: PetroShale US 8H, US12H, & US 13H Production Facility

### **Actual Emission Calculations**

### **Compressor Engine 2**

 $^2$  Global warming potentials obtained from Table A-1 to Subpart 98 - Global Warming Potentials Equation

A-1: CO₂e = ∑GHGi x GWPi

Where:

CO<sub>2</sub>e = Carbon dioxide equivalent (tons/year) GHGi = Mass emissions of each GHG (tons/year)

GWPi = Global warming potential for each GHG (1 for CO<sub>2</sub>; 25 for CH<sub>4</sub>; 298 for N<sub>2</sub>O)

 $^2$  Global warming potentials obtained from Table A-1 to Subpart 98 - Global Warming Potentials

Equation A-1: CO<sub>2</sub>e = ∑GHGi x GWPi

Where:

CO<sub>2</sub>e = Carbon dioxide equivalent (tons/year) GHGi = Mass emissions of each GHG (tons/year)

GWPi = Global warming potential for each GHG (1 for CO<sub>2</sub>; 25 for CH<sub>4</sub>; 298 for N<sub>2</sub>O)

Table B.38. - Compressor Engine HAP Emissions

C	AP-42 Emission Factor 1	Uncontrolled	Emission Rate	Controlled E	Controlled Emission Rate	
Component	lb/MMBtu	lb/hr	tons/year	lb/hr	tons/year	
1,1,2,2-Tetrachloroethane	2.53E-05	4.22E-05	1.85E-04	4.22E-05	1.85E-04	
1,1,2-Trichloroethane	1.53E-05	2.55E-05	1.12E-04	2.55E-05	1.12E-04	
1,3-Butadiene	6.63E-04	1.11E-03	4.85E-03	1.11E-03	4.85E-03	
1,3-Dichloropropene	1.27E-05	2.12E-05	9.29E-05	2.12E-05	9.29E-05	
Acetaldehyde	2.79E-03	4.66E-03	2.04E-02	4.66E-03	2.04E-02	
Acrolein	2.63E-03	4.39E-03	1.92E-02	4.39E-03	1.92E-02	
Benzene	1.58E-03	2.64E-03	1.16E-02	2.64E-03	1.16E-02	
Carbon Tetrachloride	1.77E-05	2.96E-05	1.29E-04	2.96E-05	1.29E-04	
Chlorobenzene	1.29E-05	2.15E-05	9.44E-05	2.15E-05	9.44E-05	
Chloroform	1.37E-05	2.29E-05	1.00E-04	2.29E-05	1.00E-04	
Ethylbenzene	2.48E-05	4.14E-05	1.81E-04	4.14E-05	1.81E-04	
Ethylene Dibromide	2.13E-05	3.56E-05	1.56E-04	3.56E-05	1.56E-04	
Methanol	3.06E-03	5.11E-03	2.24E-02	5.11E-03	2.24E-02	
Methylene Chloride	4.12E-05	6.88E-05	3.01E-04	6.88E-05	3.01E-04	
Naphthalene	9.71E-05	1.62E-04	7.10E-04	1.62E-04	7.10E-04	
PAH	1.41E-04	2.35E-04	1.03E-03	2.35E-04	1.03E-03	
Styrene	1.19E-05	1.99E-05	8.70E-05	1.99E-05	8.70E-05	
Toluene	5.58E-04	9.32E-04	4.08E-03	9.32E-04	4.08E-03	
Vinyl Chloride	7.18E-06	1.20E-05	5.25E-05	1.20E-05	5.25E-05	
Xylene	1.95E-04	3.26E-04	1.43E-03	3.26E-04	1.43E-03	
Total HAPs <sup>2</sup>	3.24E-02	5.41E-02	0.24	5.41E-02	0.24	

<sup>&</sup>lt;sup>1</sup> Emission factors from AP-42 Chapter 3 Section 2, Table 3.2-3.

<sup>&</sup>lt;sup>2</sup> Total HAPs emissions include formaldehyde emissions from Tables B.36 and B.37.

### Primus Facility: PetroShale US 8H, US12H, & US 13H Production Facility **Actual Emission Calculations**

#### **Produced Gas**

Table B.39. - Produced Gas Sent to Flare Information

Parameter	Value
Produced Gas Volume, MCFD	162.22
Produced Gas Volume, scf/hr	6,759.29
Produced Gas Heating Value, Btu/scf	1,535.40
Total Gas Volume per Hour, 10 <sup>6</sup> scf/hr	0.01

Note: The wells are connected to a gas sales pipeline. The flared gas volumes for the US12H and US13H wells are based on the percentage of gas flared for the US8H well. Heating value based on gas analysis dated March 6, 2017 (included in this appendix).

Table B.40. - Produced Gas Sent to Flare Criteria Pollutant Emissions

Pollutant	Emission Factor, lb/10 <sup>6</sup> scf	Emission Factor, lb/MMBtu	Emissions, lb/hr	Emissions, tpy
PM <sub>10</sub> 1	7.60	7.451E-03	0.08	0.34
PM <sub>2.5</sub> <sup>1</sup>	7.60	7.451E-03	0.08	0.34
SO <sub>2</sub>	0.60	5.882E-04	0.01	0.03
NO <sub>x</sub>	-	0.07	0.71	3.09
со	-	0.31	3.22	14.09
voc	5.50	5.392E-03	0.06	0.25

Note: SO, and VOC emissions are calculated using fuel in Table B.36. Emission factors for NOX and CO from AP-42, Section 13.5, Industrial Flares, Table 13.5-1, and calculated using the equation below:

$$NO_{x} \ and \ CO, \\ \frac{lb}{hr} = \left[HHV, \\ \frac{\text{Btu}}{\text{scf}}\right] \times \left[\frac{\text{scf}}{\text{hr}}\right] \times \left[EF, \\ \frac{lb}{\text{MMBtu}}\right] \times \left[\frac{\text{MMBtu}}{10^{6}Btu}\right]$$
 Emission factors for PM<sub>10</sub>, PM<sub>2.5</sub>, VOC, and SO<sub>2</sub> from AP-42, Section 1.4, Natural Gas Combustion, Table 1.4-2, calculated using the equation below:

$$PM_{10}, PM_{2.5}, \frac{lb}{hr} = \begin{bmatrix} Total\ gas\ volume, \frac{10^6\ scf}{hr} \end{bmatrix} \times \begin{bmatrix} EF, \frac{lb}{10^6\ scf} \end{bmatrix} \times \frac{Produced\ Gas\ heating\ value\ \left[\frac{btu}{scf}\right]}{Average\ NG\ heating\ value\ (1,020)} \begin{bmatrix} \frac{btu}{scf} \end{bmatrix}$$

$$^{1}\text{PM}_{10} \text{ and PM}_{25} \text{ are assumed to equal total particulate\ matter.}$$

Table B.41. - Produced Gas Sent to Flare Hazardous Air Pollutant Emissions

Pollutant	Emission Factor, lb/10 <sup>6</sup> scf	Emission Rate, lb/hr	Emission Rate, tpy
2-Methylnaphthalene	2.40E-05	2.44E-07	1.07E-06
3-Methylchloranthrene	1.80E-06	1.83E-08	8.02E-08
7,12-Dimethylbenz(a)anthracene	1.60E-05	1.63E-07	7.13E-07
Acenaphthene	1.80E-06	1.83E-08	8.02E-08
Anthracene	2.40E-06	2.44E-08	1.07E-07
Benz(a)anthracene	1.80E-06	1.83E-08	8.02E-08
Benzene	2.10E-03	2.14E-05	9.36E-05
Benzo(a)pyrene	1.20E-06	1.22E-08	5.35E-08
Benzo(b)fluoranthene	1.80E-06	1.83E-08	8.02E-08
Benzo(g,h,i)perylene	1.20E-06	1.22E-08	5.35E-08
Benzo(k)fluoranthene	1.80E-06	1.83E-08	8.02E-08
Crysene	1.80E-06	1.83E-08	8.02E-08
Dibenzo(a,h)anthracene	1.20E-06	1.22E-08	5.35E-08
Dichlorobenzene	1.20E-03	1.22E-05	5.35E-05
Fluoranthene	3.00E-06	3.05E-08	1.34E-07
Fluorene	2.80E-06	2.85E-08	1.25E-07
Formaldehyde	7.50E-02	7.63E-04	3.34E-03
n-Hexane	1.80E+00	1.83E-02	8.02E-02
indeno(1,2,3-cd)pyrene	1.80E-06	1.83E-08	8.02E-08
Naphthalene	6.10E-04	6.21E-06	2.72E-05
Phenanathrene	1.70E-05	1.73E-07	7.58E-07
Pyrene	5.00E-06	5.09E-08	2.23E-07
Toluene	3.40E-03	3.46E-05	1.52E-04
Total:		0.02	80.0

Note: Based on EPA AP-42, Section 1.4, Natural Gas Combustion (Table 1.4-3).

Table B.42. - Produced Gas Sent to Flare Greenhouse Gas Emissions

Pollutant	Emission Factor, kg/MMBtu	Emission Factor, lb/MMBtu	Emissions, lb/hr	Emissions, tpy
CO₂	53.06	116.98	1,214.02	5,317.39
CH₄	1.00E-03	2.20E-03	0.02	0.10
N <sub>2</sub> O	1.00E-04	2.20E-04	0.00	0.01
		Total CO₂e:	1,215.27	5,322.88

Note: Emission factors from 40 CFR Part 98 Subpart C, Table C-1 and C-2. Converted from kilograms to pounds. Global warming potentials for CH<sub>4</sub> and N<sub>2</sub>O are 25 and 298, respectively.

Table B.43. - Flare and Produced Gas Information

Parameter	Value
Flare Destruction Efficiency, %	98
Specific Gravity of Produced Gas	0.92
Molecular Weight of Produced Gas, lb/lb-mole	26.53
HHV of Produced Gas, Btu/scf	1,535.40
Volume of Produced Gas to Flare, MCFD	162.22
Volume of Produced Gas to Flare, scf/hr	6,759.29

Note: Heating value based on gas analysis dated March 6, 2017 (included in this appendix). Molecular weight of gas calculated by multiplying the specific gravity by the molecular weight of air (28.96443 lb/lb-mole).

Table B.44. - Uncontrolled and Controlled Produced Gas Emissions

Pollutant	Gas Ana	Gas Analysis Data		Uncontrolled		Controlled		Total Controlled Emissions	
	Weight Percent	Mole Percent	lb/hr	tpy	lb/hr	tpy	Combustion Emissions, tpy	lb/hr	tpy
voc	37.76	-	178.69	782.65	3.57	15.65	0.25	3.63	15.90
Total CO₂e	-	-	4,066.53	17,811.42	86.20	377.56	5,322.88	1,301.47	5,700.44
CH <sub>4</sub>	34.33	-	162.46	711.59	3.25	14.23	0.10	3.27	14.33
CO <sub>2</sub>	1.05	_	4.97	21.77	4.97	21.77	5,317.39	1,218.99	5,339.16
N <sub>2</sub> O	-	-	_	-	_	-	0.01	2.29E-03	0.01
Total HAPs	0.74	-	3.50	15.31	0.07	0.31	0.08	0.09	0.39
Benzene	0.06	-	0.30	1.31	0.01	0.03	9.36E-05	0.01	0.03
Toluene	0.32	-	1.52	6.67	0.03	0.13	1.52E-04	0.03	0.13
Ethylbenzene	4.26E-03	-	0.02	0.09	4.03E-04	1.77E-03	-	4.03E-04	1.77E-03
Xylene	0.02	_	0.08	0.34	1.57E-03	0.01	-	1.57E-03	0.01
n-C6	0.74	-	3.50	15.31	0.07	0.31	0.08	0.09	0.39
2,2,4-Trimethylpentane	0.05	-	0.26	1.14	0.01	0.02	-	0.01	0.02
H <sub>2</sub> S	0.00	_	0.00	0.00	0.00	0.00	0.00	0.00	0.00
PM <sub>10</sub>	-	-	-	-			0.34	0.08	0.34
PM <sub>2.5</sub>	-	-	_	-			0.34	0.08	0.34
SO <sub>2</sub>	-	-	-	-			0.03	0.01	0.03
NO <sub>X</sub>	-	-	_	-			3.09	0.71	3.09
со	-	-	-	-			14.09	3.22	14.09

Note: Speciated HAPs are proportionally based on the speciated HAPs in the E&P TANK v2.0 flashed gas results. Emission factors for NO<sub>X</sub> and CO from AP-42, Chapter 13.5, Industrial Flares, Table 13.5-1. Emissions in tons per year assume flaring 8,760 hours per year. Uncontrolled emissions for VOC, HAPs, and H<sub>2</sub>S were calculated using the following equation:

$$VOC, HAPs, and \ H_2S \ uncontrolled \ emission \ rate, \\ \frac{lb}{hr} = Molecular \ weight, \\ \frac{lb}{lb-mole} \times \\ \frac{1 \ lb-mole}{379 \ scf} \times Volume \ of \ gas, \\ \frac{scf}{hr} \times Weight \ Percent \ School \ School$$

### **APPENDIX C**

**Supporting Documentation** 

### QUESTAR ENERGY SERVICES

### 1210 D. Street, Rock Springs, Wyoming 82901 (307) 352-7292

US 8H LIMS ID: N/A Description: Analysis Date/Time: 3/6/2017 12:57 PM Field: Mckenzie Analyst Initials: JFL ML#: Petro Shale Sample Temperature: 89 GC Method: Quesliql GPA 2186

Sample Pressure: 32 Data File: QPC21.D Date Sampled: 3/2/2017 Instrument ID: 1

Component	Mol%	Wt%	LV%
Methane	0.2204	0.0316	0.0747
Ethane	2.4328	0.6532	1.3013
Propane	6.2208	2.4495	3.4279
Isobutane	1.6599	0.8615	1.0864
n-Butane	7.7361	4.0153	4.8783
Neopentane	0.0321	0.0207	0.0246
Isopentane	3.0908	1.9913	2.2609
n-Pentane	6.2262	4.0114	4.5141
2,2-Dimethylbutane	0.0446	0.0343	0.0373
2,3-Dimethylbutane	0.6316	0.4861	0.5178
2-Methylpentane	2.2666	1.7442	1.8818
3-Methylpentane	1.3808	1.0626	1.1271
n-Hexane	4.5613	3.5100	3.7516
Heptanes	15.1972	13.0228	12.6496
Octanes	9.5641	9.5415	9.2495
Nonanes	8.8266	9.6931	9.1966
Decanes plus	29.8220	46.8471	43.9999
Nitrogen	0.0686	0.0172	0.0151
Carbon Dioxide	0.0163	0.0064	0.0056
Total	100.0000	100.0000	100.0000

Units

### Calculated Global Properties

Avg Molecular Weight	111.9861	gm/mole
Pseudocritical Pressure	414.46	psia
Pseudocritical Temperatu	524.50	degF
Specific Gravity	0.70979	gm/ml
Liquid Density	5.9174	lb/gal
Liquid Density	248.53	lb/bbl
Specific Gravity	2.7078	air=1
SCF/bbl	844.11	SCF/bbl
SCF/gal	20.0979	SCF/gal
MCF/gal	0.0201	MCF/gal
gal/MCF	49.778	gal/MCF
Net Heating Value	3917.1	BTU/SCF at 60°F
Net Heating Value	13188.4	BTU/lb at 60°F
Gross Heating Value	4239.2	BTU/SCF at 60°F
Gross Heating Value	14244.7	BTU/lb at 60°F
Gross Heating Value	82736.7	BTU/gal at 60°F
API Gravity	67.9	
MON	46.2	
RON	47.7	
TVP	53.646	psia

Page #1 C-10

Component	Mol%	Wt%	LV%
Benzene	0.5895	0.4112	0.3299
Toluene	0.9843	0.8098	0.6592
Ethylbenzene	0.3646	0.3457	0.2814
M&P Xylene	1.3430	1.2732	1.0401
O-Xylene	0.4030	0.3821	0.3066
2,2,4-Trimethylpentane	1.0350	1.0558	1.0404

Data File: US 8H Page #2

GRI E&P TANK INFORI	MATION		
Component	Mol%	Wt%	LV%
H2S	ND	ND	ND
O2	ND	ND	ND
CO2	0.0163	0.0064	0.0056
N2	0.0686	0.0172	0.0151
C1	0.2204	0.0316	0.0747
C2	2.4328	0.6532	1.3013
C3	6.2208	2.4495	3.4279
IC4	1.6599	0.8615	1.0864
NC4	7.7682	4.0360	4.9029
IC5	3.0908	1.9913	2.2609
NC5	6.2262	4.0114	4.5141
Hexanes	4.3236	3.3272	3.5640
Heptanes	14.6077	12.6116	12.3197
Octanes	7.5448	7.6759	7.5499
Nonanes	6.7160	7.6921	7.5685
Benzene	0.5895	0.4112	0.3299
Toluene	0.9843	0.8098	0.6592
E-Benzene	0.3646	0.3457	0.2814
Xylene	1.7460	1.6553	1.3467
n-C6	4.5613	3.5100	3.7516
2,2,4-Trimethylpentane	1.0350	1.0558	1.0404
C10 Plus			
C10 Mole %	29.8220	46.8471	43.9999
Molecular Wt.	177.6260		
Specific Gravity	0.7548		
Total	100.00	100.00	100.00

# QUESTAR ENERGY SERVICES

# 1210 D. Street, Rock Springs, Wyoming 82901 (307) 352-7292

Description:	US 8H	Company:	Petro Shale
Field:	Mckenzie	Data File:	002393.D

Meter Number: G.C. Method: GAS EXTENDED.M

Analysis Date/Time: 06-Mar-17, 10:30:28 GPA Method GPA 2286
Date Sampled: 2-Mar-17 Sampled By: WD
Sample Temperature: 89 Analyst Initials: JFL

Sample Pressure: 32

Component	Mol%	Wt%	LV%
Methane	56.5905	34.3070	44.5929
Ethane	21.8904	24.8738	27.2899
Propane	11.5154	19.1886	14.7601
Isobutane	1.2456	2.7359	1.8955
n-Butane	3.6969	8.1197	5.4216
Neopentane	0.0113	0.0308	0.0201
Isopentane	0.6312	1.7210	1.0747
n-Pentane	0.9382	2.5579	1.5806
2,2-Dimethylbutane	0.0047	0.0153	0.0091
2,3-Dimethylbutane	0.0461	0.1503	0.0879
2-Methylpentane	0.1564	0.5092	0.3018
3-Methylpentane	0.0941	0.3064	0.1786
n-Hexane	0.2267	0.7383	0.4336
Heptanes	0.4024	1.4357	0.7554
Octanes	0.0444	0.1897	0.1017
Nonanes	0.0213	0.0863	0.0387
Decanes plus	0.0052	0.0282	0.0150
Nitrogen	1.8481	1.9563	0.9425
Carbon Dioxide	0.6311	1.0496	0.5003
Oxygen	ND	ND	ND
Hydrogen Sulfide	ND	ND	ND
Total	100.0000	100.0000	100.0000
Calculated Global Prope	erties Units		

rotai	100.0000	100.000	100.000
Calculated Global Proper	ties Units		
Gross BTU/Real CF	1535.4	BTU/SCF at 60°F and 14	4.73 psia
Sat.Gross BTU/Real CF	1510.2	BTU/SCF at 60°F and14	4.73 psia
Gas Compressibility (Z)	0.9941		
Specific Gravity	0.9160	air=1	
Avg Molecular Weight	26.463	gm/mole	
Propane GPM	3.155942	gal/MCF	
Butane GPM	1.569078	gal/MCF	
Gasoline GPM	0.947957	gal/MCF	
26# Gasoline GPM	2.114046	gal/MCF	
Total GPM	11.858136	gal/MCF	
Base Mol%	99.052	%v/v	

H2S detection limit 100 ppm (+/-)

Component	Mol%	Wt%	LV%
Benzene	0.0235	0.0693	0.0306
Toluene	0.0248	0.0864	0.0386
Ethylbenzene	0.0086	0.0346	0.0155
M&P Xylene	0.0038	0.0153	0.0069
O-Xylene	0.0082	0.0330	0.0145
2,2,4-Trimethylpentane	0.0215	0.0929	0.0503
Cyclopentane	0.0000	0.0000	0.0000
Cyclohexane	0.0384	0.1220	0.0607
Methylcyclohexane	0.0440	0.1632	0.0822
Description:	US 8H		

### GRI GlyCalc Information

Component	Mol%	Wt%	LV%	
Carbon Dioxide	0.6311	1.0496	0.5003	0000000000
Hydrogen Sulfide	ND	ND	ND	
Nitrogen	1.8481	1.9563	0.9425	
Methane	56.5905	34.3070	44.5929	
Ethane	21.8904	24.8738	27.2899	
Propane	11.5154	19.1886	14.7601	
Isobutane	1.2456	2.7359	1.8955	
n-Butane	3.7082	8.1197	5.4216	
Isopentane	0.6312	1.7518	1.0948	
n-Pentane	0.9382	2.5579	1.5806	
Cyclopentane	0.0000	0.0000	0.0000	
n-Hexane	0.2267	0.7383	0.4336	
Cyclohexane	0.0384	0.1220	0.0607	
Other Hexanes	0.3013	0.9812	0.5774	
Heptanes	0.2502	0.9019	0.4930	
Methylcyclohexane	0.0440	0.1632	0.0822	
2,2,4 Trimethylpentane	0.0215	0.0929	0.0503	
Benzene	0.0235	0.0693	0.0306	
Toluene	0.0248	0.0864	0.0386	
Ethylbenzene	0.0086	0.0346	0.0155	
Xylenes	0.0120	0.0483	0.0214	
C8+ Heavies	0.0503	0.2213	0.1185	
Subtotal	100.0000	100.0000	100.0000	
Oxygen	ND	ND	ND	
Total	100.0000	100.0000	100.0000	

## Petroshale (US), Inc. PETROSHALE US 8H Natural Gas Analysis Summary

#### **Tank Vapor Compositional Analysis**

Species	Formula	MW	Mole %	Mole Fraction	Weight %
Hydrogen sulfide	H <sub>2</sub> S	34.08	0.0000	0.0000	0.000
Oxygen	O <sub>2</sub>	32.00	0.0000	0.0000	0.000
Nitrogen	N <sub>2</sub>	28.01	1.3431	0.0185	1.958
Carbon dioxide	CO <sub>2</sub>	44.01	0.6311	0.0063	1.050
Methane	C1	16.04	56.5905	0.5659	34.335
Ethane	C2	30.07	21.8904	0.2189	24.894
Propane	C3	44.10	11.5154	0.1152	19.204
iso-Butane	iC4	58.12	1.2456	0.0125	2.738
n-Butane	nC4	58.12	3.7477	0.0375	8.238
iso-Pentane	iC5	72.15	0.6425	0.0064	1.753
n-Pentane	nC5	72.15	1.1887	0.0119	3.244
Cyclopentane	C <sub>5</sub> H <sub>10</sub>	70.13	0.0000	0.0000	0.000
C6 Mix	C6	86.18	0.0000	0.0000	0.000
n-Hexane	C <sub>6</sub> H <sub>14</sub>	86.18	0.2267	0.0023	0.739
Cyclohexane	C <sub>6</sub> H <sub>12</sub>	84.16	0.0000	0.0000	0.000
Hexanes	C6	86.18	0.0000	0.0000	0.000
Benzene	C <sub>6</sub> H <sub>6</sub>	78.11	0.0000	0.0000	0.000
Heptanes	C7	100.20	0.4024	0.0040	1.525
Methylcyclohexane	C <sub>7</sub> H <sub>14</sub>	98.19	0.0000	0.0000	0.000
Toluene	C <sub>7</sub> H <sub>8</sub>	92.14	0.0000	0.0000	0.000
Octanes	C8	114.23	0.0444	0.0004	0.192
Ethylbenzene	C <sub>8</sub> H <sub>10</sub>	106.17	0.0000	0.0000	0.000
Xylenes	C <sub>8</sub> H <sub>10</sub>	106.17	0.0000	0.0000	0.000
2,2,4-Trimethylpentane	C <sub>8</sub> H <sub>18</sub>	114.23	0.0000	0.0000	0.000
Nonanes	C9	128.26	0.0213	0.0002	0.103
Pseudo Comp1	-	102.91	0.0000	0.0000	0.000
Pseudo Comp2	-	121.00	0.0000	0.0000	0.000
Pseudo Comp3	-	134.00	0.0000	0.0000	0.000
Pseudo Comp4	-	152.95	0.0000	0.0000	0.000
Pseudo Comp5	-	217.22	0.0000	0.0000	0.000
Decanes+	C10+	142.29	0.0052	0.0001	0.028
Total:			100.000	1.000	100.000

# $\textit{CC}_{\textit{Mixture}} = \frac{\sum_{i=1}^{\# \ of \ \textit{Components}} (n \times \textit{AW}_{\textit{Carbon}} \times \textit{Xmi})}{\sum_{i=1}^{\# \ of \ \textit{Components}} (\textit{MWi} \times \textit{Xmi})}$

Parameter	Mole %	Mole Fraction	Weight %
Total Methane (CH <sub>4</sub> )	56.59	0.566	34.33
Total Carbon Dioxide (CO <sub>2</sub> )	0.63	0.006	1.05
Total Hazardous Air Pollutants (HAPs)	0.23	0.002	0.74
Total Volatile Organic Compounds (VOCs)	19.04	0.190	37.76
Total Hydrogen Sulfide (H <sub>2</sub> S)	0.00	0.00	0.00

### Petroshale (US), Inc. **PETROSHALE US 8H E&P TANK Tank Vapor Analysis**

#### **Tank Vapor Compositional Analysis**

Species	Formula	MW	Mole %	Mole Fraction	Weight %
Hydrogen sulfide	H <sub>2</sub> S	34.08	0.0000	0.0000	0.000
Oxygen	O <sub>2</sub>	32.00	0.0000	0.0000	0.000
Nitrogen	N <sub>2</sub>	28.01	0.6277	0.0063	0.391
Carbon dioxide	CO <sub>2</sub>	44.01	0.1491	0.0015	0.146
Methane	C1	16.04	2.0167	0.0202	0.720
Ethane	C2	30.07	22.2371	0.2224	14.872
Propane	C3	44.10	49.7363	0.4974	48.779
iso-Butane	iC4	58.12	5.1150	0.0512	6.612
n-Butane	nC4	58.12	14.3036	0.1430	18.490
iso-Pentane	iC5	72.15	1.7519	0.0175	2.811
n-Pentane	nC5	72.15	2.5393	0.0254	4.075
Cyclopentane	C <sub>5</sub> H <sub>10</sub>	70.13	0.0000	0.0000	0.000
C6 Mix	C6	86.18	0.0000	0.0000	0.000
n-Hexane	C <sub>6</sub> H <sub>14</sub>	86.18	0.4922	0.0049	0.943
Cyclohexane	C <sub>6</sub> H <sub>12</sub>	84.16	0.000.0	0.0000	0.000
Hexanes	C6	86.18	0.4879	0.0049	0.935
Benzene	C <sub>6</sub> H <sub>6</sub>	78.11	0.0606	0.0006	0.105
Heptanes	C7	100.20	0.0000	0.0000	0.000
Methylcyclohexane	C <sub>7</sub> H <sub>14</sub>	98.19	0.0000	0.0000	0.000
Toluene	C <sub>7</sub> H <sub>8</sub>	92.14	0.0261	0.0003	0.053
Octanes	C8	114.23	0.0000	0.0000	0.000
Ethylbenzene	C <sub>8</sub> H <sub>10</sub>	106.17	0.0030	0.0000	0.007
Xylenes	C <sub>8</sub> H <sub>10</sub>	106.17	0.0117	0.0001	0.028
2,2,4-Trimethylpentane	C <sub>8</sub> H <sub>18</sub>	114.23	0.0359	0.0004	0.091
Nonanes	C9	128.26	0.0000	0.0000	0.000
Pseudo Comp1	-	102.91	0.3782	0.0038	0.866
Pseudo Comp2	-	121.00	0.0248	0.0002	0.067
Pseudo Comp3	-	134.00	0.0028	0.0000	0.008
Pseudo Comp4	-	152.95	0.0002	0.0000	0.001
Pseudo Comp5	-	217.22	0.0000	0.0000	0.000
Decanes+	C10+	142.29	0.0000	0.0000	0.000
Total:	100.000	1.000	100.000		

Total:

Note: Tank vapor compositional analysis from E&P TANK modeling run.

Tank Vapor Analysis Summary  $CC_{Mixture} = \frac{\sum_{i=1}^{\# \ of \ Components} (n \times AW_{Carbon} \times Xmi)}{\sum_{i=1}^{\# \ of \ Components} (MWi \times Xmi)}$ 

Parameter	Mole %	Mole Fraction	Weight %
Total Methane (CH <sub>4</sub> )	2.02	0.020	0.72
Total Carbon Dioxide (CO₂)	0.15	0.001	0.15
Total Hazardous Air Pollutants (HAPs)	0.63	0.006	1.23
Total Volatile Organic Compounds (VOCs)	74.97	0.750	83.87
Total Hydrogen Sulfide (H <sub>2</sub> S)	0.00	0.00	0.00

```
**************************
* Project Setup Information
**************
Project File : C:\Documents and Settings\AirQuality\Desktop\Entire Primus Facility PTE version 2.0
Flowsheet Selection : Oil Tank with Separator
Calculation Method : RVP Distillation
Control Efficiency : 98.0%
Control Efficiency : 98.0%
Known Separator Stream : Low Pressure Oil
Entering Air Composition : No
Filed Name
                   : Antelope
Well Name
Well ID
                   : Primus Facility
                   : PetroShale US8H, 12H, & 13H
: Entire Primus Facility PTE
Permit Number
                   : 2019.10.23
**************************
* Data Input
*******************************
Separator Pressure : 32.00[psig]
Separator Temperature : 89.00[F]
Ambient Pressure : 14.70[psia]
Ambient Temperature : 43.40[F]
C10+ SG
                   : 0.7548
C10+ MW
                    : 177.626
-- Low Pressure Oil ------
 No. Component
                       mol %
  1
       H2S
                         0.0000
       02
                         0.0000
  2
       CO2
  3
                         0.0163
  4
      N2
                         0.0686
  5 C1
                         0.2204
  6 C2
7 C3
8 i-C4
                         2.4328
                         6.2209
                        1.6599
  9
      n-C4
                        7.7683
  10 i-C5
                        3.0908
                        6.2263
      n-C5
  11
  12
       C6
                         4.3237
  13
      C7
                       14.6079
                        7.5449
  14 C8
  15
     C9
                         6.7161
     C10+
Benzene
Toluene
  16
                       29.8224
  17
                       0.5895
0.9843
  18
     E-Benzene
Xylenes
n-C6
  19
                       0.3646
                        1.7460
  20
  21
       n-C6
                         4.5613
       224Trimethylp
  22
                         1.0350
-- Sales Oil -----
Production Rate : 2053.5[bb1/day]
Days of Annual Operation : 365 [days/year]
API Gravity : 67.9
Reid Vapor Pressure : 7.60[psia]
*****************************
    Calculation Results
*************************
-- Emission Summary ------
               Uncontrolled Uncontrolled Controlled Controlled
```

Total HAPs Total HC VOCs, C2+ VOCs, C3+	[ton/yr] 54.820 4765.999 4736.507 4126.635	[1b/hr] 12.516 1088.128 1081.394 942.154	1.09 95.3	320 730	[1b/hr] 0.250 21.763 21.628 18.843		
V003, C31	4120.033	J42.134	02.	,,,,	10.045		
Uncontrolled Recov	-						
Vapor	214.4400	[MSCFD]					
HC Vapor GOR	212.9700 104.43	[MSCFD] [SCF/bb1]	Ī				
OOL	104.45	[SCE/DDI]					
Emission Compos	ition						
No Component	Uncontrolled			rolled	Controlle	ed	
1 1100	[ton/yr]	[lb/hr]		ı/yr]	[lb/hr]		
1 H2S 2 O2	0.000 0.000	0.000 0.000	0.00		0.000 0.000		
3 CO2	5.983	1.366	5.98		1.366		
4 N2	16.028	3.659	16.0		3.659		
5 C1	29.491	6.733	0.59	90	0.135		
6 C2	609.873	139.240	12.3	L97	2.785		
7 C3	2154.595	491.917	43.0		9.838		
8 i-C4	368.817	84.205	7.3		1.684		
9 n-C4	1055.908	241.075	21.3		4.821		
10 i-C5 11 n-C5	150.882 215.335	34.448 49.163	3.00 4.30		0.689 0.983		
12 C6	50.780	11.594	1.0		0.232		
13 C7	60.846	13.892	1.2		0.278		
14 C8	10.500	2.397	0.23		0.048		
15 C9	3.516	0.803	0.0	70	0.016		
16 C10+	0.633	0.145	0.03	13	0.003		
17 Benzene	4.827	1.102	0.09		0.022		
18 Toluene	2.451	0.560	0.04		0.011		
<pre>19 E-Benzene 20 Xylenes</pre>	0.321	0.073 0.302	0.00		0.001 0.006		
21 n-C6	1.321 41.941	9.576	0.02		0.000		
22 224Trimethylp		0.904	0.0		0.018		
Total	4788.007	1093.152			21.863		
Stream Data		LP Oil	71b 0:		Eleck Co.	WCC Coo	Mahal Maississa
No. Component	MW	mol %	mol %	l Sale Oil mol %	mol %	mol %	Total Emissions mol %
1 H2S	34.80	0.0000	0.0000	0.0000	0.0000		0.0000
2 02	32.00	0.0000	0.0000	0.0000	0.0000		0.0000
3 CO2	44.01	0.0163	0.0074	0.0000	0.3604	0.0731	0.1317
4 N2	28.01	0.0686	0.0045	0.0000	2.5417	0.0449	0.5541
5 C1	16.04	0.2204	0.0451	0.0000	6.9884	0.4459	1.7802
6 C2	30.07	2.4328	1.5442	0.0012	36.7372	15.2616	19.6415
7 C3	44.10	6.2209	5.5176	0.4140	33.3698	50.8914	47.3179
8 i-C4 9 n-C4	58.12 58.12	1.6599 7.7683	1.6133 7.6800	1.0262 6.3801	3.4599 11.1789	6.8329 19.2362	6.1450 17.5930
10 i-C5	72.15	3.0908	3.1298	3.2414	1.5855	2.1378	2.0252
11 n-C5	72.15	6.2263	6.3282	6.6977	2.2911	3.0438	2.8903
12 C6	86.16	4.3237	4.4237	4.8519	0.4624	0.6170	0.5854
13 C7	100.20	14.6079	14.9742	16.5861	0.4650	0.6440	0.6075
14 C8	114.23	7.5449	7.7386	8.5980	0.0673	0.0978	0.0916
15 C9	128.28	6.7161	6.8896	7.6612	0.0185	0.0300	0.0277
16 C10+	177.63	29.8224	30.5948	34.0357	0.0021	0.0038	0.0034
17 Benzene 18 Toluene	78.11 92.13	0.5895 0.9843	0.6036 1.0093	0.6643 1.1197	0.0470 0.0195	0.0631 0.0274	0.0598 0.0258
19 E-Benzene	106.17	0.3646	0.3740	0.4157	0.0193	0.0274	0.0029
20 Xylenes	106.17	1.7460	1.7910	1.9910	0.0087	0.0129	0.0120
21 n-C6	86.18	4.5613	4.6699	5.1392	0.3689	0.4976	0.4713
22 224Trimethylp	114.24	1.0350	1.0611	1.1765	0.0257	0.0356	0.0336
мw		111 00	113.84	101 05	40.41	47.89	16 37
mw Stream Mole Ra	tio	111.98 1.0000	0.9748	121.25 0.8762	0.0252	0.0986	46.37 0.1238
Heating Value	[BTU/SCF]		0.0730	0.0702	2268.06	2715.46	2624.21
Gas Gravity	[Gas/Air				1.40	1.65	1.60

Bubble Pt. @ 100F	[psia]	47.50	29.98	8.22
RVP @ 100F	[psia]	25.93	20.86	7.59
Spec. Gravity @ 100F		0.668	0.670	0.677

```
**************************
* Project Setup Information
**************
Project File : C:\Documents and Settings\AirQuality\Desktop\Entire Primus Facility Actual Emissions
Flowsheet Selection : Oil Tank with Separator
Calculation Method : RVP Distillation
Control Efficiency : 98.0%
Control Efficiency : 98.0%
Known Separator Stream : Low Pressure Oil
Entering Air Composition : No
                  : Antelope
Filed Name
Well Name
Well ID
                  : Primus Facility
                  : PetroShale US8H, 12H, & 13H
Permit Number
                  : Entire Primus Facility Actual Emissions
                  : 2019.10.23
*************************
* Data Input
*******************************
Separator Pressure : 32.00[psig]
Separator Temperature : 89.00[F]
Ambient Pressure : 14.70[psia]
Ambient Temperature : 43.40[F]
C10+ SG
                 : 0.7548
C10+ MW
                  : 177.626
-- Low Pressure Oil ------
 No. Component mol % 0.0000
  1
      H2S
                       0.0000
      02
C02
                       0.0000
  2
  3
                       0.0163
     N2
  4
                      0.0686
  5 C1
                      0.2204
  6 C2
7 C3
8 i-C4
                      2.4328
                       6.2209
                      1.6599
  9
     n-C4
                      7.7683
  10 i-C5
                      3.0908
                      6.2263
     n-C5
  11
  12
       C6
                       4.3237
     C7
  13
                     14.6079
  14 C8
                      7.5449
  15 C9
                      6.7161
  16 C10+
17 Benzene
18 Toluene
                     29.8224
                     0.5895
0.9843
     E-Benzene
Xylenes
                     0.3646
  19
                      1.7460
  20
  21
       n-C6
                       4.5613
       224Trimethylp
  22
                       1.0350
-- Sales Oil -----
Production Rate : 1327[bbl/day]
Days of Annual Operation : 365 [days/year]
API Gravity : 67.9
Reid Vapor Pressure : 7.60[psia]
*******************************
   Calculation Results
*************************
-- Emission Summary ------
              Uncontrolled Uncontrolled Controlled Controlled
```

Total HAPs Total HC VOCs, C2+ VOCs, C3+	[ton/yr] 35.420 3079.622 3060.566 2666.487	[1b/hr] 8.087 703.110 698.759 608.787	[to: 0.70 61.5 61.2 53.3	592 211	[1b/hr] 0.162 14.062 13.975 12.176		
Umanahan 11 ad Danas	T						
Uncontrolled Recov Vapor	138.5600	[MSCFD]					
HC Vapor	137.6100	[MSCFD]					
GOR	104.42	[SCF/bb1]	]				
Emission Compos							
No Component	Uncontrolled			rolled	Controlle	ed	
1 1100	[ton/yr]	[lb/hr] 0.000		1/yr]	[lb/hr] 0.000		
1 H2S 2 O2	0.000 0.000	0.000	0.00		0.000		
3 CO2	3.866	0.883	3.86		0.883		
4 N2	10.357	2.365	10.3		2.365		
5 C1	19.056	4.351	0.38		0.087		
6 C2	394.078	89.972	7.88	32	1.799		
7 C3	1392.224	317.859	27.8	344	6.357		
8 i-C4	238.317	54.410	4.76		1.088		
9 n-C4	682.291	155.774	13.6		3.115		
10 i-C5	97.495	22.259	1.95		0.445		
11 n-C5 12 C6	139.142 32.812	31.768 7.491	2.78 0.65		0.635 0.150		
13 C7	39.317	8.976	0.78		0.180		
14 C8	6.785	1.549	0.13		0.031		
15 C9	2.272	0.519	0.04		0.010		
16 C10+	0.409	0.093	0.00	8	0.002		
17 Benzene	3.119	0.712	0.06	52	0.014		
18 Toluene	1.584	0.362	0.03		0.007		
19 E-Benzene	0.208	0.047	0.00		0.001		
20 Xylenes 21 n-C6	0.853	0.195	0.01		0.004 0.124		
22 224Trimethylp	27.101 2.558	6.187 0.584	0.54		0.124		
Total	3093.844	706.357			14.127		
Stream Data							
No. Component	MW			L Sale Oil			
4	04.00	mol %		mol %	mol %		mol %
1 H2S 2 O2	34.80 32.00	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000	0.0000 0.0000		0.0000
3 CO2	44.01	0.0000	0.0000	0.0000	0.3604	0.0000	0.0000 0.1317
4 N2	28.01	0.0686	0.0045	0.0000	2.5417	0.0449	0.5541
5 C1	16.04	0.2204	0.0451	0.0000	6.9884	0.4459	1.7802
6 C2	30.07	2.4328	1.5442	0.0012	36.7372	15.2616	19.6415
7 C3	44.10	6.2209	5.5176	0.4140	33.3698	50.8914	47.3179
8 i-C4	58.12	1.6599	1.6133	1.0262	3.4599	6.8329	6.1450
9 n-C4	58.12	7.7683	7.6800	6.3801	11.1789	19.2362	17.5930
10 i-C5 11 n-C5	72.15 72.15	3.0908	3.1298	3.2414	1.5855 2.2911	2.1378 3.0438	2.0252
11 H=C3	86.16	6.2263 4.3237	6.3282 4.4237	6.6977 4.8519	0.4624	0.6170	2.8903 0.5854
13 C7	100.20	14.6079	14.9742	16.5861	0.4650	0.6440	0.6075
14 C8	114.23	7.5449	7.7386	8.5980	0.0673	0.0978	0.0916
15 C9	128.28	6.7161	6.8896	7.6612	0.0185	0.0300	0.0277
16 C10+	177.63	29.8224	30.5948	34.0357	0.0021	0.0038	0.0034
17 Benzene	78.11	0.5895	0.6036	0.6643	0.0470	0.0631	0.0598
18 Toluene	92.13	0.9843	1.0093	1.1197	0.0195	0.0274	0.0258
19 E-Benzene	106.17	0.3646	0.3740	0.4157	0.0021	0.0031	0.0029
20 Xylenes 21 n-C6	106.17 86.18	1.7460 4.5613	1.7910 4.6699	1.9910 5.1392	0.0087 0.3689	0.0129 0.4976	0.0120 0.4713
21 n-Co 22 224Trimethylp	114.24	1.0350	1.0611	1.1765	0.3689	0.4976	0.4713
				- · · <del>- ·</del>		<del>-</del>	-
MW		111.98	113.84	121.25	40.41	47.89	46.37
Stream Mole Ra		1.0000	0.9748	0.8762	0.0252	0.0986	0.1238
Heating Value	[BTU/SCF				2268.06	2715.46	2624.21
Gas Gravity	[Gas/Air	J			1.40	1.65	1.60

Bubble Pt. @ 100F	[psia]	47.50	29.98	8.22
RVP @ 100F	[psia]	25.93	20.86	7.59
Spec. Gravity @ 100F		0.668	0.670	0.677

TANKS 4.0 Report Page 1 of 5

#### **TANKS 4.0.9d**

# **Emissions Report - Detail Format Tank Indentification and Physical Characteristics**

Identification

User Identification: Produced Water Tank

City: State: North Dakota

Company: PetroShale (US), Inc. Type of Tank: Vertical Fixed Roof Tank

Description: Produced Water Tank - PetroShale US8H

**Tank Dimensions** 

Shell Height (ft): 20.00 Diameter (ft): 12.00 Liquid Height (ft): 17.50 Avg. Liquid Height (ft): 17.50 Volume (gallons): 16,074.56 Turnovers: 41.77 Net Throughput(gal/yr): 671,386.37

Is Tank Heated (y/n): Ν

**Paint Characteristics** 

Shell Color/Shade: White/White Shell Condition Good White/White Roof Color/Shade:

Roof Condition: Good

**Roof Characteristics** 

Type: Cone

Height (ft) 1.00 Slope (ft/ft) (Cone Roof) 0.17

**Breather Vent Settings** 

Vacuum Settings (psig): -0.03 Pressure Settings (psig) 0.03

Meterological Data used in Emissions Calculations: Williston, North Dakota (Avg Atmospheric Pressure = 13.82 psia)

TANKS 4.0.9d Emissions Report - Detail Format Liquid Contents of Storage Tank

Troduced Water   Jan   27.55   23.33   31.96   41.45   0.0862   0.0730   0.1016   22.7094   0.0500   0	Mixture/Component	Month	Ten	aily Liquid S nperature (d Min.	eg F)	Liquid Bulk Temp		or Pressure	(psia) Max.	Vapor Mol.	Liquid Mass Fract.	Vapor Mass	Mol.	Basis for Vapor Pressure
Carle of IRVP 8	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,				***************************************		***************************************	***************************************	***************************************		FIACL	FIACL	***************************************	Calculations
Water Perboduced Water Perbo 31.7 26.51 38.44 41.45 0.098 0.0825 0.175 2.4708 15.000 0.950 0.671 18.02 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.0000 0.00		Jan	27.65	23.33	31.96	41.45								
Part   Control	, ,													,
Coude of I(RVP 8)											0.9500	0.6771		Option 2: A=8.10765, B=1750.286, C=235
Water Orduced Water Orduced Water Orduced Water Orduced Water Orduced (RVP 8)		Feb	31.17	26.51	35.84	41.45								
Produced Water   Mar	, ,													•
Crude oil (RVP 8)   Water   RVP 4											0.9500	0.6931		Option 2: A=8.10765, B=1750.286, C=235
Water   Wate	Produced Water	Mar	37.19	31.92	42.46	41.45								
Produced Water Crude oil (RVP 8) Water Crude Oil (RVP	Crude oil (RVP 8)													,
Crude oil (RVP 8)	Water										0.9500	0.7187		Option 2: A=8.10765, B=1750.286, C=235
Value   Valu	Produced Water	Apr	44.20	37.87	50.52	41.45	0.1596							
Produced Water Crude Oil (RVP 8)  Water Crude	Crude oil (RVP 8)						3.8282	3.3921	4.3076		0.0500	0.2542		•
Crude oil (RVP 8) Water  Crude oil (RVP 8) Water  Crude oil (RVP 8)  Use of Start St	Water						0.1428	0.1117	0.1813	18.0200	0.9500	0.7458	18.02	Option 2: A=8.10765, B=1750.286, C=235
Water         Water         United Water         54.43         47.20         61.65         41.45         0.2296         0.1777         0.1369         0.2287         18.020         0.9500         0.7662         18.02         Option 2: A=8.10765, B=1750.286, C=235           Crudue oil (RVP 8)         10.000         0.000         0.000         0.0500         0.0500         0.2193         207.00         Option 4: RVP=7.6           Water         10.000         37.24         49.54         49.54         41.45         0.2531         0.3200         0.8204         0.9500         0.7807         18.02         Option 2: A=8.10765, B=1750.286, C=235           Voduced Water         Jul         57.24         49.54         44.95         41.45         0.2531         0.3030         0.2284         0.0500         0.7807         18.02         Option 2: A=8.10765, B=1750.286, C=235           Voduced Water         Jul         57.24         49.54         41.45         0.2230         0.1748         0.3049         18.020         0.7804         18.02         Option 4: RVP=7.6           Water         Crudue Oil (RVP 8)         49.76         41.45         0.2420         0.1861         0.3164         0.9500         0.7854         18.02         Option 4: RVP=7.6	Produced Water	May	49.98	43.10	56.85	41.45	0.1963	0.1534	0.2497	21.1885			18.88	
Produced Water Crude oil (RVP 8)  Water Crude oil (RVP 8)  Produced Water Crude oil (RVP 8)  Water Crude oil (RVP 8)  Produced Water Crude oil (RVP 8)  Water Crude oil (RVP	Crude oil (RVP 8)						4.2645	3.7499	4.8331	50.0000	0.0500	0.2338	207.00	Option 4: RVP=7.6
Crude oil (RVP 8) Water Water Water Water Water Water  Value oil (RVP 8) Water  Value oil (RVP 8	Water						0.1777	0.1369	0.2287	18.0200	0.9500	0.7662	18.02	Option 2: A=8.10765, B=1750.286, C=235
Water	Produced Water	Jun	54.43	47.20	61.65	41.45	0.2296	0.1779	0.2944	20.9594			18.88	
Crude oil (RVP 8) Water Crude oil (RVP 8)  Dec  Water  The second of the second of the second oil	Crude oil (RVP 8)						4.6266	4.0507	5.2649	50.0000	0.0500	0.2193	207.00	Option 4: RVP=7.6
Crude oil (RVP 8) Water Crude oil (RVP 8) Water  Aug 55.94 48.47 63.41 41.45 0.2420 0.1748 0.3049 18.020 0.9500 0.7894 18.02 0.0010 0.2106 0.0010 0.2106 0.0010 0.2106 0.0010 0.2106 0.0010 0.0	Water						0.2094	0.1601	0.2716	18.0200	0.9500	0.7807	18.02	Option 2: A=8.10765, B=1750.286, C=235
Water Aug 55.94 48.47 63.41 41.45 0.2420 0.1748 0.3049 18.020 0.9500 0.7894 18.02 Option 2: A=8.10765, B=1750.286, C=235 Option 2: A=8.	Produced Water	Jul	57.24	49.54	64.95	41.45	0.2531	0.1933	0.3290	20.8248			18.88	
Produced Water Aug 55.94 48.47 63.41 41.45 0.2420 0.1861 0.3124 20.8862 18.88  Crude oil (RVP 8) 48.47 63.41 41.45 0.2420 0.1861 0.3124 20.8862 18.88  Crude oil (RVP 8) 49.76 43.18 56.34 41.45 0.2213 0.1679 0.2890 18.0200 0.9500 0.7854 18.02 Option 2: A=8.10765, B=1750.286, C=235 18.88  Crude oil (RVP 8) 49.76 43.18 56.34 41.45 0.1948 0.1538 0.2454 18.020 0.9500 0.7854 18.02  Crude oil (RVP 8) 49.76 44.08 38.23 49.93 41.45 0.1589 0.1873 0.2245 18.020 0.9500 0.7655 18.02  Crude oil (RVP 8) 38.29 49.93 41.45 0.1589 0.1283 0.1960 21.5254 18.020 0.9500 0.7655 18.02  Crude oil (RVP 8) 38.29 49.93 41.45 0.1589 0.1283 0.1960 21.5254 18.020 0.9500 0.7655 18.02  Crude oil (RVP 8) 38.09 31.32 40.28 41.45 0.1133 0.1774 18.0200 0.9500 0.7454 18.02 Option 2: A=8.10765, B=1750.286, C=235 18.02  Crude oil (RVP 8) 35.80 31.32 40.28 41.45 0.1133 0.1774 18.0200 0.9500 0.7454 18.02 Option 2: A=8.10765, B=1750.286, C=235 18.02  Crude oil (RVP 8) 35.80 31.32 40.28 41.45 0.1173 0.0991 0.1384 22.0723 18.020  Crude oil (RVP 8) 35.80 31.32 40.28 41.45 0.1173 0.0991 0.1384 22.0723 18.020  Crude oil (RVP 8) 35.80 31.32 40.28 41.45 0.1173 0.0991 0.1384 22.0723 18.020  Crude oil (RVP 8) 35.80 31.32 40.28 41.45 0.1173 0.0991 0.1384 22.0723 18.020  Crude oil (RVP 8) 35.80 31.32 40.28 41.45 0.1173 0.0991 0.1384 22.0723 18.020  Crude oil (RVP 8) 35.80 37.00 0.0500	Crude oil (RVP 8)						4.8675	4.2302	5.5778	50.0000	0.0500	0.2106	207.00	Option 4: RVP=7.6
Crude oil (RVP 8) Water  Sep 49.76 43.18 56.34 41.45 1.45 1.45 1.47 1.54 1.45 1.47 1.47 1.47 1.47 1.47 1.47 1.47 1.47	Water						0.2320	0.1748	0.3049	18.0200	0.9500	0.7894	18.02	Option 2: A=8.10765, B=1750.286, C=235
Crude oil (RVP 8) Water  Value oil (RVP 8)  Val	Produced Water	Aug	55.94	48.47	63.41	41.45	0.2420	0.1861	0.3124	20.8862			18.88	
Produced Water Sep 49.76 43.18 56.34 41.45 0.1948 0.1538 0.2454 21.2000 18.88  Crude oil (RVP 8) 4.2476 3.7554 4.7893 50.0000 0.0500 0.2345 207.00 Option 4: RVP=7.6  Water 0.1763 0.1373 0.2245 18.020 0.9500 0.7655 18.02 Option 2: A=8.10765, B=1750.286, C=235 0.000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.0000 0.0000 0.00000 0.0	Crude oil (RVP 8)						4.7548	4.1471	5.4303	50.0000	0.0500	0.2146	207.00	Option 4: RVP=7.6
Crude oil (RVP 8) Water  Oct 44.08 38.23 49.93 41.45 0.1589 0.1283 0.1960 0.2245 18.020 0.9500 0.2345 207.00 Option 4: RVP=7.6  Water  Crude oil (RVP 8) Water  Oct 44.08 38.23 49.93 41.45 0.1589 0.1283 0.1960 21.5254 18.020 0.9500 0.7655 18.02 Option 2: A=8.10765, B=1750.286, C=235 18.02 Option 2: A=8.10765, B=1750.286, C=235 18.02 Option 4: RVP=7.6  Water  Water  Water  Oct 44.08 38.23 49.93 41.45 0.1589 0.1283 0.1960 21.5254 18.020 0.9500 0.2546 207.00 Option 4: RVP=7.6  Water  Oct 44.08 38.23 49.93 41.45 0.1133 0.1774 18.020 0.9500 0.7454 18.02 Option 2: A=8.10765, B=1750.286, C=235 18.02 Option 2: A=8.10765, B=1750.286, C=235 18.02 Option 4: RVP=7.6  Water  Oct 44.08 38.23 49.93 41.45 0.1133 0.1774 18.020 0.9500 0.7454 18.02 Option 2: A=8.10765, B=1750.286, C=235 18.02 Option 4: RVP=7.6  Water  Oct 44.08 38.23 49.93 41.45 0.1133 0.1774 18.020 0.9500 0.2546 207.00 Option 4: RVP=7.6  Water  Oct 44.08 38.23 49.93 41.45 0.1133 0.1774 18.020 0.9500 0.2500 0.2500 0.2500 0.2500 Option 4: RVP=7.6  Water  Oct 44.08 38.23 49.93 41.45 0.1133 0.1774 18.020 0.9500 0.2500 0.2500 0.2500 Option 4: RVP=7.6  Water  Oct 44.08 38.23 49.93 41.45 0.0924 0.0788 0.1080 22.5579	Water						0.2213	0.1679	0.2890	18.0200	0.9500	0.7854	18.02	Option 2: A=8.10765, B=1750.286, C=235
Water 0.1763 0.1373 0.2245 18.020 0.9500 0.7655 18.02 Option 2: A=8.10765, B=1750.286, C=235 opt	Produced Water	Sep	49.76	43.18	56.34	41.45	0.1948	0.1538	0.2454	21.2000			18.88	·
Produced Water Oct 44.08 38.23 49.93 41.45 0.1589 0.1283 0.1960 21.5254 18.88  Crude oil (RVP 8)  Water  Nov 35.80 31.32 40.28 41.45 0.1173 0.0991 0.1384 22.0723 18.88  Crude oil (RVP 8)  Water  18.88  18.80 0.1680 0.2546 207.00 Option 4: RVP=7.6  18.80 0.1589 0.1283 0.1774 18.0200 0.9500 0.7454 18.02 Option 2: A=8.10765, B=1750.286, C=235  Crude oil (RVP 8)  Water  18.88  18.80 0.1680 0.1774 18.0200 0.9500 0.7454 18.02 Option 2: A=8.10765, B=1750.286, C=235  18.88  18.80 0.1680 0.1774 18.0200 0.9500 0.7454 18.02 Option 2: A=8.10765, B=1750.286, C=235  18.88  18.80 0.16	Crude oil (RVP 8)	•					4.2476	3.7554	4.7893	50.0000	0.0500	0.2345	207.00	Option 4: RVP=7.6
Crude oil (RVP 8) Water  Nov 35.80 31.32 40.28 41.45 0.1173 0.0991 0.1384 22.0723 5.0000 0.0500 0.2546 207.00 Option 4: RVP=7.6  Water  Crude oil (RVP 8)  Water  Crude oil (RVP 8)  Water  Dec 29.47 25.33 33.61 41.45 0.0924 0.0950 0.0859 0.1227 18.020 0.9500 0.7454 18.02 Option 2: A=8.10765, B=1750.286, C=235 0.0000 0.0950	Water						0.1763	0.1373	0.2245	18.0200	0.9500	0.7655	18.02	Option 2: A=8.10765, B=1750.286, C=235
Water 0.1422 0.1133 0.1774 18.020 0.9500 0.7454 18.02 Option 2: A=8.10765, B=1750.286, C=235 Opt	Produced Water	Oct	44.08	38.23	49.93	41.45	0.1589	0.1283	0.1960	21.5254			18.88	, ,
Water 0.1422 0.1133 0.1774 18.020 0.9500 0.7454 18.02 Option 2: A=8.10765, B=1750.286, C=235 Opt			•	•	-						0.0500	0.2546		Option 4: RVP=7.6
Produced Water Nov 35.80 31.32 40.28 41.45 0.1173 0.0991 0.1384 22.0723 18.88  Crude oil (RVP 8) 3.2582 2.9831 3.5531 50.0000 0.0500 0.2870 207.00 Option 4: RVP=7.6  Water 0.1029 0.0859 0.1227 18.0200 0.9500 0.7130 18.02 Option 2: A=8.10765, B=1750.286, C=235 Option 2: A=8.10765, B=1750.286, C=235 Option 3: A=8.10765, B=1750.286	Water													•
Crude oil (RVP 8)  3.2582 2.9831 3.5531 50.000 0.0500 0.2870 207.00 Option 4: RVP=7.6  Water  0.1029 0.0859 0.1227 18.0200 0.9500 0.7130 18.02 Option 2: A=8.10765, B=1750.286, C=235  Produced Water  Dec 29.47 25.33 33.61 41.45 0.0924 0.0788 0.1080 22.5579 18.88  Crude oil (RVP 8)  2.8745 2.6437 3.1211 50.0000 0.0500 0.3145 207.00 Option 4: RVP=7.6	Produced Water	Nov	35.80	31.32	40.28	41.45								
Water         0.1029         0.0859         0.1227         18.0200         0.9500         0.7130         18.02         Option 2: A=8.10765, B=1750.286, C=235           Produced Water         Dec         29.47         25.33         33.61         41.45         0.0924         0.0788         0.1080         22.5579         18.88           Crude oil (RVP 8)         2.8745         2.6437         3.1211         50.0000         0.0500         0.3145         207.00         Option 4: RVP=7.6			50.50	0							0.0500	0.2870		Option 4: RVP=7.6
Produced Water Dec 29.47 25.33 33.61 41.45 0.0924 0.0788 0.1080 22.5579 18.88  Crude oil (RVP 8) 2.8745 2.6437 3.1211 50.0000 0.0500 0.3145 207.00 Option 4: RVP=7.6	, ,													
Crude oil (RVP 8) 2.8745 2.6437 3.1211 50.0000 0.0500 0.3145 207.00 Option 4: RVP=7.6		Dec	29.47	25 33	33.61	41 45					0.0000	0.7100		Option 2.77-0.10700, B-1700.200, 0-200
		D-60	20.71	20.00	55.01	71.75					0.0500	0.3145		Ontion 4: RVP=7.6
	Water						0.0796	0.0671	0.0942	18.0200	0.9500	0.6855	18.02	Option 2: A=8.10765, B=1750.286, C=235

TANKS 4.0.9d Emissions Report - Detail Format Detail Calculations (AP-42)

#### **Produced Water Tank - Vertical Fixed Roof Tank**

Month:	January	February	March	April	May	June	July	August	September	October	November	December
Standing Losses (lb):	0.1216	0.1344	0.2066	0.3053	0.4154	0.4893	0.5929	0.5503	0.3809	0.2887	0.1592	0.1230
Vapor Space Volume (cu ft):	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425
Vapor Density (lb/cu ft):	0.0004	0.0004	0.0005	0.0006	0.0008	0.0009	0.0010	0.0009	0.0008	0.0006	0.0005	0.0004
Vapor Space Expansion Factor:	0.0331	0.0362	0.0416	0.0512	0.0566	0.0604	0.0652	0.0629	0.0540	0.0470	0.0346	0.0316
Vented Vapor Saturation Factor:	0.9872	0.9854	0.9818	0.9766	0.9714	0.9667	0.9634	0.9649	0.9716	0.9767	0.9827	0.9863
vented vapor editaretori actor.	0.0072	0.000	0.0010	0.0700	0.0771	0.0007	0.0001	0.0010	0.0710	0.07 07	0.0027	0.0000
Tank Vapor Space Volume:												
Vapor Space Volume (cu ft):	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425
Tank Diameter (ft):	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000
Vapor Space Outage (ft):	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333
Tank Shell Height (ft):	20.0000	20.0000	20.0000	20.0000	20.0000	20.0000	20.0000	20.0000	20.0000	20.0000	20.0000	20.0000
Average Liquid Height (ft):	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000
Roof Outage (ft):	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333
Roof Outage (Cone Roof)	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Roof Outage (ft):	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333
Roof Height (ft):	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
Roof Slope (ft/ft):	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700
Shell Radius (ft):	6.0000	6.0000	6.0000	6.0000	6.0000	6.0000	6.0000	6.0000	6.0000	6.0000	6.0000	6.0000
Vapor Density												
Vapor Density (lb/cu ft):	0.0004	0.0004	0.0005	0.0006	0.0008	0.0009	0.0010	0.0009	0.0008	0.0006	0.0005	0.0004
Vapor Molecular Weight (lb/lb-mole):	22.7094	22,4208	21.9740	21.5183	21.1885	20.9594	20.8248	20.8862	21.2000	21.5254	22.0723	22.5579
Vapor Pressure at Daily Average Liquid												
Surface Temperature (psia):	0.0862	0.0986	0.1235	0.1596	0.1963	0.2296	0.2531	0.2420	0.1948	0.1589	0.1173	0.0924
Daily Avg. Liquid Surface Temp. (deg. R):	487.3186	490.8447	496.8602	503.8659	509.6452	514.0987	516.9127	515.6102	509.4312	503.7493	495.4708	489.1381
Daily Average Ambient Temp. (deg. F):	8.9000	16.0500	28.4000	43.1500	55.2500	64.7000	70.6500	68.7000	56.2500	44.7500	27.1500	13.2000
Ideal Gas Constant R	3.3333	10.0000	20,1000	10.1000	00.2000	0111000	, 0.0000	55.7 555	00.2000	1111000	27.1.000	10.2000
(psia cuft / (lb-mol-deg R)):	10.731	10.731	10.731	10.731	10.731	10.731	10.731	10.731	10.731	10.731	10.731	10.731
Liquid Bulk Temperature (deg. R):	501.1192	501.1192	501.1192	501.1192	501.1192	501.1192	501.1192	501.1192	501.1192	501,1192	501.1192	501.1192
Tank Paint Solar Absorptance (Shell):	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700
Tank Paint Solar Absorptance (Roof):	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700
Daily Total Solar Insulation												
Factor (Btu/sqft day):	388.0000	671.0000	1.104.0000	1,488.0000	1,827.0000	2,047.0000	2,193.0000	1,862.0000	1,340.0000	877.0000	479.0000	334.0000
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Vapor Space Expansion Factor												
Vapor Space Expansion Factor:	0.0331	0.0362	0.0416	0.0512	0.0566	0.0604	0.0652	0.0629	0.0540	0.0470	0.0346	0.0316
Daily Vapor Temperature Range (deg. R):	17.2549	18.6740	21.0950	25.2989	27.4885	28.8957	30.8147	29.8871	26.3224	23.3985	17.9040	16.5658
Daily Vapor Pressure Range (psia):	0.0286	0.0350	0.0485	0.0735	0.0963	0.1165	0.1357	0.1264	0.0915	0.0677	0.0392	0.0292
Breather Vent Press. Setting Range(psia):	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600
Vapor Pressure at Daily Average Liquid												
Surface Temperature (psia):	0.0862	0.0986	0.1235	0.1596	0.1963	0.2296	0.2531	0.2420	0.1948	0.1589	0.1173	0.0924
Vapor Pressure at Daily Minimum Liquid	0.0700	0.0005	0.4044	0.4000	0.4504	0.4770	0.4000	0.4004	0.4500	0.4000	0.0004	0.0700
Surface Temperature (psia):	0.0730	0.0825	0.1014	0.1266	0.1534	0.1779	0.1933	0.1861	0.1538	0.1283	0.0991	0.0788
Vapor Pressure at Daily Maximum Liquid	0.4040	0.4475	0.4400	0.0004	0.0407	0.0044	0.0000	0.0404	0.0454	0.4000	0.4004	0.4000
Surface Temperature (psia):	0.1016	0.1175	0.1499	0.2001	0.2497	0.2944	0.3290	0.3124	0.2454	0.1960	0.1384	0.1080
Daily Avg. Liquid Surface Temp. (deg R):	487.3186	490.8447	496.8602	503.8659	509.6452	514.0987	516.9127	515.6102	509.4312	503.7493	495.4708	489.1381
Daily Min. Liquid Surface Temp. (deg R):	483.0049	486.1762	491.5864	497.5412	502.7731	506.8747	509.2091	508.1384	502.8506	497.8997	490.9948	484.9966
Daily Max. Liquid Surface Temp. (deg R):	491.6323	495.5132	502.1340	510.1906	516.5173	521.3226	524.6164	523.0820	516.0118	509.5990	499.9468	493.2796
Daily Ambient Temp. Range (deg. R):	21.4000	21.5000	22.0000	25.3000	26.1000	26.6000	28.3000	29.2000	27.7000	26.7000	21.7000	20.8000
Vented Vapor Saturation Factor												
Vented Vapor Saturation Factor:	0.9872	0.9854	0.9818	0.9766	0.9714	0.9667	0.9634	0.9649	0.9716	0.9767	0.9827	0.9863
Vapor Pressure at Daily Average Liquid:	0.0072	000 /			3.5	3.0007	3,0001	3.55.5			002.	2.0000
Surface Temperature (psia):	0.0862	0.0986	0.1235	0.1596	0.1963	0.2296	0.2531	0.2420	0.1948	0.1589	0.1173	0.0924
Vapor Space Outage (ft):	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333
	2.5550	2.0000	2.0000	2.5550	2.3330	2.0000	2.0000	2.0000	2.0000	2.0000	2.5550	2.0000
Working Losses (lb):	1.7306	1.9540	2.3991	3.0366	3.6775	4.2542	4.6604	4.4682	3.6517	3.0248	2.2885	1.8427
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PetroShale US8H PTE 09/02/2019

Vapor Molecular Weight (lb/lb-mole): Vapor Pressure at Daily Average Liquid	22.7094	22.4208	21.9740	21.5183	21.1885	20.9594	20.8248	20.8862	21.2000	21.5254	22.0723	22.5579
Surface Temperature (psia):	0.0862	0.0986	0.1235	0.1596	0.1963	0.2296	0.2531	0.2420	0.1948	0.1589	0.1173	0.0924
Net Throughput (gal/mo.):	55,948.8642	55,948.8642	55,948.8642	55,948.8642	55,948.8642	55,948.8642	55,948.8642	55,948.8642	55,948.8642	55,948.8642	55,948.8642	55,948.8642
Annual Turnovers:	41.7670	41.7670	41.7670	41.7670	41.7670	41.7670	41.7670	41.7670	41.7670	41.7670	41.7670	41.7670
Turnover Factor:	0.8849	0.8849	0.8849	0.8849	0.8849	0.8849	0.8849	0.8849	0.8849	0.8849	0.8849	0.8849
Maximum Liquid Volume (gal):	16,074.5628	16,074.5628	16,074.5628	16,074.5628	16,074.5628	16,074.5628	16,074.5628	16,074.5628	16,074.5628	16,074.5628	16,074.5628	16,074.5628
Maximum Liquid Height (ft):	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000
Tank Diameter (ft):	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000
Working Loss Product Factor:	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500
Total Losses (lb):	1.8522	2.0884	2.6056	3.3419	4.0929	4.7435	5.2533	5.0184	4.0326	3.3135	2.4478	1.9657

# TANKS 4.0.9d Emissions Report - Detail Format Individual Tank Emission Totals

Emissions Report for: January, February, March, April, May, June, July, August, September, October, November, December

		Losses(lbs)	
Components	Working Loss	Breathing Loss	Total Emissions
Produced Water	36.99	3.77	40.76
Crude oil (RVP 8)	9.20	0.91	10.11
Water	27.79	2.86	30.64

TANKS 4.0 Report Page 1 of 5

#### **TANKS 4.0.9d**

# **Emissions Report - Detail Format Tank Indentification and Physical Characteristics**

Identification

User Identification: Produced Water Tank

City: State: North Dakota

Company: PetroShale (US), Inc. Type of Tank: Vertical Fixed Roof Tank

Description: Produced Water Tank - PetroShale US12H & US 13H

**Tank Dimensions** 

30.00 Shell Height (ft): Diameter (ft): 15.50 Liquid Height (ft): 28.50 Avg. Liquid Height (ft): 28.50 Volume (gallons): 40,228.27 Turnovers: 56.47 Net Throughput(gal/yr): 2,271,670.82

Is Tank Heated (y/n): Ν

**Paint Characteristics** 

Shell Color/Shade: White/White Shell Condition Good White/White Roof Color/Shade:

Roof Condition: Good

**Roof Characteristics** 

Type: Cone

Height (ft) 1.00 Slope (ft/ft) (Cone Roof) 0.13

**Breather Vent Settings** 

Vacuum Settings (psig): -0.03 Pressure Settings (psig) 0.03

Meterological Data used in Emissions Calculations: Williston, North Dakota (Avg Atmospheric Pressure = 13.82 psia)

TANKS 4.0.9d Emissions Report - Detail Format Liquid Contents of Storage Tank

			aily Liquid Si nperature (de		Liquid Bulk Temp	Vapo	or Pressure	(psia)	Vapor Mol.	Liquid Mass	Vapor Mass	Mol.	Basis for Vapor Pressure
Mixture/Component	Month	Avg.	Min.	Max.	(deg F)	Avg.	Min.	Max.	Weight.	Fract.	Fract.	Weight	Calculations
Produced Water	Jan	27.65	23.33	31.96	41.45	0.0862	0.0730	0.1016	22.7094			18.88	
Crude oil (RVP 8)						2.7712	2.5381	3.0211	50.0000	0.0500	0.3229	207.00	Option 4: RVP=7.6
Water						0.0739	0.0617	0.0882	18.0200	0.9500	0.6771	18.02	Option 2: A=8.10765, B=1750.286, C=235
Produced Water	Feb	31.17	26.51	35.84	41.45	0.0986	0.0825	0.1175	22.4208			18.88	
Crude oil (RVP 8)						2.9742	2.7079	3.2609	50.0000	0.0500	0.3069	207.00	Option 4: RVP=7.6
Water						0.0854	0.0705	0.1031	18.0200	0.9500	0.6931	18.02	Option 2: A=8.10765, B=1750.286, C=235
roduced Water	Mar	37.19	31.92	42.46	41.45	0.1235	0.1014	0.1499	21.9740			18.88	
Crude oil (RVP 8)						3.3476	3.0183	3.7046	50.0000	0.0500	0.2813	207.00	Option 4: RVP=7.6
Water						0.1087	0.0880	0.1336	18.0200	0.9500	0.7187	18.02	Option 2: A=8.10765, B=1750.286, C=235
roduced Water	Apr	44.20	37.87	50.52	41.45	0.1596	0.1266	0.2001	21.5183			18.88	
Crude oil (RVP 8)						3.8282	3.3921	4.3076	50.0000	0.0500	0.2542	207.00	Option 4: RVP=7.6
Water						0.1428	0.1117	0.1813	18.0200	0.9500	0.7458	18.02	Option 2: A=8.10765, B=1750.286, C=235
Produced Water	May	49.98	43.10	56.85	41.45	0.1963	0.1534	0.2497	21.1885			18.88	
Crude oil (RVP 8)						4.2645	3.7499	4.8331	50.0000	0.0500	0.2338	207.00	Option 4: RVP=7.6
Water						0.1777	0.1369	0.2287	18.0200	0.9500	0.7662	18.02	Option 2: A=8.10765, B=1750.286, C=235
roduced Water	Jun	54.43	47.20	61.65	41.45	0.2296	0.1779	0.2944	20.9594			18.88	
Crude oil (RVP 8)						4.6266	4.0507	5.2649	50.0000	0.0500	0.2193	207.00	Option 4: RVP=7.6
Water						0.2094	0.1601	0.2716	18.0200	0.9500	0.7807	18.02	Option 2: A=8.10765, B=1750.286, C=235
roduced Water	Jul	57.24	49.54	64.95	41.45	0.2531	0.1933	0.3290	20.8248			18.88	
Crude oil (RVP 8)						4.8675	4.2302	5.5778	50.0000	0.0500	0.2106	207.00	Option 4: RVP=7.6
Water						0.2320	0.1748	0.3049	18.0200	0.9500	0.7894	18.02	Option 2: A=8.10765, B=1750.286, C=235
roduced Water	Aug	55.94	48.47	63.41	41.45	0.2420	0.1861	0.3124	20.8862			18.88	
Crude oil (RVP 8)						4.7548	4.1471	5.4303	50.0000	0.0500	0.2146	207.00	Option 4: RVP=7.6
Water						0.2213	0.1679	0.2890	18.0200	0.9500	0.7854	18.02	Option 2: A=8.10765, B=1750.286, C=235
roduced Water	Sep	49.76	43.18	56.34	41.45	0.1948	0.1538	0.2454	21.2000			18.88	
Crude oil (RVP 8)						4.2476	3.7554	4.7893	50.0000	0.0500	0.2345	207.00	Option 4: RVP=7.6
Water						0.1763	0.1373	0.2245	18.0200	0.9500	0.7655	18.02	Option 2: A=8.10765, B=1750.286, C=235
roduced Water	Oct	44.08	38.23	49.93	41.45	0.1589	0.1283	0.1960	21.5254			18.88	
Crude oil (RVP 8)						3.8198	3.4157	4.2608	50.0000	0.0500	0.2546	207.00	Option 4: RVP=7.6
Water						0.1422	0.1133	0.1774	18.0200	0.9500	0.7454	18.02	Option 2: A=8.10765, B=1750.286, C=235
roduced Water	Nov	35.80	31.32	40.28	41.45	0.1173	0.0991	0.1384	22.0723			18.88	
Crude oil (RVP 8)						3.2582	2.9831	3.5531	50.0000	0.0500	0.2870	207.00	Option 4: RVP=7.6
Water						0.1029	0.0859	0.1227	18.0200	0.9500	0.7130	18.02	Option 2: A=8.10765, B=1750.286, C=235
roduced Water	Dec	29.47	25.33	33.61	41.45	0.0924	0.0788	0.1080	22.5579			18.88	, , , , , , , , , , , , , , , , , , , ,
Crude oil (RVP 8)						2.8745	2.6437	3.1211	50.0000	0.0500	0.3145	207.00	Option 4: RVP=7.6
Water						0.0796	0.0671	0.0942	18.0200	0.9500	0.6855	18.02	Option 2: A=8.10765, B=1750.286, C=235

TANKS 4.0.9d Emissions Report - Detail Format Detail Calculations (AP-42)

### **Produced Water Tank - Vertical Fixed Roof Tank**

Month:	January	February	March	April	May	June	July	August	September	October	November	December
Standing Losses (lb):	0.1318	0.1458	0.2244	0.3324	0.4530	0.5345	0.6484	0.6015	0.4154	0.3142	0.1729	0.1335
Vapor Space Volume (cu ft):	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352
Vapor Density (lb/cu ft):	0.0004	0.0004	0.0005	0.0006	0.0008	0.0009	0.0010	0.0009	0.0008	0.0006	0.0005	0.0004
Vapor Space Expansion Factor:	0.0331	0.0362	0.0416	0.0512	0.0566	0.0604	0.0652	0.0629	0.0540	0.0470	0.0346	0.0316
Vented Vapor Saturation Factor:	0.9917	0.9905	0.9881	0.9847	0.9813	0.9782	0.9760	0.9770	0.9814	0.9848	0.9887	0.9911
vented vapor editardient deter.	0.0017	0.0000	0.0007	0.0017	0.0070	0.07.02	0.0700	0.0770	0.0011	0.0010	0.0007	0.0011
Tank Vapor Space Volume:												
Vapor Space Volume (cu ft):	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352
Tank Diameter (ft):	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000
Vapor Space Outage (ft):	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333
Tank Shell Height (ft):	30.0000	30.0000	30.0000	30.0000	30.0000	30.0000	30.0000	30.0000	30.0000	30.0000	30.0000	30.0000
Average Liquid Height (ft):	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000
Roof Outage (ft):	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333
D 10 1 10 D 1												
Roof Outage (Cone Roof)	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Roof Outage (ft):	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333
Roof Height (ft):	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
Roof Slope (ft/ft):	0.1300	0.1300	0.1300	0.1300	0.1300	0.1300	0.1300	0.1300	0.1300	0.1300	0.1300	0.1300
Shell Radius (ft):	7.7500	7.7500	7.7500	7.7500	7.7500	7.7500	7.7500	7.7500	7.7500	7.7500	7.7500	7.7500
Vapor Density												
Vapor Density (lb/cu ft):	0.0004	0.0004	0.0005	0.0006	0.0008	0.0009	0.0010	0.0009	8000.0	0.0006	0.0005	0.0004
Vapor Molecular Weight (lb/lb-mole):	22.7094	22,4208	21.9740	21.5183	21.1885	20.9594	20.8248	20.8862	21.2000	21.5254	22.0723	22.5579
Vapor Pressure at Daily Average Liquid												
Surface Temperature (psia):	0.0862	0.0986	0.1235	0.1596	0.1963	0.2296	0.2531	0.2420	0.1948	0.1589	0.1173	0.0924
Daily Avg. Liquid Surface Temp. (deg. R):	487.3186	490.8447	496.8602	503.8659	509.6452	514.0987	516.9127	515.6102	509.4312	503.7493	495.4708	489.1381
Daily Average Ambient Temp. (deg. F):	8.9000	16.0500	28.4000	43.1500	55.2500	64.7000	70.6500	68.7000	56.2500	44.7500	27.1500	13.2000
Ideal Gas Constant R												
(psia cuft / (lb-mol-deg R)):	10.731	10.731	10.731	10.731	10.731	10.731	10.731	10.731	10.731	10.731	10.731	10.731
Liquid Bulk Temperature (deg. R):	501.1192	501.1192	501.1192	501.1192	501.1192	501.1192	501.1192	501.1192	501.1192	501,1192	501.1192	501.1192
Tank Paint Solar Absorptance (Shell):	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700
Tank Paint Solar Absorptance (Roof):	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700
Daily Total Solar Insulation												
Factor (Btu/sqft day):	388.0000	671.0000	1.104.0000	1,488.0000	1,827.0000	2,047.0000	2,193.0000	1,862.0000	1,340.0000	877.0000	479.0000	334.0000
Vapor Space Expansion Factor												
Vapor Space Expansion Factor:	0.0331	0.0362	0.0416	0.0512	0.0566	0.0604	0.0652	0.0629	0.0540	0.0470	0.0346	0.0316
Daily Vapor Temperature Range (deg. R):	17.2549	18.6740	21.0950	25.2989	27.4885	28.8957	30.8147	29.8871	26.3224	23.3985	17.9040	16.5658
Daily Vapor Pressure Range (psia):	0.0286	0.0350	0.0485	0.0735	0.0963	0.1165	0.1357	0.1264	0.0915	0.0677	0.0392	0.0292
Breather Vent Press. Setting Range(psia):	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600
Vapor Pressure at Daily Average Liquid												
Surface Temperature (psia):	0.0862	0.0986	0.1235	0.1596	0.1963	0.2296	0.2531	0.2420	0.1948	0.1589	0.1173	0.0924
Vapor Pressure at Daily Minimum Liquid												
Surface Temperature (psia):	0.0730	0.0825	0.1014	0.1266	0.1534	0.1779	0.1933	0.1861	0.1538	0.1283	0.0991	0.0788
Vapor Pressure at Daily Maximum Liquid												
Surface Temperature (psia):	0.1016	0.1175	0.1499	0.2001	0.2497	0.2944	0.3290	0.3124	0.2454	0.1960	0.1384	0.1080
Daily Avg. Liquid Surface Temp. (deg R):	487.3186	490.8447	496.8602	503.8659	509.6452	514.0987	516.9127	515.6102	509.4312	503.7493	495.4708	489.1381
Daily Min. Liquid Surface Temp. (deg R):	483.0049	486.1762	491.5864	497.5412	502.7731	506.8747	509.2091	508.1384	502.8506	497.8997	490.9948	484.9966
Daily Max. Liquid Surface Temp. (deg R):	491.6323	495.5132	502.1340	510.1906	516.5173	521.3226	524.6164	523.0820	516.0118	509.5990	499.9468	493.2796
Daily Ambient Temp. Range (deg. R):	21.4000	21.5000	22.0000	25.3000	26.1000	26.6000	28.3000	29.2000	27.7000	26.7000	21.7000	20.8000
Vented Vapor Saturation Factor												
Vented Vapor Saturation Factor:	0.9917	0.9905	0.9881	0.9847	0.9813	0.9782	0.9760	0.9770	0.9814	0.9848	0.9887	0.9911
Vapor Pressure at Daily Average Liquid:	0.0011	0.0000	5.5551	0.0017	5.5510	5.5.52	2.2.30	5.5.70	0.00.1	5.55.0	2.2331	0.0071
Surface Temperature (psia):	0.0862	0.0986	0.1235	0.1596	0.1963	0.2296	0.2531	0.2420	0.1948	0.1589	0.1173	0.0924
Vapor Space Outage (ft):	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333
0- x: xhanz a nan <b>3</b> z (n/,												
Working Losses (lb):	4.6181	5.2143	6.4020	8.1032	9.8135	11.3525	12.4363	11.9234	9.7446	8.0717	6.1070	4.9172
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PetroShale US 12H & 13H - PTE

10/23/2019

Vapor Molecular Weight (lb/lb-mole): Vapor Pressure at Daily Average Liguid	22.7094	22.4208	21.9740	21.5183	21.1885	20.9594	20.8248	20.8862	21.2000	21.5254	22.0723	22.5579
Surface Temperature (psia):	0.0862	0.0986	0.1235	0.1596	0.1963	0.2296	0.2531	0.2420	0.1948	0.1589	0.1173	0.0924
Net Throughput (gal/mo.):	189,305.9020	189,305.9020	189,305.9020	189,305.9020	189,305.9020	189,305.9020	189,305.9020	189,305.9020	189,305.9020	189,305.9020	189,305.9020	189,305.9020
Annual Turnovers:	56.4695	56.4695	56.4695	56.4695	56.4695	56.4695	56.4695	56.4695	56.4695	56.4695	56.4695	56.4695
Turnover Factor:	0.6979	0.6979	0.6979	0.6979	0.6979	0.6979	0.6979	0.6979	0.6979	0.6979	0.6979	0.6979
Maximum Liquid Volume (gal):	40,228.2679	40,228.2679	40,228.2679	40,228.2679	40,228.2679	40,228.2679	40,228.2679	40,228.2679	40,228.2679	40,228.2679	40,228.2679	40,228.2679
Maximum Liquid Height (ft):	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000
Tank Diameter (ft):	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000
Working Loss Product Factor:	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500
Total Losses (lb):	4.7500	5.3601	6.6264	8.4355	10.2665	11.8870	13.0847	12.5249	10.1600	8,3859	6.2800	5.0507

# TANKS 4.0.9d Emissions Report - Detail Format Individual Tank Emission Totals

Emissions Report for: January, February, March, April, May, June, July, August, September, October, November, December

		Losses(lbs)	
Components	Working Loss		Total Emissions
Produced Water	98.70	4.11	102.81
Crude oil (RVP 8)	24.55	0.99	25.55
Water	74.15	3.12	77.27

TANKS 4.0 Report Page 1 of 5

#### **TANKS 4.0.9d**

# **Emissions Report - Detail Format Tank Indentification and Physical Characteristics**

Identification

User Identification: Produced Water Tank

City: State: North Dakota

Company: PetroShale (US), Inc. Type of Tank: Vertical Fixed Roof Tank

Description: Produced Water Tank - PetroShale US8H

**Tank Dimensions** 

20.00 Shell Height (ft): Diameter (ft): 12.00 Liquid Height (ft): 17.50 Avg. Liquid Height (ft): 17.50 Volume (gallons): 16,074.56 Turnovers: 30.01 Net Throughput(gal/yr): 482,338.50

Is Tank Heated (y/n): Ν

**Paint Characteristics** 

Shell Color/Shade: White/White Shell Condition Good Roof Color/Shade: White/White

Roof Condition: Good

**Roof Characteristics** 

Type: Cone

Height (ft) 1.00 Slope (ft/ft) (Cone Roof) 0.17

**Breather Vent Settings** 

Vacuum Settings (psig): -0.03 Pressure Settings (psig) 0.03

Meterological Data used in Emissions Calculations: Williston, North Dakota (Avg Atmospheric Pressure = 13.82 psia)

TANKS 4.0.9d Emissions Report - Detail Format Liquid Contents of Storage Tank

			aily Liquid S perature (de		Liquid Bulk Temp	Vapo	or Pressure	(psia)	Vapor Mol.	Liquid Mass	Vapor Mass	Mol.	Basis for Vapor Pressure
Mixture/Component	Month	Avg.	Min.	Max.	(deg F)	Avg.	Min.	Max.	Weight.	Fract.	Fract.	Weight	Calculations
Produced Water	Jan	27.65	23.33	31.96	41.45	0.0862	0.0730	0.1016	22.7094			18.88	
Crude oil (RVP 8)						2.7712	2.5381	3.0211	50.0000	0.0500	0.3229	207.00	Option 4: RVP=7.6
Water						0.0739	0.0617	0.0882	18.0200	0.9500	0.6771	18.02	Option 2: A=8.10765, B=1750.286, C=235
Produced Water	Feb	31.17	26.51	35.84	41.45	0.0986	0.0825	0.1175	22.4208			18.88	
Crude oil (RVP 8)						2.9742	2.7079	3.2609	50.0000	0.0500	0.3069	207.00	Option 4: RVP=7.6
Water						0.0854	0.0705	0.1031	18.0200	0.9500	0.6931	18.02	Option 2: A=8.10765, B=1750.286, C=235
Produced Water	Mar	37.19	31.92	42.46	41.45	0.1235	0.1014	0.1499	21.9740			18.88	
Crude oil (RVP 8)						3.3476	3.0183	3.7046	50.0000	0.0500	0.2813	207.00	Option 4: RVP=7.6
Water						0.1087	0.0880	0.1336	18.0200	0.9500	0.7187	18.02	Option 2: A=8.10765, B=1750.286, C=235
Produced Water	Apr	44.20	37.87	50.52	41.45	0.1596	0.1266	0.2001	21.5183			18.88	
Crude oil (RVP 8)						3.8282	3.3921	4.3076	50.0000	0.0500	0.2542	207.00	Option 4: RVP=7.6
Water						0.1428	0.1117	0.1813	18.0200	0.9500	0.7458	18.02	Option 2: A=8.10765, B=1750.286, C=235
Produced Water	May	49.98	43.10	56.85	41.45	0.1963	0.1534	0.2497	21.1885			18.88	
Crude oil (RVP 8)						4.2645	3.7499	4.8331	50.0000	0.0500	0.2338	207.00	Option 4: RVP=7.6
Water						0.1777	0.1369	0.2287	18.0200	0.9500	0.7662	18.02	Option 2: A=8.10765, B=1750.286, C=235
Produced Water	Jun	54.43	47.20	61.65	41.45	0.2296	0.1779	0.2944	20.9594			18.88	
Crude oil (RVP 8)						4.6266	4.0507	5.2649	50.0000	0.0500	0.2193	207.00	Option 4: RVP=7.6
Water						0.2094	0.1601	0.2716	18.0200	0.9500	0.7807	18.02	Option 2: A=8.10765, B=1750.286, C=235
Produced Water	Jul	57.24	49.54	64.95	41.45	0.2531	0.1933	0.3290	20.8248			18.88	
Crude oil (RVP 8)						4.8675	4.2302	5.5778	50.0000	0.0500	0.2106	207.00	Option 4: RVP=7.6
Water						0.2320	0.1748	0.3049	18.0200	0.9500	0.7894	18.02	Option 2: A=8.10765, B=1750.286, C=235
Produced Water	Aug	55.94	48.47	63.41	41.45	0.2420	0.1861	0.3124	20.8862			18.88	
Crude oil (RVP 8)						4.7548	4.1471	5.4303	50.0000	0.0500	0.2146	207.00	Option 4: RVP=7.6
Water						0.2213	0.1679	0.2890	18.0200	0.9500	0.7854	18.02	Option 2: A=8.10765, B=1750.286, C=235
Produced Water	Sep	49.76	43.18	56.34	41.45	0.1948	0.1538	0.2454	21.2000			18.88	
Crude oil (RVP 8)						4.2476	3.7554	4.7893	50.0000	0.0500	0.2345	207.00	Option 4: RVP=7.6
Water						0.1763	0.1373	0.2245	18.0200	0.9500	0.7655	18.02	Option 2: A=8.10765, B=1750.286, C=235
Produced Water	Oct	44.08	38.23	49.93	41.45	0.1589	0.1283	0.1960	21.5254			18.88	
Crude oil (RVP 8)						3.8198	3.4157	4.2608	50.0000	0.0500	0.2546	207.00	Option 4: RVP=7.6
Water						0.1422	0.1133	0.1774	18.0200	0.9500	0.7454	18.02	Option 2: A=8.10765, B=1750.286, C=235
Produced Water	Nov	35.80	31.32	40.28	41.45	0.1173	0.0991	0.1384	22.0723			18.88	
Crude oil (RVP 8)						3.2582	2.9831	3.5531	50.0000	0.0500	0.2870	207.00	Option 4: RVP=7.6
Water						0.1029	0.0859	0.1227	18.0200	0.9500	0.7130	18.02	Option 2: A=8.10765, B=1750.286, C=235
Produced Water	Dec	29.47	25.33	33.61	41.45	0.0924	0.0788	0.1080	22.5579			18.88	
Crude oil (RVP 8)						2.8745	2.6437	3.1211	50.0000	0.0500	0.3145	207.00	Option 4: RVP=7.6
Water						0.0796	0.0671	0.0942	18.0200	0.9500	0.6855	18.02	Option 2: A=8.10765, B=1750.286, C=235

TANKS 4.0.9d Emissions Report - Detail Format Detail Calculations (AP-42)

#### **Produced Water Tank - Vertical Fixed Roof Tank**

Month:	January	February	March	April	May	June	July	August	September	October	November	December
Standing Losses (lb):	0.1216	0.1344	0.2066	0.3053	0.4154	0.4893	0.5929	0.5503	0.3809	0.2887	0.1592	0.1230
Vapor Space Volume (cu ft):	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425
Vapor Density (lb/cu ft):	0.0004	0.0004	0.0005	0.0006	0.0008	0.0009	0.0010	0.0009	0.0008	0.0006	0.0005	0.0004
Vapor Space Expansion Factor:	0.0331	0.0362	0.0416	0.0512	0.0566	0.0604	0.0652	0.0629	0.0540	0.0470	0.0346	0.0316
Vented Vapor Saturation Factor:	0.9872	0.9854	0.9818	0.9766	0.9714	0.9667	0.9634	0.9649	0.9716	0.9767	0.9827	0.9863
Tomou Tapor Bataration Labor.	0.0072	0.000	0.0010	0.0700	0.0771	0.0007	0.0001	0.0010	0.0710	0.07 07	0.0027	0.0000
Tank Vapor Space Volume:												
Vapor Space Volume (cu ft):	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425	320.4425
Tank Diameter (ft):	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000
Vapor Space Outage (ft):	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333
Tank Shell Height (ft):	20.0000	20.0000	20.0000	20.0000	20.0000	20.0000	20.0000	20.0000	20.0000	20.0000	20.0000	20.0000
Average Liquid Height (ft):	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000
Roof Outage (ft):	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333
Roof Outage (Cone Roof)	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Roof Outage (ft):	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333
Roof Height (ft):	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
Roof Slope (ft/ft):	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700
Shell Radius (ft):	6.0000	6.0000	6.0000	6.0000	6.0000	6.0000	6.0000	6.0000	6.0000	6.0000	6.0000	6.0000
Vapor Density												
Vapor Density (lb/cu ft):	0.0004	0.0004	0.0005	0.0006	0.0008	0.0009	0.0010	0.0009	0.0008	0.0006	0.0005	0.0004
Vapor Molecular Weight (lb/lb-mole):	22.7094	22,4208	21.9740	21.5183	21.1885	20.9594	20.8248	20.8862	21.2000	21.5254	22.0723	22.5579
Vapor Pressure at Daily Average Liquid	22.7001	22.1200	21.07.10	21.0100	21.1000	20.0001	20.02.10	20.5052	21.2000	21.0201	22.0720	22.0070
Surface Temperature (psia):	0.0862	0.0986	0.1235	0.1596	0.1963	0.2296	0.2531	0.2420	0.1948	0.1589	0.1173	0.0924
Daily Avg. Liquid Surface Temp. (deg. R):	487.3186	490.8447	496.8602	503.8659	509.6452	514.0987	516.9127	515.6102	509.4312	503.7493	495.4708	489.1381
Daily Average Ambient Temp. (deg. F):	8.9000	16.0500	28.4000	43.1500	55.2500	64.7000	70.6500	68.7000	56.2500	44.7500	27.1500	13.2000
Ideal Gas Constant R	0.0000	10.0000	20,1000	10.1000	00.2000	0117000	, 0.0000	55.7 555	00.2000		2711000	10.2000
(psia cuft / (lb-mol-deg R)):	10.731	10.731	10.731	10.731	10.731	10.731	10.731	10.731	10.731	10.731	10.731	10.731
Liquid Bulk Temperature (deg. R):	501.1192	501.1192	501.1192	501.1192	501.1192	501.1192	501.1192	501.1192	501.1192	501,1192	501.1192	501.1192
Tank Paint Solar Absorptance (Shell):	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700
Tank Paint Solar Absorptance (Roof):	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700
Daily Total Solar Insulation												
Factor (Btu/sqft day):	388.0000	671.0000	1.104.0000	1,488.0000	1,827.0000	2,047.0000	2,193.0000	1,862.0000	1,340.0000	877.0000	479.0000	334.0000
Vapor Space Expansion Factor												
Vapor Space Expansion Factor:	0.0331	0.0362	0.0416	0.0512	0.0566	0.0604	0.0652	0.0629	0.0540	0.0470	0.0346	0.0316
Daily Vapor Temperature Range (deg. R):	17.2549	18.6740	21.0950	25.2989	27.4885	28.8957	30.8147	29.8871	26.3224	23.3985	17.9040	16.5658
Daily Vapor Pressure Range (psia):	0.0286	0.0350	0.0485	0.0735	0.0963	0.1165	0.1357	0.1264	0.0915	0.0677	0.0392	0.0292
Breather Vent Press. Setting Range(psia):	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600
Vapor Pressure at Daily Average Liquid												
Surface Temperature (psia):	0.0862	0.0986	0.1235	0.1596	0.1963	0.2296	0.2531	0.2420	0.1948	0.1589	0.1173	0.0924
Vapor Pressure at Daily Minimum Liquid	0.0700	0.0005	0.4044	0.4000	0.4504	0.4770	0.4000	0.4004	0.4500	0.4000	2 2004	0.0700
Surface Temperature (psia):	0.0730	0.0825	0.1014	0.1266	0.1534	0.1779	0.1933	0.1861	0.1538	0.1283	0.0991	0.0788
Vapor Pressure at Daily Maximum Liquid	0.4040	0.4475	0.4400	0.0004	0.0407	0.0044	0.0000	0.0404	0.0454	0.4000	0.4004	0.4000
Surface Temperature (psia):	0.1016	0.1175	0.1499	0.2001	0.2497	0.2944	0.3290	0.3124	0.2454	0.1960	0.1384	0.1080
Daily Avg. Liquid Surface Temp. (deg R):	487.3186	490.8447	496.8602	503.8659	509.6452 502.7731	514.0987	516.9127	515.6102	509.4312	503.7493	495.4708	489.1381 484.9966
Daily Min. Liquid Surface Temp. (deg R):	483.0049	486.1762	491.5864	497.5412		506.8747	509.2091	508.1384	502.8506	497.8997	490.9948	
Daily Max. Liquid Surface Temp. (deg R):	491.6323	495.5132	502.1340	510.1906	516.5173	521.3226	524.6164	523.0820	516.0118	509.5990	499.9468	493.2796
Daily Ambient Temp. Range (deg. R):	21.4000	21.5000	22.0000	25.3000	26.1000	26.6000	28.3000	29.2000	27.7000	26.7000	21.7000	20.8000
Vented Vapor Saturation Factor												
Vented Vapor Saturation Factor:	0.9872	0.9854	0.9818	0.9766	0.9714	0.9667	0.9634	0.9649	0.9716	0.9767	0.9827	0.9863
Vapor Pressure at Daily Average Liquid:				2,2,50								
Surface Temperature (psia):	0.0862	0.0986	0.1235	0.1596	0.1963	0.2296	0.2531	0.2420	0.1948	0.1589	0.1173	0.0924
Vapor Space Outage (ft):	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333	2.8333
i an alternative work.												
Working Losses (lb):	1.4050	1.5863	1.9477	2.4652	2.9855	3.4537	3.7835	3.6274	2.9646	2.4556	1.8579	1.4959
- ' '												

PetroShale US8H - Most Recent 12 Months of Production

09/02/2019

Vapor Molecular Weight (lb/lb-mole):	22.7094	22.4208	21.9740	21.5183	21.1885	20.9594	20.8248	20.8862	21.2000	21.5254	22.0723	22.5579
Vapor Pressure at Daily Average Liquid Surface Temperature (psia):	0.0862	0.0986	0.1235	0.1596	0.1963	0.2296	0.2531	0.2420	0.1948	0.1589	0.1173	0.0924
Net Throughput (gal/mo.):	40,194.8750	40,194.8750	40,194.8750	40,194.8750	40,194.8750	40,194.8750	40,194.8750	40,194.8750	40,194.8750	40,194.8750	40,194.8750	40,194.8750
Annual Turnovers:	30.0063	30.0063	30.0063	30.0063	30.0063	30.0063	30.0063	30.0063	30,0063	30.0063	30.0063	30.0063
Turnover Factor:	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
Maximum Liquid Volume (gal):	16,074.5628	16,074.5628	16,074.5628	16,074.5628	16,074.5628	16,074.5628	16,074.5628	16,074.5628	16,074.5628	16,074.5628	16,074.5628	16,074.5628
Maximum Liquid Height (ft):	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000	17.5000
Tank Diameter (ft):	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000	12.0000
Working Loss Product Factor:	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500
Total Losses (lb):	1.5265	1.7207	2.1542	2.7705	3.4009	3.9430	4.3763	4.1777	3.3455	2.7443	2.0171	1.6190

# TANKS 4.0.9d Emissions Report - Detail Format Individual Tank Emission Totals

Emissions Report for: January, February, March, April, May, June, July, August, September, October, November, December

	Losses(lbs)						
Components	Working Loss	Breathing Loss	Total Emissions				
Produced Water	30.03	3.77	33.80				
Crude oil (RVP 8)	7.47	0.91	8.38				
Water	22.56	2.86	25.42				

TANKS 4.0 Report Page 1 of 5

#### **TANKS 4.0.9d**

# **Emissions Report - Detail Format Tank Indentification and Physical Characteristics**

Identification

User Identification: Produced Water Tank

City: State: North Dakota

Company: PetroShale (US), Inc. Type of Tank: Vertical Fixed Roof Tank

Description: Produced Water Tank - PetroShale US12H & US 13H

**Tank Dimensions** 

30.00 Shell Height (ft): Diameter (ft): 15.50 Liquid Height (ft): 28.50 Avg. Liquid Height (ft): 28.50 Volume (gallons): 40,228.27 Turnovers: 36.78 Net Throughput(gal/yr): 1,479,480.12

Is Tank Heated (y/n): Ν

**Paint Characteristics** 

Shell Color/Shade: White/White Shell Condition Good Roof Color/Shade: White/White

Roof Condition: Good

**Roof Characteristics** 

Type: Cone

Height (ft) 1.00 Slope (ft/ft) (Cone Roof) 0.13

**Breather Vent Settings** 

Vacuum Settings (psig): -0.03 Pressure Settings (psig) 0.03

Meterological Data used in Emissions Calculations: Williston, North Dakota (Avg Atmospheric Pressure = 13.82 psia)

TANKS 4.0.9d Emissions Report - Detail Format Liquid Contents of Storage Tank

Mixture/Component	Month		aily Liquid S nperature (d Min.		Liquid Bulk Temp (deg F)		or Pressure Min.	(psia) Max.	Vapor Mol. Weight.	Liquid Mass Fract.	Vapor Mass	Mol. Weight	Basis for Vapor Pressure Calculations
·	***************************************	***************************************	***************************************			Avg.	***************************************	***************************************	***************************************	FIACL	Fract.		Calculations
Produced Water	Jan	27.65	23.33	31.96	41.45	0.0862	0.0730	0.1016	22.7094			18.88	
Crude oil (RVP 8)						2.7712	2.5381	3.0211	50.0000	0.0500	0.3229	207.00	Option 4: RVP=7.6
Water						0.0739	0.0617	0.0882	18.0200	0.9500	0.6771	18.02	Option 2: A=8.10765, B=1750.286, C=235
Produced Water	Feb	31.17	26.51	35.84	41.45	0.0986	0.0825	0.1175	22.4208			18.88	
Crude oil (RVP 8)						2.9742	2.7079	3.2609	50.0000	0.0500	0.3069	207.00	Option 4: RVP=7.6
Water						0.0854	0.0705	0.1031	18.0200	0.9500	0.6931	18.02	Option 2: A=8.10765, B=1750.286, C=235
Produced Water	Mar	37.19	31.92	42.46	41.45	0.1235	0.1014	0.1499	21.9740			18.88	
Crude oil (RVP 8)						3.3476	3.0183	3.7046	50.0000	0.0500	0.2813	207.00	Option 4: RVP=7.6
Water						0.1087	0.0880	0.1336	18.0200	0.9500	0.7187	18.02	Option 2: A=8.10765, B=1750.286, C=235
Produced Water	Apr	44.20	37.87	50.52	41.45	0.1596	0.1266	0.2001	21.5183			18.88	
Crude oil (RVP 8)						3.8282	3.3921	4.3076	50.0000	0.0500	0.2542	207.00	Option 4: RVP=7.6
Water						0.1428	0.1117	0.1813	18.0200	0.9500	0.7458	18.02	Option 2: A=8.10765, B=1750.286, C=235
Produced Water	May	49.98	43.10	56.85	41.45	0.1963	0.1534	0.2497	21.1885			18.88	
Crude oil (RVP 8)						4.2645	3.7499	4.8331	50.0000	0.0500	0.2338	207.00	Option 4: RVP=7.6
Water						0.1777	0.1369	0.2287	18.0200	0.9500	0.7662	18.02	Option 2: A=8.10765, B=1750.286, C=235
Produced Water	Jun	54.43	47.20	61.65	41.45	0.2296	0.1779	0.2944	20.9594			18.88	
Crude oil (RVP 8)						4.6266	4.0507	5.2649	50.0000	0.0500	0.2193	207.00	Option 4: RVP=7.6
Water						0.2094	0.1601	0.2716	18.0200	0.9500	0.7807	18.02	Option 2: A=8.10765, B=1750.286, C=235
Produced Water	Jul	57.24	49.54	64.95	41.45	0.2531	0.1933	0.3290	20.8248			18.88	
Crude oil (RVP 8)						4.8675	4.2302	5.5778	50.0000	0.0500	0.2106	207.00	Option 4: RVP=7.6
Water						0.2320	0.1748	0.3049	18.0200	0.9500	0.7894	18.02	Option 2: A=8.10765, B=1750.286, C=235
Produced Water	Aug	55.94	48.47	63.41	41.45	0.2420	0.1861	0.3124	20.8862			18.88	
Crude oil (RVP 8)	J					4.7548	4.1471	5.4303	50.0000	0.0500	0.2146	207.00	Option 4: RVP=7.6
Water						0.2213	0.1679	0.2890	18.0200	0.9500	0.7854	18.02	Option 2: A=8.10765, B=1750.286, C=235
Produced Water	Sep	49.76	43.18	56.34	41.45	0.1948	0.1538	0.2454	21.2000			18.88	,
Crude oil (RVP 8)	'					4,2476	3.7554	4.7893	50.0000	0.0500	0.2345	207.00	Option 4: RVP=7.6
Water						0.1763	0.1373	0.2245	18.0200	0.9500	0.7655	18.02	Option 2: A=8.10765, B=1750.286, C=235
Produced Water	Oct	44.08	38.23	49.93	41.45	0.1589	0.1283	0.1960	21.5254			18.88	, , , , , , , , , , , , , , , , , , , ,
Crude oil (RVP 8)						3.8198	3.4157	4.2608	50.0000	0.0500	0.2546	207.00	Option 4: RVP=7.6
Water						0.1422	0.1133	0.1774	18.0200	0.9500	0.7454	18.02	Option 2: A=8.10765, B=1750.286, C=235
Produced Water	Nov	35.80	31.32	40.28	41.45	0.1422	0.0991	0.1384	22.0723	0.0000	0., 107	18.88	5 p. 10.1 2. 71-0.10 100, B-11 00.200, O-200
Crude oil (RVP 8)	1404	55.50	01.02	70.20	71.70	3.2582	2.9831	3.5531	50.0000	0.0500	0.2870	207.00	Option 4: RVP=7.6
Water						0.1029	0.0859	0.1227	18.0200	0.9500	0.7130	18.02	Option 2: A=8.10765, B=1750.286, C=235
Produced Water	Dec	29.47	25.33	33.61	41.45	0.1023	0.0788	0.1227	22.5579	0.3300	0.7130	18.88	Option 2. A=0.10700, B=1700.200, O=230
Crude oil (RVP 8)	Dec	20.47	25.55	55.01	41.40	2.8745	2.6437	3.1211	50.0000	0.0500	0.3145	207.00	Option 4: RVP=7.6
Water						0.0796	0.0671	0.0942	18.0200	0.0500	0.6855	18.02	,
vvatei						0.0796	0.0671	0.0942	18.0200	0.9500	0.0833	18.02	Option 2: A=8.10765, B=1750.286, C=235

TANKS 4.0.9d Emissions Report - Detail Format Detail Calculations (AP-42)

### **Produced Water Tank - Vertical Fixed Roof Tank**

Month:	January	February	March	April	May	June	July	August	September	October	November	December
Standing Losses (lb):	0.1318	0.1458	0.2244	0.3324	0.4530	0.5345	0.6484	0.6015	0.4154	0.3142	0.1729	0.1335
Vapor Space Volume (cu ft):	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352
Vapor Density (lb/cu ft):	0.0004	0.0004	0.0005	0.0006	0.0008	0.0009	0.0010	0.0009	0.0008	0.0006	0.0005	0.0004
Vapor Space Expansion Factor:	0.0331	0.0362	0.0416	0.0512	0.0566	0.0604	0.0652	0.0629	0.0540	0.0470	0.0346	0.0316
Vented Vapor Saturation Factor:	0.9917	0.9905	0.9881	0.9847	0.9813	0.9782	0.9760	0.9770	0.9814	0.9848	0.9887	0.9911
Tank Vapor Space Volume:												
Vapor Space Volume (cu ft):	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352	345.9352
Tank Diameter (ft):	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000
Vapor Space Outage (ft):	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333
Tank Shell Height (ft):	30.0000	30.0000	30.0000	30.0000	30.0000	30.0000	30.0000	30.0000	30.0000	30.0000	30.0000	30.0000
Average Liquid Height (ft):	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000
Roof Outage (ft):	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333
Roof Outage (Cana Roof)												
Roof Outage (Cone Roof) Roof Outage (ft):	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333	0.3333
Roof Height (ft):	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
Roof Slope (ft/ft):	0.1300	0.1300	0.1300	0.1300	0.1300	0.1300	0.1300	0.1300	0.1300	0.1300	0.1300	0.1300
Shell Radius (ft):	7.7500	7.7500	7.7500	7.7500	7.7500	7.7500	7.7500	7.7500	7.7500	7.7500	7.7500	7.7500
Offer Madida (it).	7.7500	7.7500	7.7500	7.7500	7.7500	7.7500	1.1300	7.7500	7.7500	7.7500	7.7500	7.7500
Vapor Density	0.0004	0.0004	0.0005	0.0006	0.0008	0.0009	0.0010	0.0009	0.0008	0.0006	0.0005	0.0004
Vapor Density (lb/cu ft): Vapor Molecular Weight (lb/lb-mole):	22.7094	22.4208	21.9740	21.5183	21.1885	20.9594	20.8248	20.8862	21.2000	21.5254	22.0723	22.5579
Vapor Pressure at Daily Average Liquid	22.7094	22.4208	21.9740	21.5183	21.1883	20.9594	20.8248	20.8862	21.2000	21.3234	22.0723	22.5579
Surface Temperature (psia):	0.0862	0.0986	0.1235	0.1596	0.1963	0.2296	0.2531	0.2420	0.1948	0.1589	0.1173	0.0924
Daily Avg. Liquid Surface Temp. (deg. R):	487.3186	490.8447	496.8602	503.8659	509.6452	514.0987	516.9127	515.6102	509.4312	503.7493	495.4708	489.1381
Daily Avg. Equid Surface Temp. (deg. Ty).  Daily Average Ambient Temp. (deg. F):	8.9000	16.0500	28.4000	43.1500	55.2500	64.7000	70.6500	68.7000	56.2500	44.7500	27.1500	13.2000
Ideal Gas Constant R	0.3000	10.0300	20.4000	43.1300	33.2300	04.7000	70.0300	00.7000	30.2300	44.7500	27.1500	13.2000
(psia cuft / (lb-mol-deg R)):	10.731	10.731	10.731	10.731	10.731	10.731	10.731	10.731	10.731	10.731	10.731	10.731
Liquid Bulk Temperature (deg. R):	501.1192	501.1192	501.1192	501.1192	501.1192	501.1192	501.1192	501.1192	501.1192	501,1192	501.1192	501.1192
Tank Paint Solar Absorptance (Shell):	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700
Tank Paint Solar Absorptance (Roof):	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700	0.1700
Daily Total Solar Insulation												
Factor (Btu/sqft day):	388.0000	671.0000	1,104.0000	1,488.0000	1,827.0000	2,047.0000	2,193.0000	1,862.0000	1,340.0000	877.0000	479.0000	334.0000
Vapor Space Expansion Factor												
Vapor Space Expansion Factor:	0.0331	0.0362	0.0416	0.0512	0.0566	0.0604	0.0652	0.0629	0.0540	0.0470	0.0346	0.0316
Daily Vapor Temperature Range (deg. R):	17.2549	18.6740	21.0950	25.2989	27.4885	28.8957	30.8147	29.8871	26.3224	23.3985	17.9040	16.5658
Daily Vapor Pressure Range (psia):	0.0286	0.0350	0.0485	0.0735	0.0963	0.1165	0.1357	0.1264	0.0915	0.0677	0.0392	0.0292
Breather Vent Press. Setting Range(psia):	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600	0.0600
Vapor Pressure at Daily Average Liquid												
Surface Temperature (psia):	0.0862	0.0986	0.1235	0.1596	0.1963	0.2296	0.2531	0.2420	0.1948	0.1589	0.1173	0.0924
Vapor Pressure at Daily Minimum Liquid												
Surface Temperature (psia):	0.0730	0.0825	0.1014	0.1266	0.1534	0.1779	0.1933	0.1861	0.1538	0.1283	0.0991	0.0788
Vapor Pressure at Daily Maximum Liquid		0.4475	0.4400	2 2 2 2 4	0.0407	0.0014			0.0454	0.4000		
Surface Temperature (psia):	0.1016	0.1175	0.1499	0.2001	0.2497	0.2944	0.3290	0.3124	0.2454	0.1960	0.1384	0.1080
Daily Avg. Liquid Surface Temp. (deg R):	487.3186	490.8447	496.8602	503.8659	509.6452	514.0987	516.9127	515.6102	509.4312	503.7493	495.4708	489.1381
Daily Min. Liquid Surface Temp. (deg R):	483.0049	486.1762	491.5864	497.5412	502.7731	506.8747	509.2091	508.1384	502.8506	497.8997	490.9948	484.9966
Daily Max. Liquid Surface Temp. (deg R):	491.6323 21.4000	495.5132 21.5000	502.1340 22.0000	510.1906 25.3000	516.5173 26.1000	521.3226 26.6000	524.6164 28.3000	523.0820 29.2000	516.0118 27.7000	509.5990 26.7000	499.9468 21.7000	493.2796 20.8000
Daily Ambient Temp. Range (deg. R):	21.4000	21.5000	22.0000	25.3000	26.1000	26.6000	28.3000	29.2000	27.7000	26.7000	21.7000	20.8000
Vented Vapor Saturation Factor												
Vented Vapor Saturation Factor:	0.9917	0.9905	0.9881	0.9847	0.9813	0.9782	0.9760	0.9770	0.9814	0.9848	0.9887	0.9911
Vapor Pressure at Daily Average Liquid:												
Surface Temperature (psia):	0.0862	0.0986	0.1235	0.1596	0.1963	0.2296	0.2531	0.2420	0.1948	0.1589	0.1173	0.0924
Vapor Space Outage (ft):	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333	1.8333
Working Losses (lb):	4.2336	4.7801	5.8689	7.4284	8.9962	10.4071	11.4007	10.9304	8.9331	7.3995	5.5985	4.5077
WORKING LUSSES (ID).	4.2330	4.7001	5.0008	1.4204	0.3302	10.4071	11.400/	10.8304	0.8331	1.3880	5.5865	4.5077

PetroShale US 12H & 13H - Estimated Actual Annual Emissions

10/23/2019

Vapor Molecular Weight (lb/lb-mole):	22.7094	22.4208	21.9740	21.5183	21.1885	20.9594	20.8248	20.8862	21.2000	21.5254	22.0723	22.5579
Vapor Pressure at Daily Average Liquid Surface Temperature (psia):	0.0862	0.0986	0.1235	0.1596	0.1963	0.2296	0.2531	0.2420	0.1948	0.1589	0.1173	0.0924
Net Throughput (gal/mo.):	123,290.0100	123,290.0100	123,290.0100	123,290.0100	123,290.0100	123,290.0100	123,290.0100	123,290.0100	123,290.0100	123,290.0100	123,290.0100	123,290.0100
Annual Turnovers:	36.7771	36.7771	36.7771	36.7771	36.7771	36.7771	36.7771	36.7771	36.7771	36.7771	36.7771	36.7771
Turnover Factor:	0.9824	0.9824	0.9824	0.9824	0.9824	0.9824	0.9824	0.9824	0.9824	0.9824	0.9824	0.9824
Maximum Liquid Volume (gal):	40,228.2679	40,228.2679	40,228.2679	40,228.2679	40,228.2679	40,228.2679	40,228.2679	40,228.2679	40,228.2679	40,228.2679	40,228.2679	40,228.2679
Maximum Liquid Height (ft):	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000	28.5000
Tank Diameter (ft):	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000	15.5000
Working Loss Product Factor:	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500	0.7500
Total Losses (lb):	4.3654	4.9259	6.0933	7.7607	9.4492	10.9416	12.0491	11.5319	9.3485	7.7137	5.7714	4.6412
1 otal 2000co (ID).	4.3034	4.5255	0.0555	7.7007	3.4432	10.5410	12.0431	11.5519	3.3403	7.7137	5.7714	4.0412

# TANKS 4.0.9d Emissions Report - Detail Format Individual Tank Emission Totals

Emissions Report for: January, February, March, April, May, June, July, August, September, October, November, December

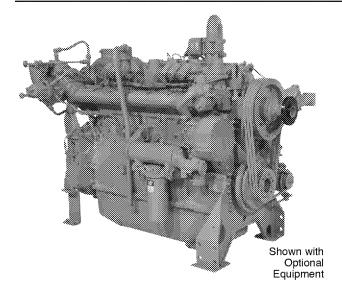
	Losses(lbs)						
Components	Working Loss	Breathing Loss	Total Emissions				
Produced Water	90.48	4.11	94.59				
Crude oil (RVP 8)	22.51	0.99	23.50				
Water	67.98	3.12	71.09				

# **CATERPILLAR®**

G3406 Gas Petroleum Engine

160-272 bkW (215-365 bhp) 1800 rpm

0.5% O<sub>2</sub> and 2.0% O<sub>2</sub> Ratings



#### **CAT® ENGINE SPECIFICATIONS**

In-line 6, 4-Stroke-Cycle
Emissions Settings 0.5% O <sub>2</sub> and 2.0% O <sub>2</sub>
Bore
Stroke
Displacement
Aspiration Naturally Aspirated or
Turbocharged-Aftercooled
Governor and Protection
Combustion Rich Burn
Engine Weight, net dry (approx) 1360.8 kg (3000 lb)
Power Density 6.7 kg/kW (11 lb/bhp)
Power per Displacement
Total Cooling System Capacity 37.9 L (10 gal)
Jacket Water 30.3 L (8 gal)
SCAC
Lube Oil System (refill) 75.7 L (20 gal)
Oil Change Interval
Rotation (from flywheel end) Counterclockwise
Flywheel and Flywheel Housing SAE No. 1
Flywheel Teeth 113

#### **FEATURES**

#### **Engine Design**

- Proven reliability and durability
- Ability to burn a wide spectrum of gaseous fuels
- Robust diesel strength design prolongs life and lowers owning and operating costs
- Broad operating speed range

#### **Emissions**

- Rich burn engine design easily meets emission requirements
- 0.5% O<sub>2</sub> rating meets U.S. EPA Spark Ignited Stationary NSPS Emissions for 2007/8 and 2010/11 with the use of aftermarket AFRC and TWC

#### **Full Range of Attachments**

Large variety of factory-installed engine attachments reduces packaging time

#### Testing

Every engine is full-load tested to ensure proper engine performance.

#### Gas Engine Rating Pro

GERP is a PC-based program designed to provide site performance capabilities for Cat® natural gas engines for the gas compression industry. GERP provides engine data for your site's altitude, ambient temperature, fuel, engine coolant heat rejection, performance data, installation drawings, spec sheets, and pump curves.

# Product Support Offered Through Global Cat Dealer Network

More than 2,200 dealer outlets

Cat factory-trained dealer technicians service every aspect of your petroleum engine

Cat parts and labor warranty

Preventive maintenance agreements available for repairbefore-failure options

S•O•S<sup>™</sup> program matches your oil and coolant samples against Caterpillar set standards to determine:

- Internal engine component condition
- Presence of unwanted fluids
- Presence of combustion by-products
- Site-specific oil change interval

#### Over 80 Years of Engine Manufacturing Experience

Over 60 years of natural gas engine production

Ownership of these manufacturing processes enables Caterpillar to produce high quality, dependable products.

- Cast engine blocks, heads, cylinder liners, and flywheel housings
- Machine critical components
- Assemble complete engine

#### Web Site

For all your petroleum power requirements, visit www.catoilandgas.cat.com.

# **CATERPILLAR®**

G3406

**GAS PETROLEUM ENGINE** 

160-272 bkW (215-365 bhp)

#### STANDARD EQUIPMENT

Air Inlet System

Air cleaner — heavy-duty Air cleaner rain cap

Service indicator

**Control System** 

Governor — Woodward PSG mechanical Governor locking — positive control

**Cooling System** 

Thermostats and housing Jacket water pump Aftercooler water pump

Aftercooler core

**Exhaust System** 

Watercooled exhaust manifolds

Dry exhaust elbow

Flywheel & Flywheel Housing

SAE No. 1 flywheel SAE No. 1 flywheel housing

SAE standard rotation

**Fuel System** 

Gas pressure regulator Natural gas carburetor **Ignition System** 

Altronic III ignition system

Instrumentation

Service meter

**Lube System** 

Crankcase breather - top mounted

Oil cooler
Oil filter — RH
Auxiliary oil reservoir
Oil pan — full sump

Oil filler in valve cover, dipstick - RH

**Mounting System** 

Engine supports

**Protection System** 

Shutoffs

General

Paint - Cat yellow

Crankshaft vibration damper and drive pulleys

Lifting eyes

#### **OPTIONAL EQUIPMENT**

#### Air Inlet System

Precleaner

#### **Charging System**

Battery chargers Charging alternators

Charging alternators f/u/w c customer supplied shutoffs

Ammeter gauge

Ammeter gauge and wiring

Control mounting

#### **Control System**

PSG Woodward governor

#### **Cooling System**

Radiators

Non-sparking blower fan

Blower fans for customer supplied radiators Fan drives for customer supplied radiators

ATAAC conversion

Aftercooler

Expansion tank

Heat exchangers

#### **Exhaust System**

Flexible fittings

Elbow

Flange

Pipe

Rain cap

Muffler

#### **Fuel System**

Fuel filter

Natural gas valve and jet kits

**Ignition System** 

CSA shielded ignition

Wiring harness

#### Instrumentation

Gauges and instrument panels

#### Lube System

Auxiliary oil reservoir removal

Lubricating oil

## Mounting System

Vibration isolators

#### Power Take-Offs

Auxiliary drive pulleys

Enclosed clutch and clutch support

Front stub shaft and flywheel stub shaft

#### **Protection System**

Gas valves

#### Starting System

Air starting motor

Electric air start control

Air pressure regulator

Air silencer

Electric starting motor — single 12- and 24-volt

Starting aids

Battery sets, cables, and rack

#### General

Damper guard

LEHW0029-00 Supersedes LEHW0615-04 Page 2 of 4



160-272 bkW (215-365 bhp)

#### **TECHNICAL DATA**

## G3406 Gas Petroleum Engine - 1800 rpm

		DM5302-01	TM8513-05	DM5084-03
Engine Power				
@ 100% Load	bkW (bhp)	242 (325)	160 (215)	205 (276)
@ 75% Load	bkW (bhp)	192 (244)	120 (161)	154 (207)
Engine Speed  Max Altitude @ Rated Torque	rpm	1800	1800	1800
and 38°C (100°F)	m (ft)	1219.2 (4000)	0	914.4 (3000)
Speed Turndown @ Max Altitude, Rated Torque, and 38°C (100°F)	%	55	45	0
SCAC Temperature	°C (°F)	54 (130)		<del>-</del>
Emissions*				
NOx	g/bkW-hr (g/bhp-hr)	35.29 (26.31)	37.47 (27.94)	20.69 (15.43)
CO	g/bkW-hr (g/bhp-hr)	2.15 (1.6)	1.9 (1.4)	20.69 (15.42)
CO,	g/bkW-hr (g/bhp-hr)	620 (463)	685 (511)	699 (521)
VOČ**	g/bkW-hr (g/bhp-hr)	0.21 (.16)	0.24 (0.18)	<u>.</u> ,
Fuel Consumption***				
@ 100% Load	MJ/bkW-hr (Btu/bhp-hr)	9.96 (7037)	10.99 (7767)	10.49 (7418)
@ 75% Load	MJ/bkW-hr (Btu/bhp-hr)	10.53 (7443)	11.75 (8304)	11.44 (8082)
Heat Balance				
Heat Rejection to Jacket Water				
@ 100% Load	bkW (Btu/min)	200 (11,401)	160 (9081)	223 (12,709)
@ 75% Load	bkW (Btu/min)	173 (9822)	138 (7868)	178 (10,156)
Heat Rejection to Aftercooler				
@ 100% Load	bkW (Btu/min)	12.6 (716)		6.53 (372)
@ 75% Load	bkW (Btu/min)	7.9 (450)	_	3.86 (220)
Heat Rejection to Exhaust				
@ 100% Load	bkW (Btu/min)	161 (9180)	128 (7292)	140 (7991)
@ 75% Load	bkW (Btu/min)	125 (7091)	99 (5636)	105 (6022)
Exhaust System				
Exhaust Gas Flow Rate				
@ 100% Load	m³/min (cfm)	38.74 (1368)	30.04 (1061)	33.1 (1168)
@ 75% Load	m³/min (cfm)	30.33 (1071)	23.84 (842)	25.4 (900)
Exhaust Stack Temperature				
@ 100% Load	°C (°F)	526 (978)	560 (1040)	540 (1004)
@ 75% Load	°C (°F)	512 (953)	535 (995)	505 (942)
Intake System				
Air Inlet Flow Rate				
@ 100% Load	m³/min (scfm)	13 (459)	9.68 (342)	10.84 (383)
@ 75% Load	m³/min (scfm)	10.36 (366)	7.93 (280)	8.72 (308)

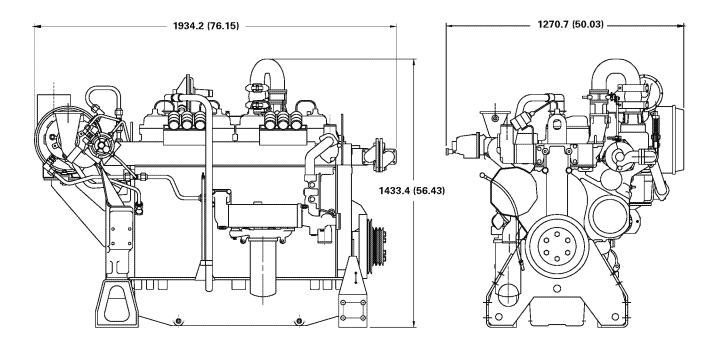
<sup>\*</sup>at 100% load and speed, all values are listed as not to exceed

<sup>\*\*</sup>Volatile organic compounds as defined in U.S. EPA 40 CFR 60, subpart JJJJ

<sup>\*\*\*</sup>ISO 3046/1

160-272 bkW (215-365 bhp)

#### **GAS PETROLEUM ENGINE**



PACKAGE DIMENSIONS						
Length	mm (in.)	1934.2 (76.15)				
Width	mm (in.)	1270.7 (50.03)				
Height	mm (in.)	1433.4 (56.43)				
Shipping Weight	kg (lb)	1360.8 (3000)				

**Note:** General configuration not to be used for installation. See general dimension drawings for detail.

Dimensions are in mm (inches).

#### RATING DEFINITIONS AND CONDITIONS

Engine performance is obtained in accordance with SAE J1995, ISO3046/1, BS5514/1, and DIN6271/1 standards.

Transient response data is acquired from an engine/ generator combination at normal operating temperature and in accordance with ISO3046/1 standard ambient conditions. Also in accordance with SAE J1995, BS5514/1, and DIN6271/1 standard reference conditions. Conditions: Power for gas engines is based on fuel having an LHV of 33.74 kJ/L (905 Btu/cu ft) at 101 kPa (29.91 in. Hg) and 15° C (59° F). Fuel rate is based on a cubic meter at 100 kPa (29.61 in. Hg) and 15.6° C (60.1° F). Air flow is based on a cubic foot at 100 kPa (29.61 in. Hg) and 25° C (77° F). Exhaust flow is based on a cubic foot at 100 kPa (29.61 in. Hg) and stack temperature.

Materials and specifications are subject to change without notice. The International System of Units (SI) is used in this publication. CAT, CATERPILLAR, their respective logos, S•O•S, "Caterpillar Yellow" and the "Power Edge" trade dress, as well as corporate and product identity used herein, are trademarks of Caterpillar and may not be used without permission.

Performance Numbers: DM5302-01, TM8513-05, DM5084-03 LEHW0029-00 (11-09) Supersedes LEHW0615-04

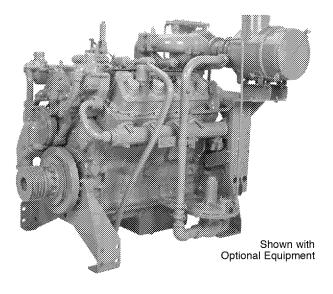
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# **CATERPILLAR®**

G3408 Gas Petroleum Engine

190-298 bkW (255-400 bhp) 1500 & 1800 rpm

2.0% O<sub>2</sub> Rating



#### CAT® ENGINE SPECIFICATIONS

V-8, 4-Stroke-Cycle	
Bore	137 mm (5.4 in.)
Stroke	152 mm (6.0 in.)
Displacement	18 L (1099 cu. in.)
Aspiration	Naturally Aspirated or
Turbo	ocharged-Aftercooled
Governor and Protection	Woodward PSG
Combustion	Rich Burn
Engine Weight, net dry (approx)	. 1678.3 kg (3700 lb)
Power Density 5	.6 kg/kW (9.3 lb/bhp)
Power per Displacement	22.2 bhp/L
Engine only Cooling System Capacit	y 54.9 L (14.5 gal)
Lube Oil System (refill)	46.2 L (12.2 gal)
Oil Change Interval	750 hours
Rotation (from flywheel end)	Counterclockwise
Flywheel and Flywheel Housing	SAE No. 0
Flywheel Teeth	136

#### **FEATURES**

#### **Engine Design**

- Improved reliability and durability
- Ability to burn a wide spectrum of gaseous fuels
- Robust diesel strength design prolongs life and lowers owning and operating costs
- Broad operating speed range

#### **Full Range of Attachments**

Large variety of factory-installed engine attachments reduces packaging time

#### Testino

Every engine is full-load tested to ensure proper engine performance.

#### Gas Engine Rating Pro

GERP is a PC-based program designed to provide site performance capabilities for Cat® natural gas engines for the gas compression industry. GERP provides engine data for your site's altitude, ambient temperature, fuel, engine coolant heat rejection, performance data, installation drawings, spec sheets, and pump curves.

# Product Support Offered Through Global Cat Dealer Network

More than 2,200 dealer outlets

Cat factory-trained dealer technicians service every aspect of your petroleum engine

Cat parts and labor warranty

Preventive maintenance agreements available for repairbefore-failure options

S•O•S<sup>SM</sup> program matches your oil and coolant samples against Caterpillar set standards to determine:

- Internal engine component condition
- Presence of unwanted fluids
- Presence of combustion by-products
- Site-specific oil change interval

#### Over 80 Years of Engine Manufacturing Experience

Over 60 years of natural gas engine production

Ownership of these manufacturing processes enables Caterpillar to produce high quality, dependable products.

- Cast engine blocks, heads, cylinder liners, and flywheel housings
- Machine critical components
- Assemble complete engine

#### Web Site

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# **CATERPILLAR®**

### G3408

#### **GAS PETROLEUM ENGINE**

190-298 bkW (255-400 bhp)

#### STANDARD EQUIPMENT

Air Inlet System

Air cleaner - single element with service indicator

**Control System** 

Governor — Woodward PSG mechanical Governor control — positive locking

**Cooling System** 

Thermostats and housing Jacket water pump Aftercooler water pump Aftercooler core

**Exhaust System** 

Watercooled exhaust manifolds

Dry exhaust elbow

Flywheel & Flywheel Housing

SAE No. 0 flywheel SAE No. 0 flywheel housing

SAE standard rotation

**Fuel System** 

Gas pressure regulator Natural gas carburetor **Ignition System** 

Digital ignition system

Instrumentation

Service meter

Lube System

Crankcase breather - top mounted

Oil cooler
Oil filter — RH
Auxiliary oil reservoir
Rear sump oil pan

Oil filler in valve cover and dipstick - RH

**Mounting System** 

Engine supports

**Protection System** 

Shutoffs

General

Paint - Cat yellow

Crankshaft vibration damper and drive pulleys

Lifting eyes

#### OPTIONAL EQUIPMENT

Air Inlet System

Air cleaner - dual element

Air inlet adapter Precleaner Air cleaner rain cap

**Charging System** 

Battery chargers

Charging alternators

Ammeter gauge

Ammeter gauge and wiring

Control mounting

Control System

EG3P/2301A speed control governor

PSG electric governor PSG pneumatic governor

**Cooling System** 

Radiators

Non-sparking blower fan

Blower fan and fan drives for customer supplied

radiators

ATAAC conversion

Aftercooler

Expansion tank

Heat exchanger

**Exhaust System** 

Flexible fittings

Elbows

Flanges

Rain caps

Mufflers

Exhaust manifold

**Fuel System** 

Dual gas regulator

Low energy fuel carburetor

Low pressure gas conversion

Propane and natural gas valve and jet kits

Fuel filter

**Ignition System** 

CSA ignition

Ignition ground wiring harness

Power supply - digital ignition system

Instrumentation

Gauges and instrument panels

Lube System

Auxiliary oil reservoir removal

Lubricating oil

**Mounting System** 

Vibration isolators

Power Take-Offs

Auxiliary drive pulleys

Enclosed clutch

Clutch support

Front stub shaft

Flywheel stub shaft

Pulley removal

**Protection System** 

Gas valves

Starting System

Air starting motor

Electric air start control

Air pressure regulator

Air silencer

Electric starting motor - single 24-volt

Starting aids

Battery sets (24-volt dry), cables, and rack

LEHW0030-00 Supersedes LEHW0747-05 Page 2 of 4



190-298 bkW (255-400 bhp)

## **TECHNICAL DATA**

## G3408 Gas Petroleum Engine - 1500 and 1800 rpm

		DM8633-01	TM9151-05	TM9213-04
Engine Power				<del></del>
@ 100% Load	bkW (bhp)	248 (332)	190 (255)	298 (400)
@ 75% Load	bkW (bhp)	186 (249)	143 (191)	224 (300)
Engine Speed May Altitude @ Rated Torque	rpm	1500	1800	1800
Max Altitude @ Rated Torque and 38°C (100°F)	m (ft)	914.4 (3000)	0	1219.2 (4000)
Speed Turndown @ Max Altitude, Rated Torque, and 38°C (100°F)	%	0	45	0
SCAC Temperature	°C (°F)	54 (130)	N/A	54 (130)
Emissions*				
NOx	g/bkW-hr (g/bhp-hr)	18.92 (14.11)	34.39 (25.64)	35.23 (26.27)
co	g/bkW-hr (g/bhp-hr)	18.91 (14.10)	2 (1.5)	2.15 (1.6)
CO <sub>2</sub>	g/bkW-hr (g/bhp-hr)	657 (490) <sup>′</sup>	654 (488)	616 (459)
VOC**	g/bkW-hr (g/bhp-hr)	<u> </u>	.3 (.22)	.21 (.16)
Fuel Consumption***				
@ 100% Load	MJ/bkW-hr (Btu/bhp-hr)	10.62 (7507)	10.71 (7568)	9.92 (7008)
@ 75% Load	MJ/bkW-hr (Btu/bhp-hr)	11.14 (7874)	11.64 (8225)	10.40 (7350)
Heat Balance				
Heat Rejection to Jacket Water				
@ 100% Load	bkW (Btu/min)	279.73 (15,922)	179 (10,169)	253 (14,372)
@ 75% Load	bkW (Btu/min)	209.84 (11,944)	164 (9324)	217 (12,368)
Heat Rejection to Aftercooler				
@ 100% Load	bkW (Btu/min)	4.36 (248)	N/A	22.7 (1292)
@ 75% Load	bkW (Btu/min)	1.74 (99)	N/A	14.5 (828)
Heat Rejection to Exhaust				
@ 100% Load	bkW (Btu/min)	168.24 (9576)	151 (8583)	183 (10,382)
@ 75% Load	bkW (Btu/min)	121.07 (6891)	114 (6501)	136 (7749)
Exhaust System Exhaust Gas Flow Rate				
@ 100% Load	m³/min (cfm)	38.37 (1355)	34.57 (1221)	45.08 (1592)
@ 75% Load	m³/min (cfm)	28.94 (1022)	26.33 (930)	34.43 (1216)
Exhaust Stack Temperature				
@ 100% Load	°C (°F)	513.89 (957)	576 (1069)	490 (914)
@ 75% Load	°C (°F)	478.89 (894)	565 (1050)	464 (867)
Intake System				
Air Inlet Flow Rate				
@ 100% Load	m³/min (scfm)	12.97 (458)	10.90 (385)	15.83 (559)
@ 75% Load	m³/min (scfm)	10.25 (362)	8.35 (295)	12.52 (442)
Gas Pressure	kPag (psig)	10.3-34.5	10.34-34.47	137.9-172.4
		(1.5-5)	(1.5-5)	(20-25)

<sup>\*</sup>at 100% load and speed, all values are listed as not to exceed

<sup>\*\*</sup>Volatile organic compounds as defined in U.S. EPA 40 CFR 60, subpart JJJJ

<sup>\*\*\*</sup>ISO 3046/1

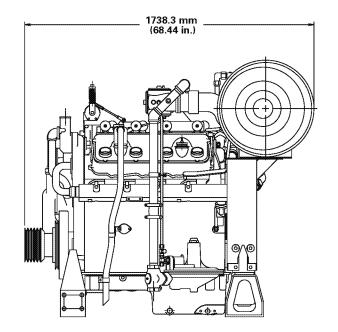


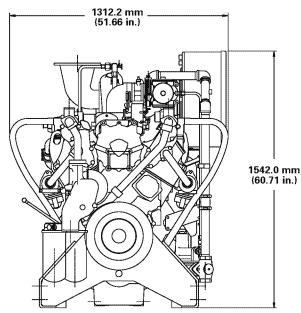
## G3408

## **GAS PETROLEUM ENGINE**

190-298 bkW (255-400 bhp)

## **GAS PETROLEUM ENGINE**





PACKAGE DIMENSIONS						
<b>Length</b> mm (in.) 1738.3 (68.44)						
Width	mm (in.)	1312.2 (51.66)				
Height	mm (in.)	1542.0 (60.71)				
Shipping Weight	kg (lb)	1678.3 (3700)				

**Note:** General configuration not to be used for installation. See general dimension drawings for detail.

Dimensions are in mm (inches).

## **RATING DEFINITIONS AND CONDITIONS**

Engine performance is obtained in accordance with SAE J1995, ISO3046/1, BS5514/1, and DIN6271/1 standards.

Transient response data is acquired from an engine/generator combination at normal operating temperature and in accordance with ISO3046/1 standard ambient conditions. Also in accordance with SAE J1995, BS5514/1, and DIN6271/1 standard reference conditions.

Conditions: Power for gas engines is based on fuel having an LHV of 33.74 kJ/L (905 Btu/cu ft) at 101 kPa (29.91 in. Hg) and 15° C (59° F). Fuel rate is based on a cubic meter at 100 kPa (29.61 in. Hg) and 15.6° C (60.1° F). Air flow is based on a cubic foot at 100 kPa (29.61 in. Hg) and 25° C (77° F). Exhaust flow is based on a cubic foot at 100 kPa (29.61 in. Hg) and stack temperature.

Materials and specifications are subject to change without notice. The International System of Units (SI) is used in this publication. CAT, CATERPILLAR, their respective logos, S•O•S, "Caterpillar Yellow" and the "Power Edge" trade dress, as well as corporate and product identity used herein, are trademarks of Caterpillar and may not be used without permission.



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Steffes Corporation Dickinson, North Dakota

High Pressure Coanda Flare Tip
And
Low Pressure Ball Tip
Performance Testing

Test Dates: July 24 & 25, 2012

Report Prepared By:

Steve Freeman Project Manager



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Report Contents	Page(s)
Summary	3
Appendix A- Gas Analysis Data	6
Appendix B- Flare Tip Calibration Data	11
Appendix C- Method 22 Field Sheets	14
Appendix D- Example Pilot Temperature Thermocouple Data	19



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#### **Summary:**

Precision Analysis was contracted to evaluate for compliance, the Steffes Corporation Flare Stacks. Field testing was conducted at the Kodiak Oil & Gas Inc., Smokey 16-20-32-16H3 location in McKenzie County south of Watford City, North Dakota. The high pressure Coanda flare tip and the low pressure Ball flare tip were tested to satisfy the specifications as described in 40 Code of Federal Reference (CFR) §60.18.

- Flare Operates with no visible emissions
  - o High Pressure Flare. Confirmed no visible emissions at 27 mscfd and 1403 mscfd.
  - o Low Pressure Flare. Confirmed no visible emissions at 17,280 scfd and 106.560 scfd.
- Flame is present at all times
  - o Observed thermocouple data logging system of pilot temperature was operational.
- Exit Velocity is less than 400 fps
  - o High Pressure Flare. Confirmed exit velocity less than 400 fps for flow rates up to 1.1 mmscfd.
  - Low Pressure Flare. Confirmed exit velocity less than 400 fps for all flow rates tested. Tested to 146,880 scfd.
- BTU content of gas in high and low pressure flare systems was greater than 1,000 BTU/scf which allows an exit velocity of 400 fps. Actual measurements during the test ranged from 1477 to 1774 BTU/scf.

The testing occurred on Tuesday, July 24 and Wednesday, July 25, 2012. Present during the tests were Dean Kovash, Jim Godlevsky, Todd Mayer, and Levi Jurgens from the Steffes Corporation. Kodiak Oil and Gas was represented by Travis Simnioniw and the testers for Precision Analysis were Scott Fairfield and Steve Freeman.

The high pressure Coanda flare tip and the low pressure Ball flare tip performance tests have shown the flares to be operating in accordance to specifications as described in 40 Code of Federal Reference (CFR) §60.18.

#### Methods:

The following EPA source emissions test methods were used.

### 40 CFR Part 60, Appendix A

- EPA Test Method 2 Determination of Stack Gas Velocity and Volumetric Flow Rate
- EPA Test Method 22 Visual Determination of Fugitive Emissions from Material Sources and Smoke Emissions from Flares

### **GPA METHOD 2261**

GPA Test Method 2261 – Analysis for Natural and Similar Gaseous Mixtures by Gas Chromatography

### Analysis for Natural Gas and Similar Gaseous Mixtures by Gas Chromatography

Components to be determined in a gaseous sample are physically separated by gas chromatography and compared to calibration data obtained under identical operating conditions. A fixed volume of sample in the gaseous phase is isolated in a suitable inlet sample system and entered into the column.



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#### **Test Narrative:**

#### **High Pressure Flare**

Precision Analysis conducted a gas analysis and verified the calibration of the ABB flow rate meter on the high pressure line prior to the testing. The flow exit area was then verified by inserting shims that were measured by a calibrated caliper. During the measurement verifications, the data from the analog proximity sensor (transducer) was recorded and used to establish the flow calibration chart. The flow and the transducer readings were recorded during the flare test so the exit velocity could be determined. The results are included in the following chart.

Table 1. Gas Flow Rates for 6" High Pressure Flare

Linear Trans.	Lin Trans	Corrected	Flow	Exit Area	Exit Velocity
Displacement	Disp	Displacement	Rate (scfd)	(sq ft)	(fps)
Reading (in)	Zeroed (in)	Reading (in)		(Calculated)	(Calculated)
0.133	0	0	0	0.01806687	0
0.138	0.005	0.008	64000	0.019223149	38.53378715
0.145	0.012	0.019	125000	0.020813034	69.51217572
0.154	0.021	0.03	227000	0.022402918	117.2755613
0.161	0.028	0.037	299000	0.023414663	147.7983327
0.169	0.036	0.046	378000	0.024715478	177.0145847
0.174	0.041	0.049	431000	0.025149082	198.3541919
0.182	0.049	0.053	510000	0.025727222	229.437042
0.19	0.057	0.057	582000	0.026305362	256.0736889
0.197	0.064	0.061	660000	0.026883502	284.1478357
0.205	0.072	0.067	747000	0.027750712	311.5535716
0.217	0.084	0.077	839000	0.029196061	332.6013078
0.222	0.089	0.082	890000	0.029918736	344.2968286
0.232	0.099	0.09	1007000	0.031075016	375.0631284
0.244	0.111	0.1	1160000	0.032520365	412.846714
0.25	0.117	0.105	1258000	0.03324304	437.991988
0.262	0.129	0.115	1403000	0.03468839	468.1227962



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#### **Low Pressure Flare**

Precision Analysis conducted a gas analysis on the tank vapor line prior to the testing. The flow exit area was then verified by using a dial indicator. During the measurement verifications, the data from the analog proximity sensor (transducer) was recorded and used to establish the flow calibration chart. Flow rates from the tanks were calculated using a S-Type Pitot tube fixed in the supply line to the flare. The flow and the Transducer readings were recorded during the flare test so the exit velocity could be determined. The results are included in the following chart.

Table 2. Gas Flow Rates for 3" Low Pressure Flare

	Lin Trans					
Linear Trans.	Disp	Corrected				Exit Velocity
Displacement	Zeroed	Displacement	Pitot Tube		Exit	(fps)
Reading (in)	(in)	Reading (in)	Velocity-Raw	Flow Rate (scfd)	Area (sq ft)	(Calculated)
0.102	0	0	0	0	0	0
0.129	0.027	0.023	0.015	31680	0.00124	295.6989247
0.179	0.077	0.061	0.115	86400	0.0033	303.030303
0.213	0.111	0.088	0.204	115200	0.0047	283.6879433
0.22	0.118	0.094	0.229	122400	0.0049	289.1156463
0.232	0.13	0.103	0.27	132480	0.0055	278.7878788
0.238	0.136	0.107	0.285	136800	0.0057	277.7777778
0.244	0.142	0.111	0.304	139680	0.006	269.4444444
0.247	0.145	0.113	0.308	141120	0.0061	267.7595628
0.249	0.147	0.115	0.333	146880	0.0062	274.1935484

### **Visible Emissions**

Visible emissions from the flare were determined by using EPA Method 22 as outlined in 40 CFR §60.18 paragraph (c) (1). Both flare stacks were observed at the high and low rates. The total observation time for each test was two hours. The observer also verified that the flame was present at all times during the tests. The Field observation sheets are included in Appendix C.

# Appendix A Gas Analysis Data



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Run File C:\Galaxie\data\12\_07\_24\Kodiak Run 13\_4.DATA

Method S1\_C10

Operator User1 Analysis Date 7/24/2012

Client: Steffes Corporation Date Sampled: 7/24/2012

Sample Identification: Kodiak Run 1 Purpose: Flare testing

Unique #: Pressure (PSI): 48.8 PSIA

Temperature (DEG F): 89 Sample Type: Onsite

Sampled By: S. Fairfield County: McKenzie

	000000000000000000000000000000000000000	000000000000000000000000000000000000000	000000000000000000000000000000000000000		***************************************	***************************************
Component	Mole %	<u>BTU</u>	<u>GPM</u>			
Nitrogen (N2)	1.1538	0.0000	0.0000			
Carbon Dioxide	0.6858	0.0000	0.0000			
Methane (CH4)	59.5731	603.0798	0.0000			
Ethane (C2)	18.8902	335.0731	5.0507			
Propane (C3)	10.5339	265.6574	2.9013			
iso-Butane (i-C4)	1.4945	48.7125	0.4889			
Butane (C4)	4.0349	131.9355	1.2717			
iso-Pentane (i-C5)	0.8573	34.3779	0.3134			
Pentane (C5)	1.1849	47.6074	0.4294			
Hexanes (C6)	0.7670	36.5599	0.3153			
Heptanes (C7)	0.4301	23.7219	0.1984			
Octanes (C8)	0.1784	11.1723	0.0914			
Nonanes (C9)	0.0316	2.2182	0.0178			
Decanes+	0.0148	1.1515	0.0091			
Benzene	0.0888	3.3305	0.0248			
Toluene	0.0569	2.5518	0.0190			
Ethylbenzene	0.0028	0.1443	0.0011			
Xylenes	0.0214	1.1152	0.0081			
Totals	100.0000	1548.4092	11.1406			
Specific Gravity from Composit	ion	0.9271				
BTUs @ 14.730 Saturated	(Ideal)	1521.4608	BTUs @	14.730	Saturated (Real)	1530.7392
BTUs @ 14.730 Dry (Ideal)		1548.4092	BTUs @	14.730	Dry (Real)	1557.8520
Compressibility		0.99394				



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Run File C:\Galaxie\data\12\_07\_24\Kodiak Run 24\_4.DATA

Method S1\_C10

Operator User1 Analysis Date 7/24/2012

Client: Steffes Corporation Date Sampled: 7/24/2012

Sample Identification: Kodiak Run 2 Purpose: Flare testing

Unique #: Pressure (PSI): 45.0 psia

Temperature (DEG F): 89 Sample Type: Onsite

Sampled By: S. Fairfield County: McKenzie

					.,.	
Component	Mole %	<u>BTU</u>	<u>GPM</u>	000000000000000000000000000000000000000		
Nitrogen (N2)	1.2555	0.0000	0.0000			
Carbon Dioxide	0.6727	0.0000	0.0000			
Methane (CH4)	62.6000	633.7223	0.0000			
Ethane (C2)	17.7990	315.7183	4.7589			
Propane (C3)	9.2802	234.0397	2.5560			
iso-Butane (i-C4)	1.3015	42.4198	0.4258			
Butane (C4)	3.5481	116.0178	1.1183			
iso-Pentane (i-C5)	0.7904	31.6953	0.2890			
Pentane (C5)	1.1172	44.8873	0.4049			
Hexanes (C6)	0.7701	36.7085	0.3166			
Heptanes (C7)	0.4685	25.8387	0.2161			
Octanes (C8)	0.1844	11.5488	0.0944			
Nonanes (C9)	0.0306	2.1465	0.0172			
Decanes+	0.0172	1.3366	0.0106			
Benzene	0.0915	3.4317	0.0256			
Toluene	0.0588	2.6392	0.0197			
Ethylbenzene	0.0011	0.0582	0.0004			
Xylenes	0.0132	0.6907	0.0050			
Totals	100.0000	1502.8993	10.2585			
Specific Gravity from Composit	tion	0.8982				
BTUs @ 14.730 Saturated	(Ideal)	1476.7429	BTUs @	14.730	Saturated (Real)	1485.1458
BTUs @ 14.730 Dry (Ideal)		1502.8993	BTUs @	14.730	Dry (Real)	1511.4510
Compressibility		0.99434				



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Run File C:\Galaxie\data\12\_07\_24\Kodiak Run 36\_7\_24\_2012 5\_56\_05 PM\_4.DATA

Method S1\_C10

Operator User1 Analysis Date 7/24/2012

Client: Steffes Corporation Date Sampled: 7/24/2012

Sample Identification: Kodiak Run 3 Purpose: Flare Testing

Unique #: Pressure (PSI): 71.2 PSIA

Temperature (DEG F): 91.1 Sample Type: Onsite

Sampled By: S. Fairfield County: McKenzie

Component	Mole %	<u>BTU</u>	<u>GPM</u>			
Nitrogen (N2)	1.1609	0.0000	0.0000			
Carbon Dioxide	0.6673	0.0000	0.0000			
Methane (CH4)	59.9011	606.4012	0.0000			
Ethane (C2)	19.8039	351.2810	5.2950			
Propane (C3)	10.6897	269.5868	2.9443			
iso-Butane (i-C4)	1.4061	45.8292	0.4600			
Butane (C4)	3.6111	118.0773	1.1382			
iso-Pentane (i-C5)	0.6894	27.6451	0.2521			
Pentane (C5)	0.9209	37.0028	0.3337			
Hexanes (C6)	0.5527	26.3469	0.2272			
Heptanes (C7)	0.3171	17.4883	0.1463			
Octanes (C8)	0.1241	7.7739	0.0636			
Nonanes (C9)	0.0241	1.6905	0.0136			
Decanes+	0.0108	0.8384	0.0066			
Benzene	0.0623	2.3362	0.0174			
Toluene	0.0396	1.7768	0.0133			
Ethylbenzene	0.0021	0.1074	0.0008			
Xylenes	0.0167	0.8733	0.0064			
Totals	100.0000	1515.0553	10.9183			
Specific Gravity from Composit	tion	0.9047				
BTUs @ 14.730 Saturated	(Ideal)	1488.6874	BTUs @	14.730	Saturated (Real)	1497.2861
BTUs @ 14.730 Dry (Ideal)		1515.0553	BTUs @	14.730	Dry (Real)	1523.8064
Compressibility		0.99426				



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Run File C:\Galaxie\data\12\_07\_24\Kodiak Vapor 15\_7\_24\_2012 5\_00\_01 PM\_3.DATA

Method S1\_C10

Operator User1 Analysis Date 7/24/2012

Client: Steffes Corporation Date Sampled: 7/24/2012

Sample Identification: Kodiak Vapor 1 Purpose: Vapor test

Unique #: Pressure (PSI): 10 "

Temperature (DEG F): 78 Sample Type: Onsite

Sampled By: S.Fairfield County: McKenzie

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Component	Mole %	<u>BTU</u>	<u>GPM</u>	000000000000000000000000000000000000000		
Nitrogen (N2)	5.8016	0.0000	0.0000			
Carbon Dioxide	0.6163	0.0000	0.0000			
Methane (CH4)	43.2367	437.7006	0.0000			
Ethane (C2)	19.4275	344.6032	5.1943			
Propane (C3)	17.9997	453.9389	4.9576			
iso-Butane (i-C4)	3.3742	109.9803	1.1039			
Butane (C4)	0.0000	0.0000	0.0000			
iso-Pentane (i-C5)	2.2881	91.7545	0.8366			
Pentane (C5)	3.1765	127.6324	1.1512			
Hexanes (C6)	2.0383	97.1655	0.8380			
Heptanes (C7)	1.1109	61.2723	0.5124			
Octanes (C8)	0.4395	27.5279	0.2251			
Nonanes (C9)	0.0624	4.3727	0.0351			
Decanes+	0.0245	1.9023	0.0151			
Benzene	0.2296	8.6096	0.0642			
Toluene	0.1364	6.1182	0.0457			
Ethylbenzene	0.0024	0.1252	0.0009			
Xylenes	0.0355	1.8536	0.0135			
Totals	100.0000	1774.5570	14.9936			
Specific Gravity from Composit	tion	1.1262				
BTUs @ 14.730 Saturated	(Ideal)	1743.6727	BTUs @	14.730	Saturated (Real)	1758.9081
BTUs @ 14.730 Dry (Ideal)		1774.5570	BTUs @	14.730	Dry (Real)	1790.0623
Compressibility		0.99134				

# Appendix B Flare Tip Calibration Data

Correction Table
Date: July 25, 2012

Description: High Pressure Flare (6" Coanda)--Standard Springs

Technician: Steve Freeman

Measured Disp (in)	Linear Transducer	Lin Trans Rdg
(shims)	Reading (inch)	Zeroed (inch)
0	0.151	0
0.021	0.164	0.013
0.046	0.187	0.036
0.06	0.214	0.063
0.123	0.29	0.139
0.154	0.321	0.17
0.185	0.347	0.196

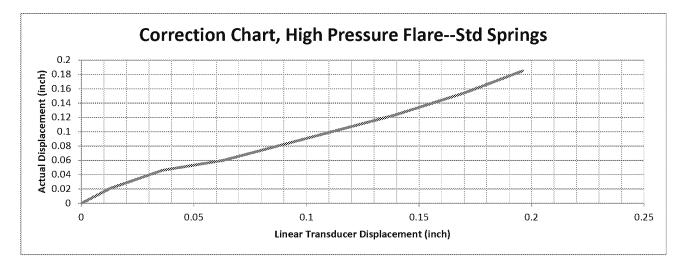
Example of interpolating data from chart

Measured Trans

Displacement Lin Trans Rdg Reading Corrected Reading

0.06 0.063 0.129 0.114710526

0.123 0.139



Correction Table Date: July 25, 2012

Description: Low Pressure Flare Technician: Steve Freeman

Measured Disp (in)	Linear Transducer	Lin Trans Rdg
(dial indicator)	Reading (inch)	Zeroed (inch)
0	0.149	0
0.008	0.158	0.009
0.018	0.169	0.02
0.022	0.175	0.026
0.03	0.186	0.037
0.036	0.193	0.044
0.065	0.231	0.082
0.08	0.25	0.101
0.09	0.262	0.113
0.1	0.275	0.126
0.11	0.29	0.141
0.12	0.303	0.154

Example of interpolating data from chart

Measured

Trans Displacement Lin Trans Rdg Reading Corrected Reading

> 0.11 0.141 0.12 0.154

**Correction Chart, Low Pressure Flare** 0.14 O.12 0.1 0.08 0.06 0.04 0.02 0 0 0.02 0.04 0.06 0.08 0.1 0.12 0.14 0.16 0.18 Linear Transducer Displacement (inch)

0.147

0.114615385

# Appendix C Method 22 Field Data Sheets

Ligh Pressure flave at Low flow of 27 mscfd FUGITIVE OR SMOKE EMISSION INSPECTION OUTDOOR LOCATION Company Steffes Corp Observer Twe freemen Location Kodiak, Smokey 16-20 32-1613 Affiliation Pression Date 7-24-12 Company Rep. Sky Conditions Pt Cloudy Wind Direction  $N^{\omega}$ Wind Speed 0-5 Precipitation Process Unit fore Industry Sketch process unit: indicate observer position relative to source; indicate potential emission points and/or actual emission points. V 100' AWay Accumulated Observation OBSERVATIONS emission period Clock duration, time, Time min:sec min:sec 0:03 Begin 20:00 Observation 10:30 0 0 0 20:00 End 20:00 Observation Figure 22-1

H:	gh pressure	slave at H	Zgk S10	w Rad	e of 1403 p	<u>1</u> scfol
	* 1	VE OR SMOKE EN OUTDOOR L	MISSION 3			-
Loc Com	pany Steffes Co ation Kodiak, Si pany Rep.	nokey 16-20-32-	16143	Affili	rerSteuc Freeman ation pacision A 1-24-12	ne/45:5
Sky	Conditions Pl	Cloudy		-8	Direction NW Speed 0-/o	To the state of th
Ind	lustry		X4000000000000000000000000000000000000	Proces	ss Unit flare	
to	etch process un source; indica ual emission p	te potential (	observe emission	r posit points	cion relative s and/or	CONTRACTOR
NO.000000000000000000000000000000000000	l V	li li	p <sup>d</sup>	W		OSESTATORIOS CONTRACTORIOS CONT
age capeac construction and ca		<i>\$</i>			8'Shack 100'away	000000000000000000000000000000000000000
The state of the s	OBSERVATIONS	Clock Time	Observ peri durat min:	iod ion,	Accumulated emission time, min:sec	nave entre construction and the construction and th
***************************************	Begin Observation	<u> 13:05</u> 13:30	30,	AND		NO STATE OF THE PROPERTY OF TH
***************************************		14:00	20:		naminationeerialisella communication and	AAAAAA
***************************************		14:25	201	and the second second second		and the second
		14:50	20.			
en de la constanta de la const		15:15	201	00		000000000000000000000000000000000000000
NOROSE SCOLOSOS CONTRACTOR DE				GERENEZ ER STERFER DE		VALES CONTRACTOR OF THE STATE O
CERCONOCIONALINA COLORIA DE PROPERTO DE COLORIA DE COLO	End Observation	15:35	120:6			TO A STATE OF THE

Figure 22-1

Tank Gas Low Pressure flave at High flow of 106,560 sedd

FUGITIVE	OR SMOKE EN		NSPECT	ION
Company Steffes Corp. Location Kodak, Smokey 16-20-32-16H3			Observer Steek Freeman Affiliation Pression	
Company Rep.			Date 7-25-/2	
Sky Conditions Clear Blue Precipitation NoNE			Wind Direction W Wind Speed /0-20	
Industry			Process Unit	
Sketch process unit: to source; indicate actual emission poin	potential e		points W	ion relative and/or  8 'Shak /00' Away
OBSERVATIONS	Clock Time	Observation period duration, min:sec		Accumulated emission time, min:sec
Observation	09:55 10:20	<u> 20%</u> 20%	nanagangangangangangan	<u> </u>
	10:45	70:0	Nonekogoucis/skratitolog	0
<del></del>	11:10	200	200000000000000000000000000000000000000	۵
	11:35	20.00		
	12:00	20:0	200000000000000000	
		Contraction of the Contraction o		
End Observation	12:20	1200	))	
Figure 22-1				

Tank Gas Low pressure Store at Low Slow of 17,280 Schol FUGITIVE OR SMOKE EMISSION INSPECTION OUTDOOR LOCATION Company Steffes Corp. Observer freene Location Koduk, Smokey 16-20-32-16 H3 Affiliation Prosper Company Rep. Date Clear -Blue Wind Direction  $N^{\omega}$ Sky Conditions Precipitation NONS Wind Speed Process Unit Industry Sketch process unit: indicate observer position relative to source; indicate potential emission points and/or actual emission points. 81 Stack OBSERVATIONS Accumulated Observation Clock period emission Time duration, time, min:sec min:sec Begin 20:00 Observation 12:55 20:00 2000 20:00 14:70 20:00 20:00 End 20:00 Observation

Figure 22-1

